

# SPECIAL MOBILITY STRAND

**Reliability Analysis Techniques**

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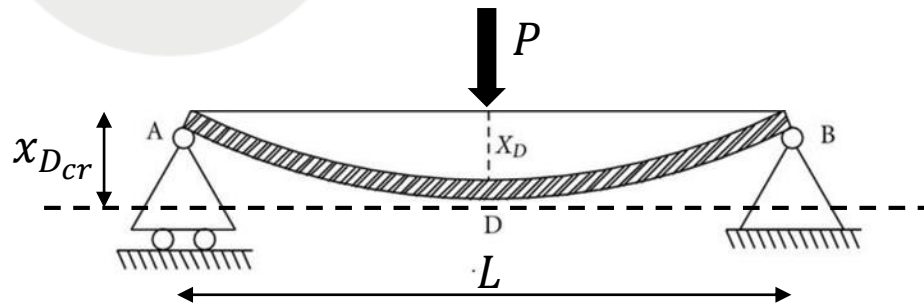
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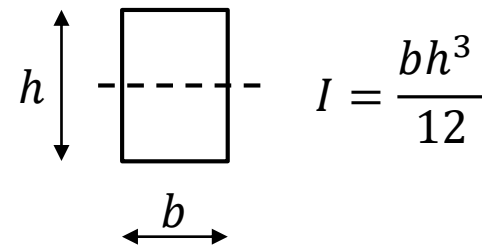
## *Presentation outline*

- *Intoduction*
  - Deterministic design*
  - Probabilistic design*
  - Variable transformation*
- *First Order Reliability Method (FORM)*
- *Second Order Reliability Method (SORM)*
- *Crude Monte Carlo Simulation (CMCS)*
- *Importance Sampling (IS)*
- *Asymptotic Samplig (AS)*





Cross section:



Known data:

$$h = 0.5$$

$$L = 15$$

$$E = 30 \cdot 10^9$$

$$x_{Dcr} = 0.03$$

$$P = 100,000$$

Limit state function

$$g = 1 - \frac{x_D}{x_{Dcr}}$$



Failure if:  $g < 0$

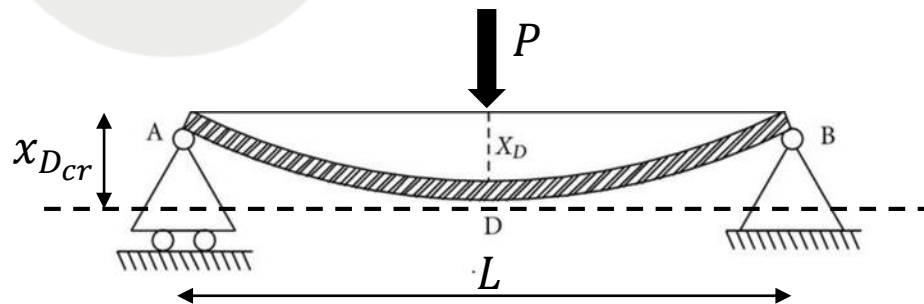
$$b = ?$$

where

$$x_D = \frac{P}{K_D} \quad \text{and} \quad K_D = \frac{48EI}{L^3}$$

then

$$g = 1 - \frac{PL^3}{4Ebh^3x_{Dcr}} > 0 \quad \Rightarrow \quad b > \frac{PL^3}{4Eh^3x_{Dcr}} = 0.22$$



Cross section:

$$I = \frac{bh^3}{12}$$

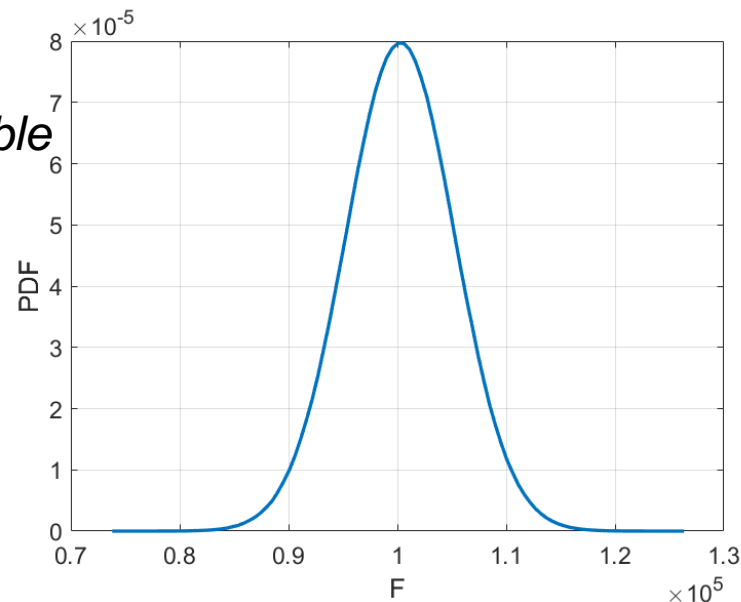
Uncertain loading:  
 $P$  is a random variable

$$P \sim N(\mu_P, \sigma_P)$$

$$\mu_P = 100,000$$

$$\sigma_P = 5,000$$

$$C.o.V. = \frac{\sigma_P}{\mu_P} = 5\%$$



It is always convenient  
to use standard normal  
random variables, i.e.:

$$P = z\sigma_P + \mu_P$$

$$z \sim N(0,1)$$

*A simple transformation from  $X_i$  to  $Z_i$  can be defined by the identity*

$$\Phi(Z_i) = F_{X_i}(X_i)$$

*where  $F_{X_i}$  is the distribution function for  $X_i$ . Given a realization  $z$  of  $Z$  a realization  $x$  of  $X$  can be determined by*

$$x_i = F_{X_i}^{-1}(\Phi(z_i))$$

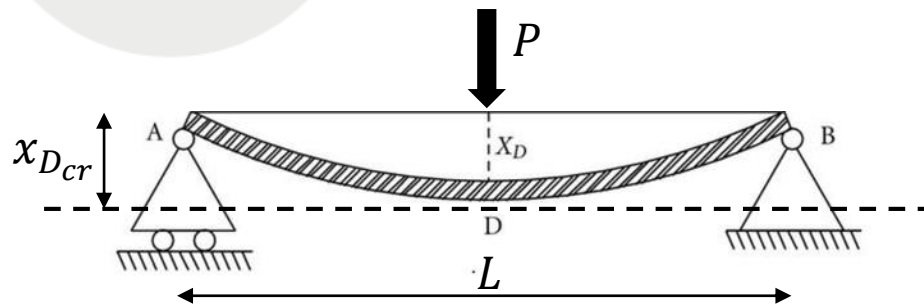
*The failure probability is given as*

$$P_F = P(g < 0) = \int_F q(\mathbf{z}) d\mathbf{z}$$

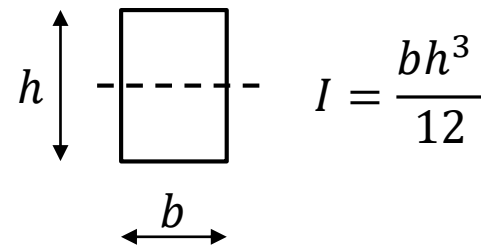
*Where  $q(\mathbf{z})$  is the joint Probability Density Function (PDF) of the random variables and*

$$F = \{\mathbf{z} : g < 0\}$$

*Denotes the “failure domain” or “failure region” which is a subset in the parameter space of  $\mathbf{z}$*



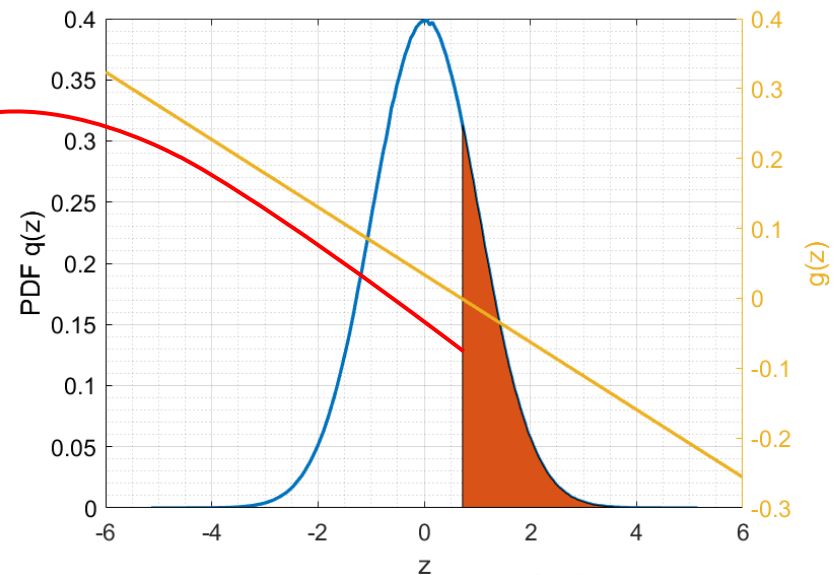
Cross section:

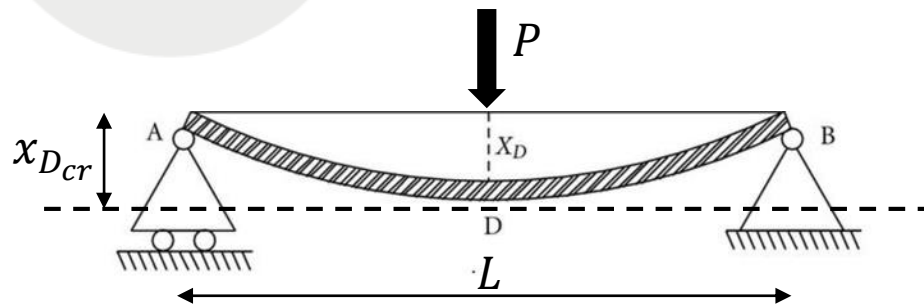


In our example, using:

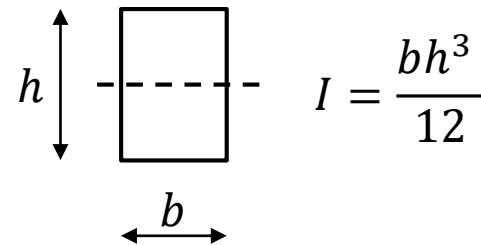
$$P_F = P(g < 0) = \int_F q(z) dz$$

For  $b = 0.23$   $\Rightarrow P_F = 0.242$





Cross section:

