

Banja Luka 10.03.2020

Knowledge FOr Resilient soCiEty KURS CJELOŽIVOTNOG UČENJA PROTIVPOŽARNE GRAĐEVINSKE MJERE

OTPORNOST KONSTRUKCIJA NA POŽAR Doc. Dr Igor Džolev



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Personal introduction

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Civil Engineering Statics of structures Computational structural analysis Concrete bridges Steel bridges Architecture Theory of structures Disaster Risk Management and Fire Safety Risk Analysis Methods

Nonlinear thermo-mechanical analysis of the behavior of reinforced concrete frame structures subjected to fire











Novi Sad, Open University Fire, 2000



April 6, 2000

April 6, 2000

present day



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Basic requirements

General objectives \rightarrow Risk limitation

- Load bearing resistance needs to be provided for a specified period of time
- Generation and spread of fire and smoke need to be limited
- Spread of fire to neighbouring structures needs to be limited
- Safe evacuation of occupants need to be provided
- Safety of rescue teams needs to be taken into consideration

Methods of fire resistance assessment

- standard fire tests
- tabulated data (largely prescriptive but also increasingly based on calculations)
- simplified calculations (neglecting complex effects, such as thermal stresses)
- advanced calculations (largely performance based)
- full scale fire tests





Basic requirements

Evaluation complexity levels

- Member analysis
- Substructure analysis
- Global structural analysis

Prescriptive and Performance based design

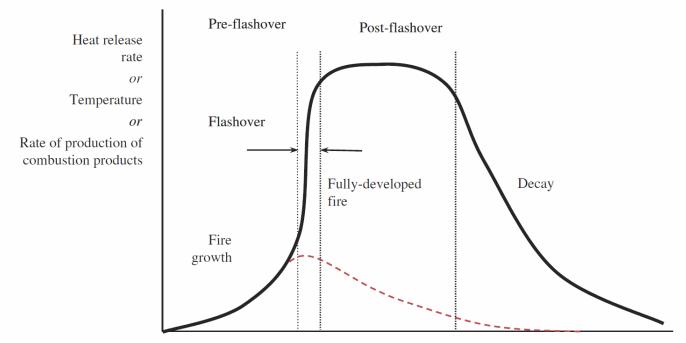
Modelling real fire to a realistic and conservative scenario

- Availability of combustible materials
- Ventilation conditions, in terms of oxygen delivery
- Physical characteristics of the space in which fire is initiated





Fire - process of uncontrolled combustion endangering human lives and health, material goods and the environment





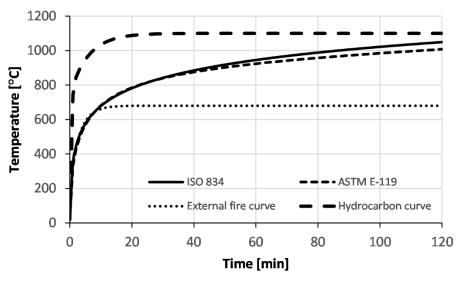
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Fire models

- Standard fire curves ISO 834, ASTM E119, Hydrocarbon, External
- Parametric fire curves
- Advanced multi-zone and CFD models







Standard fire \rightarrow Fire resistance measured in minutes

- **R** load bearing function ability of a structure or a member to sustain specified actions during the relevant fire, according to defined criteria
- **E integrity function** ability of a separating element, when exposed to fire on one side, to prevent the passage through it of flames and hot gases and to prevent the occurrence of flames on the unexposed side
- I insulation function ability of a separating element when exposed to fire on one side, to restrict the temperature rise of the unexposed face below specified levels

REI 60, EI 90, ...





Parametric fire curves

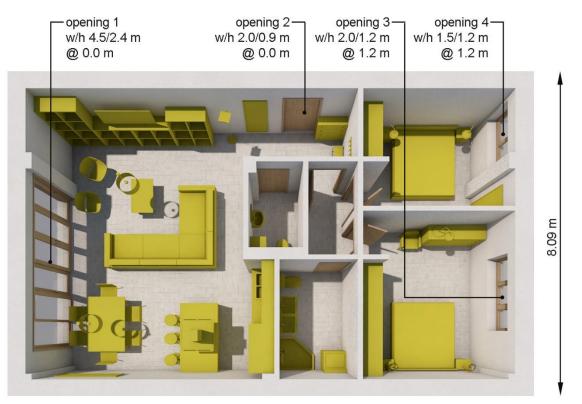
- More detailed assessment of a fire that could develop in a specific compartment
- Taking into account real geometric and material properties of the compartment, as well as ventilation conditions
- Include a cooling (decay) phase of the fire, providing temperature-time evolution during the whole course of fire

Multi-zone and CFD

- Based on mass and energy conservation laws
- Iterative procedure is needed, conditioning the use of these models to specialized computer software







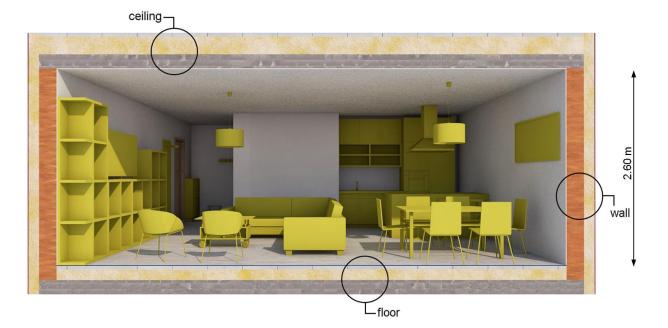
12.10 m



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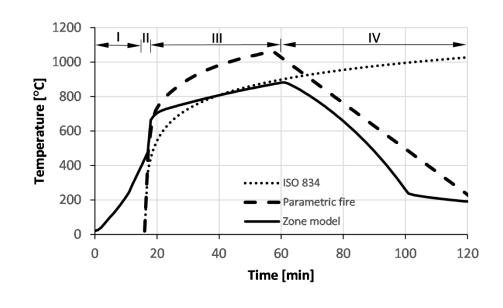
Ceramic tiles			
Concrete screed			
Rock wool			
Concrete			
Mortar			
Concrete			
Rock wool			
Concrete screed			
Mortar			
Thermo-block			
Rock wool			
Mortar			







Temperature-time curves corresponding to analysed compartment







Structural fire design analysis

- Selection of the relevant design fire scenarios
- Determination of the corresponding design fires
- Calculation of temperature evolution within the structural members
- Calculation of the mechanical behaviour of the structure exposed to fire

EN	Part	Title
EN 1990	n/a	Basis of structural design
EN 1991	1-2	Actions on structures - General actions - Actions on structures exposed to fire
EN 1992	1-2	Design of concrete structures - General rules - Structural fire design
EN 1993	1-2	Design of steel structures - General rules - Structural fire design
EN 1994	1-2	Design of composite steel and concrete structures - General rules - Structural fire design
EN 1995	1-2	Design of timber structures - General rules - Structural fire design
EN 1996	1-2	Design of masonry structures - General rules - Structural fire design
EN 1999	1-2	Design of aluminium structures - Structural fire design





Numerical model complexity

- Based on fundamental physical behaviour
- Temperature-time field coupled with structural response material nonlinearity and degradation at elevated temperatures

General purpose programs - ANSYS, ABAQUS

Specialised programs - SAFIR, VULKAN, OPENSEES





Thermal response - Heat transfer

- Conduction
- Convection
- Radiation

Input parameters

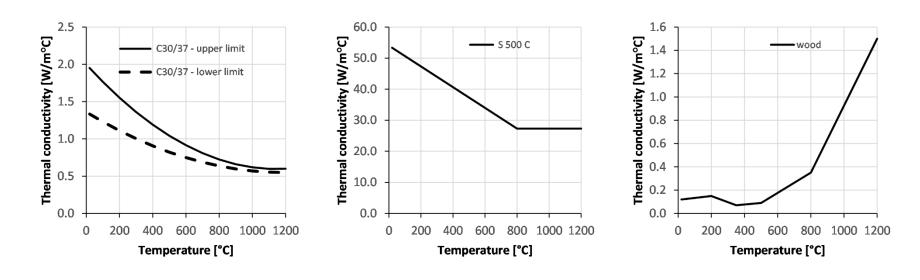
- Thermal conductivity
- Specific heat
- Density

$\frac{\partial}{\partial x} \left(\lambda_{x} \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(\lambda_{y} \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(\lambda_{z} \frac{\partial T}{\partial z} \right) = \rho c \frac{\partial T}{\partial t}$





Thermal conductivity



concrete



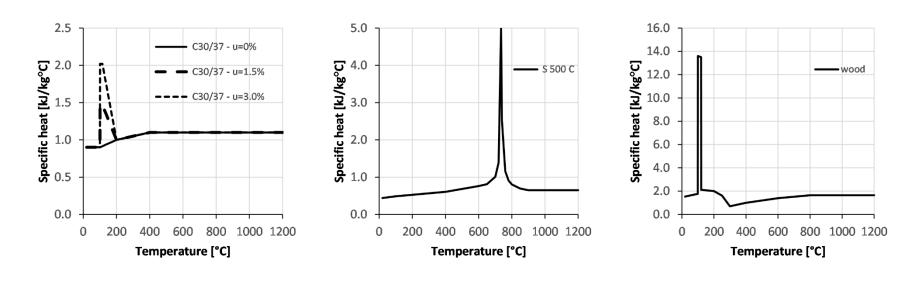
wood



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Specific heat



concrete

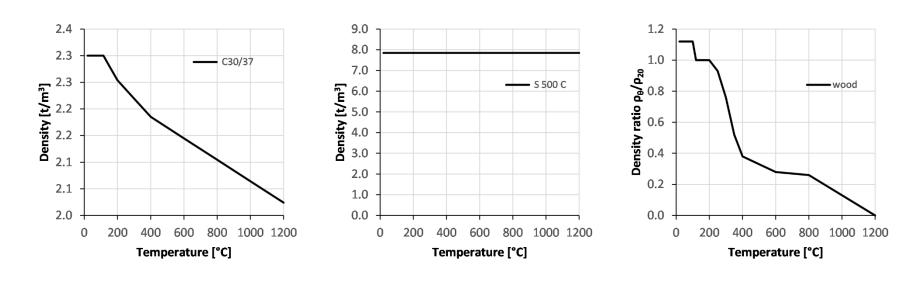








Density



concrete



wood



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Mechanical response - Structural analysis

- Material nonlinearity
- Degradation at elevated temperatures

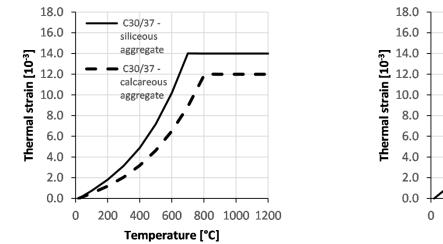
Temperature dependent properties

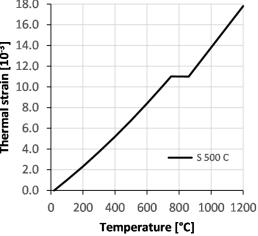
- Thermal strains
- Stress-strain relations





Thermal expansion





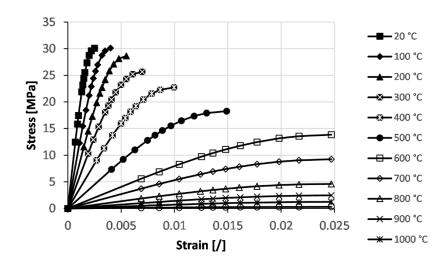
steel

concrete





Stress-strain relations - Concrete



3.5 3 2.5 -20 °C Stress [MPa] → 100 °C 2 **▲** 200 °C 1.5 -x- 300 °C **→3** 400 °C ● 500 °C 0.5 0 0.0005 0.001 0.0015 0.002 0.0025 0.003 0 Strain [/]

compression

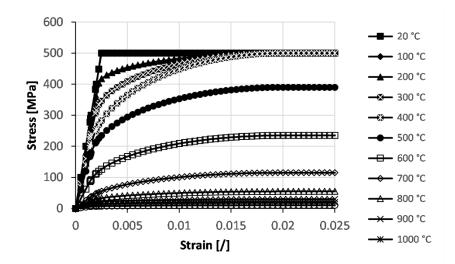
tension

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Stress-strain relations - Steel

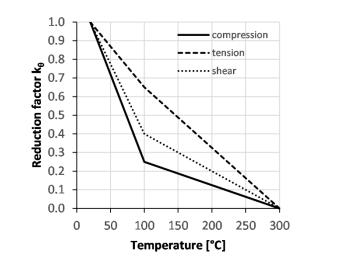


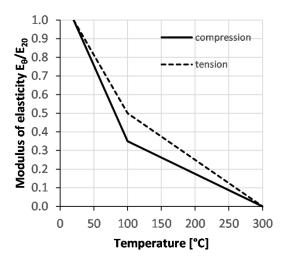
tension and compression





Strength and stiffness reduction factors - Wood





strength

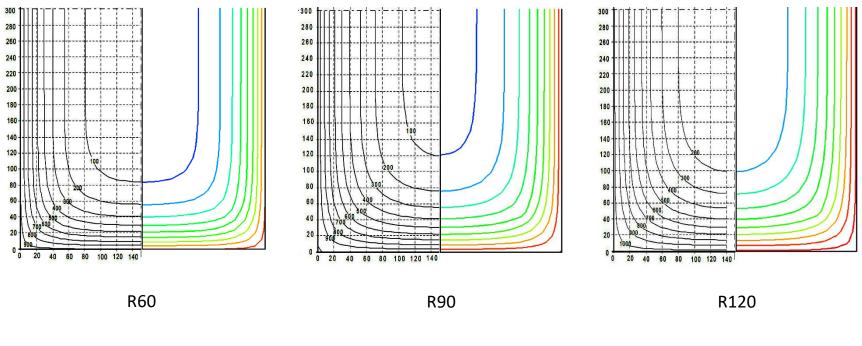
stiffness







Verification and validation of the model

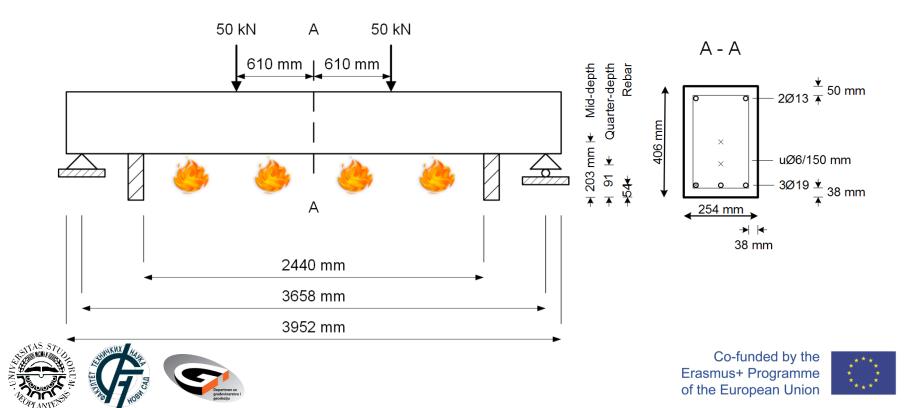




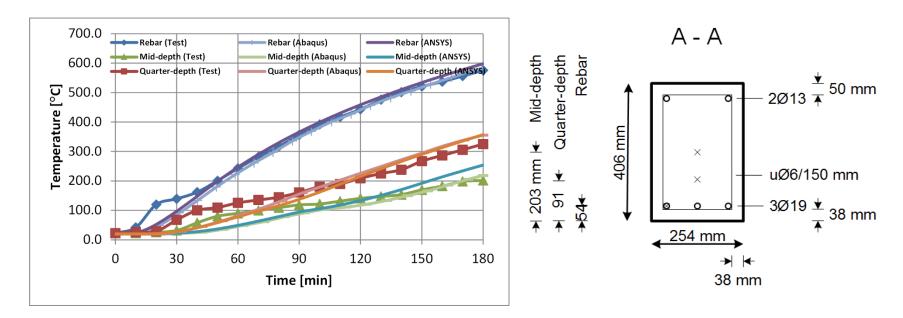




Fire test performed by Dwaikat and Kodur (2009) Numerical model in ABAQUS by Kodur and Agrawal (2016)



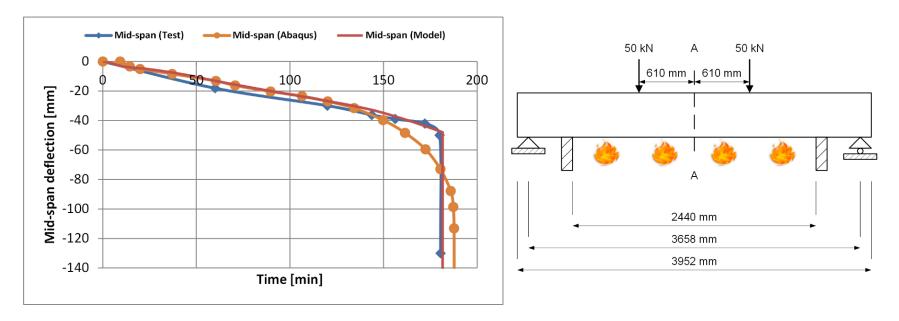
Fire test performed by Dwaikat and Kodur (2009) Numerical model in ABAQUS by Kodur and Agrawal (2016)







Fire test performed by Dwaikat and Kodur (2009) Numerical model in ABAQUS by Kodur and Agrawal (2016)

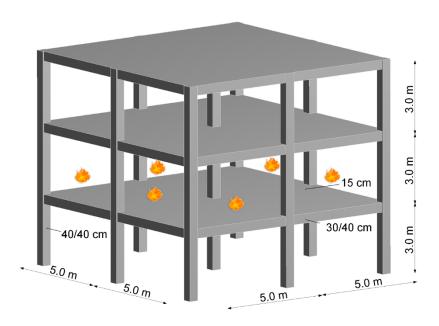






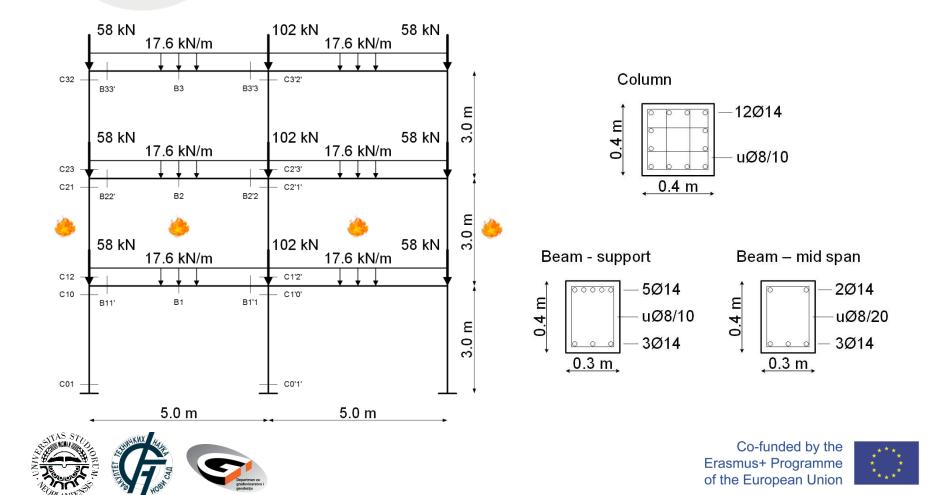
Designed according to EN 1998-1-1 DCM 0.2g PGA

- EN 1992-1-1
- EN 1998-1-1
- C 30/37
- S 500 C









	No.	Fire scenario	Load	Aggregate	Mark
 Fire scenario 1st, 2nd, 3rd storey 	1	1 st storey	50% "p"	Siliceous	P105S
_ , _ , o otore;	2			Calcareous	P105C
Aggregate type	3		80% "p"	Calcareous	P108C
 siliceous, calcareous 	4		50% "p"	Siliceous	P2O5S
Initial load level	5	2 nd storey	ου <i>ν</i> ο "μ	Calcareous	P2O5C
• 50%, 80% of Q	6		80% "p"	Calcareous	P2O8C
	7	3 rd storey	50% "p"	Siliceous	P305S
ISO 834	8		Э070 "р	Calcareous	P3O5C
	9		80% "p"	Calcareous	P308C



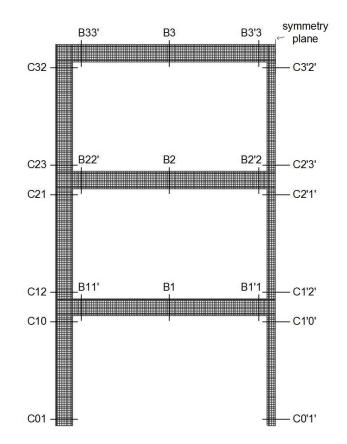


Thermal response

- Thermal profiles cross-sections
- Thermal profiles reinforcement

Structural response

- Displacements
- Axial forces / bending moments
- Stresses
- Elastic, plastic, total mechanical and thermal strains in reinforcement bars

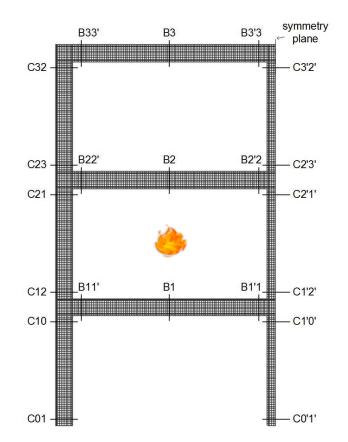


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P205S

- Fire on 2nd storey
- 50% of variable load
- Siliceous aggregate

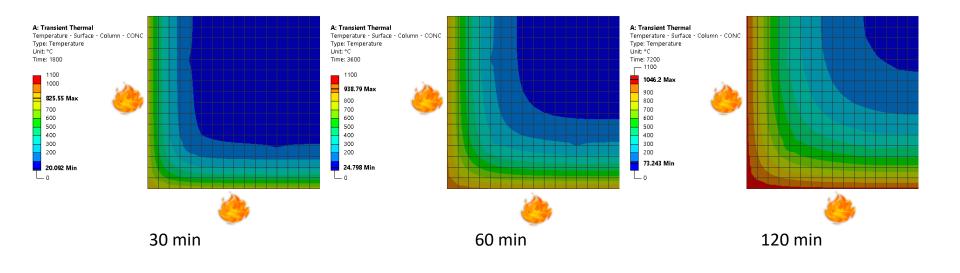








P2O5S - Thermal response - column (all surfaces exposed)

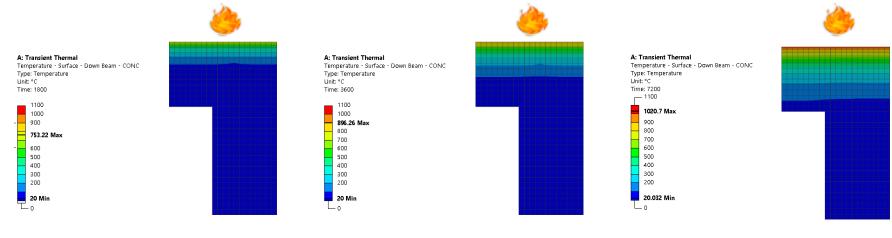


column 40/40 - 1/4 of the section





P2O5S - Thermal response - beam (top exposed)



30 min

60 min

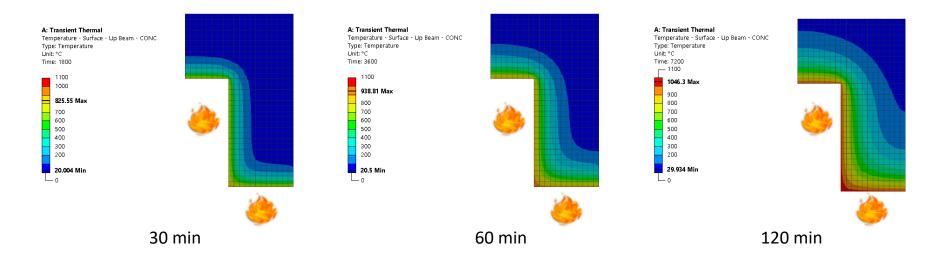
120 min

beam 30/40 - 1/2 of the section





P2O5S - Thermal response - beam (bottom/side exposed)



beam 30/40 - 1/2 of the section



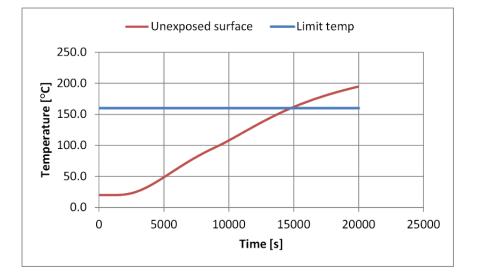


P2O5S - Insulation criteria (I)

RC slab - compartment boundary

- average temperature rise on unexposed surface < 140°C
- maximum temperature rise on unexposed surface < 180°C

RC slab d = 15 cm \rightarrow I 240







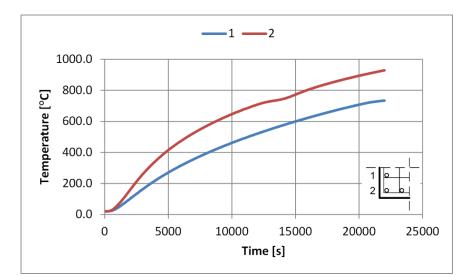
P2O5S - Thermal response of reinforcement

60 min

 concrete max temp. 940°C reinforcement max temp. 310°C

120 min

 concrete max temp. 1050°C reinforcement max temp. 540°C



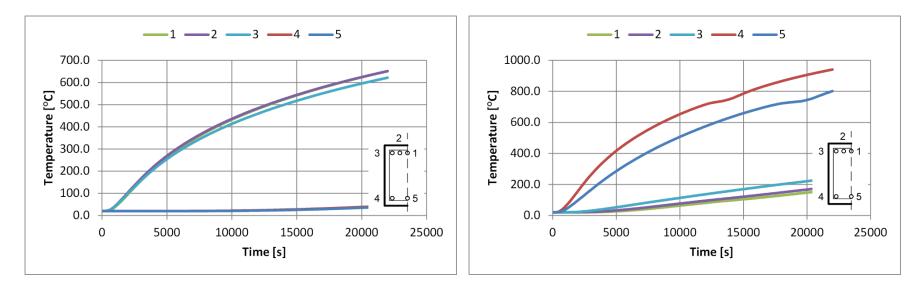
column (all surfaces exposed)







P2O5S - Thermal response of reinforcement



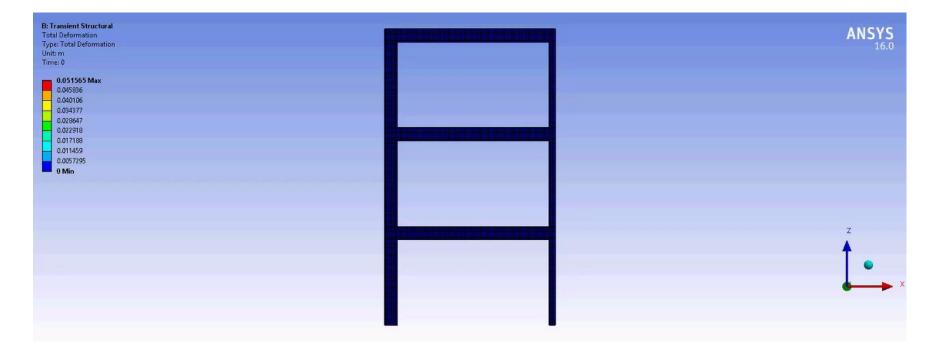
beam (top exposed)

beam (bottom/side exposed)





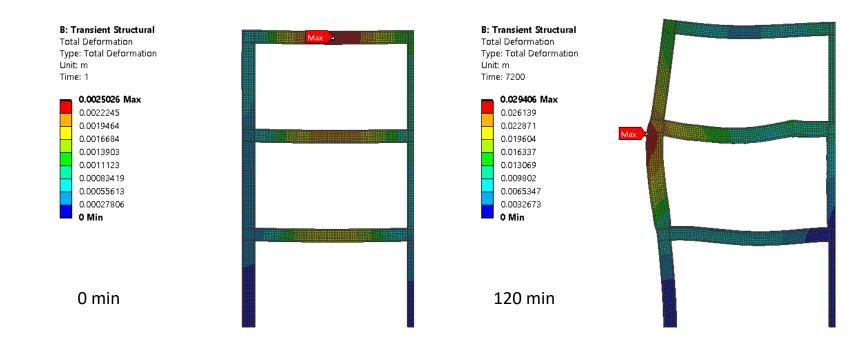
P2O5S - Structural response - Total displacements







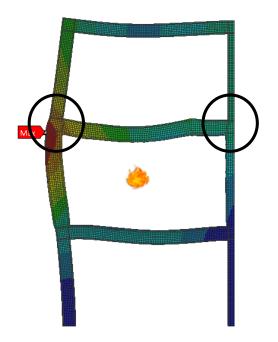
P2O5S - Structural response - Total displacements

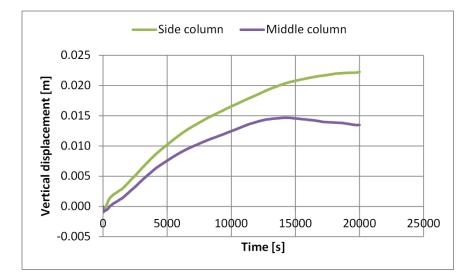






P2O5S - Structural response - Vertical displacements



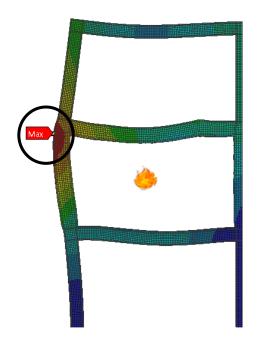


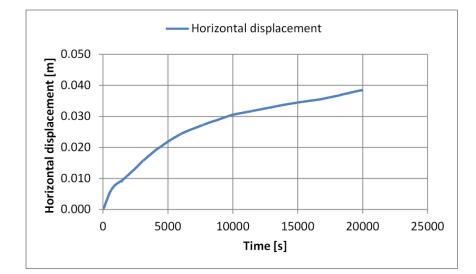
exposed column top vertical displacement





P2O5S - Structural response - Horizontal displacements





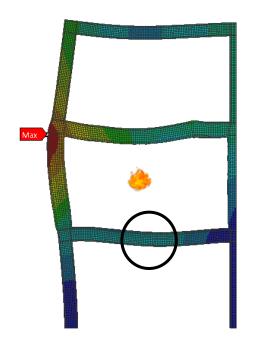
max horizontal displacement

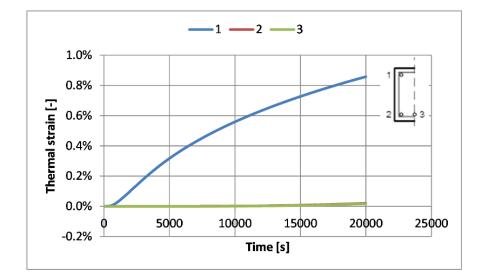






P2O5S - Structural response - Reinforcement



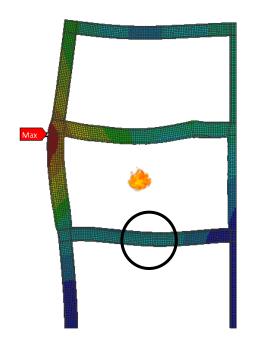


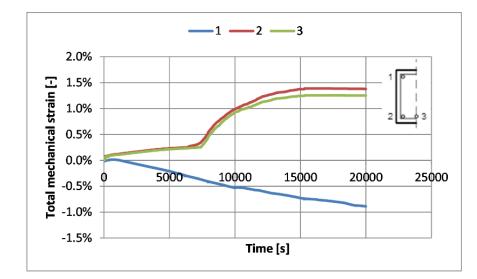
thermal strain in reinforcement bars at beam B1 mid-span





P2O5S - Structural response - Reinforcement



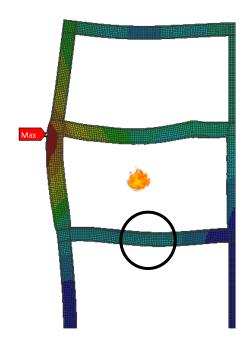


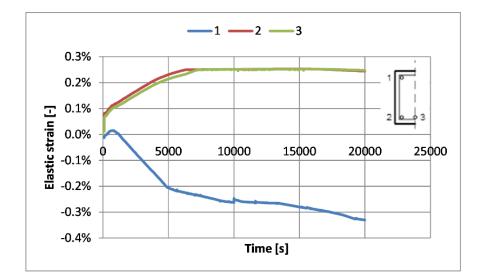
mechanical strain in reinforcement bars at beam B1 mid-span





P2O5S - Structural response - Reinforcement



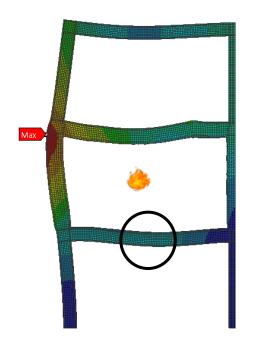


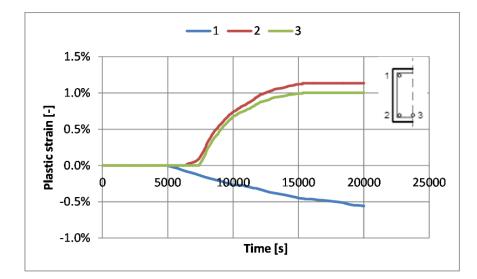
elastic strain in reinforcement bars at beam B1 mid-span





P2O5S - Structural response - Reinforcement



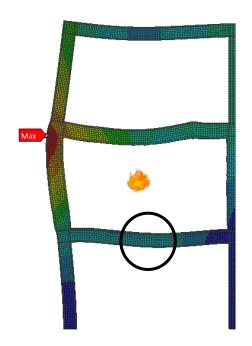


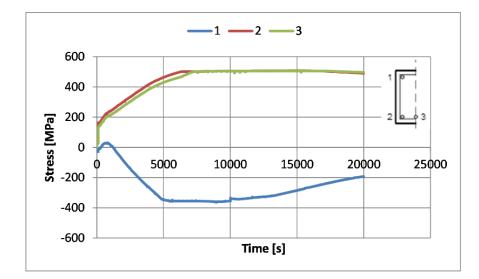
plastic strain in reinforcement bars at beam B1 mid-span





P2O5S - Structural response - Reinforcement



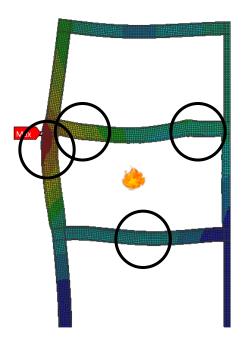


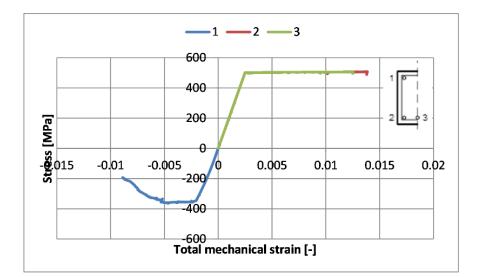
stress in reinforcement bars at beam B1 mid-span





P2O5S - Structural response - Reinforcement



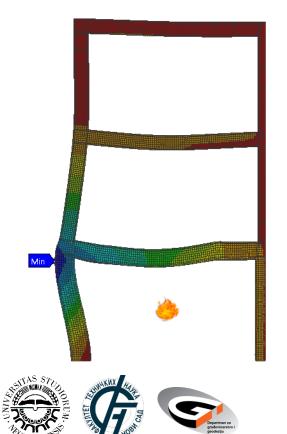


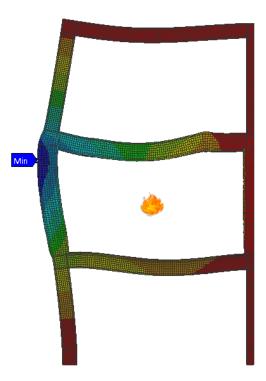
stress/strain in reinforcement bars at beam B1 mid-span

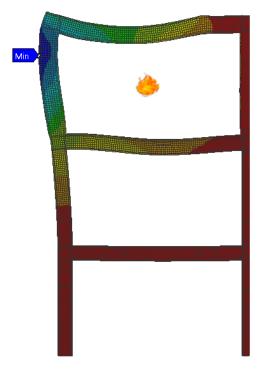




Parametric analysis - fire scenario



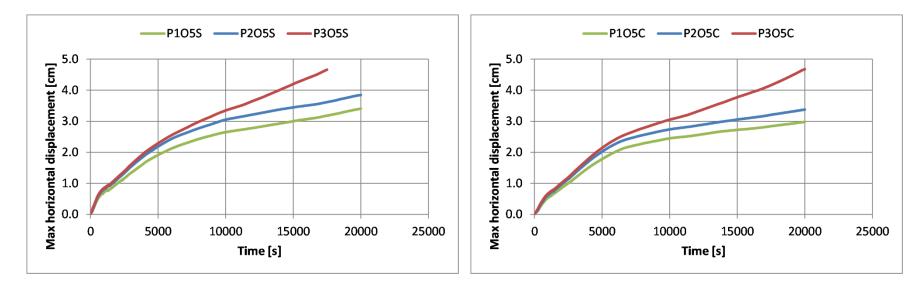




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Parametric analysis - fire scenario and aggregate type



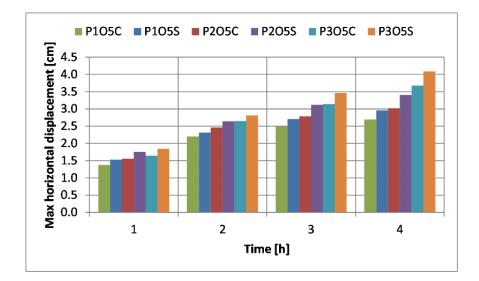
max horizontal displacements siliceous aggregate

max horizontal displacements calcareous aggregate

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Parametric analysis - fire scenario and aggregate type

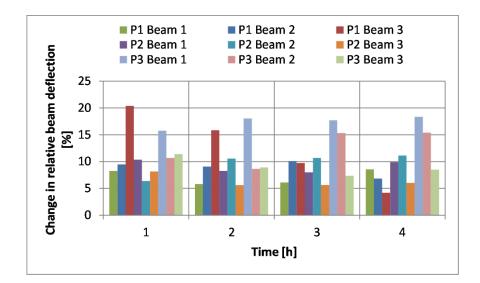


max horizontal displacements





Parametric analysis - fire scenario and variable load



change in relative beam deflections



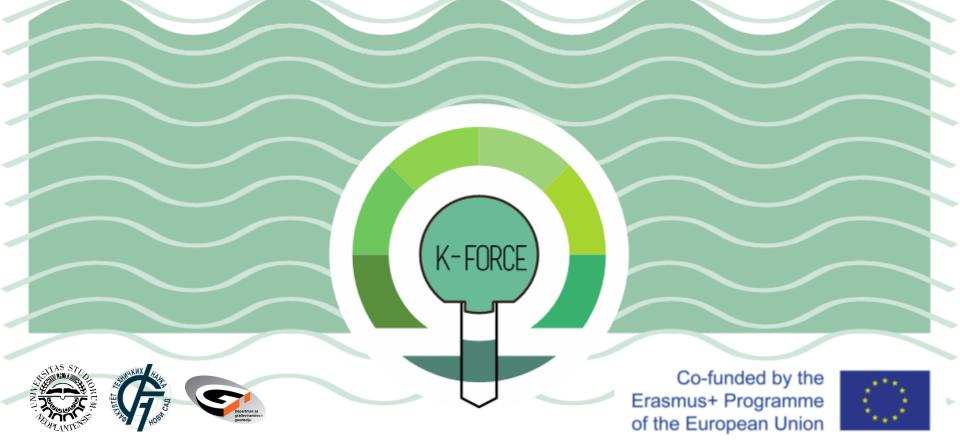


Conclusions

- Fire is an accidental action
- If not supressed, fire can initiate nonlinear inelastic structural response
- Structures need to be designed and constructed to be able to sustain certain fire resistance time
- Fire resistance can be determined by tests or by calculation methods, the latter utilizing mainly numerical methods, such as the finite element method
- Properly developed numerical models are able to assess realistic behaviour of structures exposed to fire
- RC frame structure designed according to Eurocode standards for seismically active regions has proved to be very resistant in case of fire, due to the inherent load bearing and deformation capacity reserve







Thank you for your attention *idzolev@uns.ac.rs*

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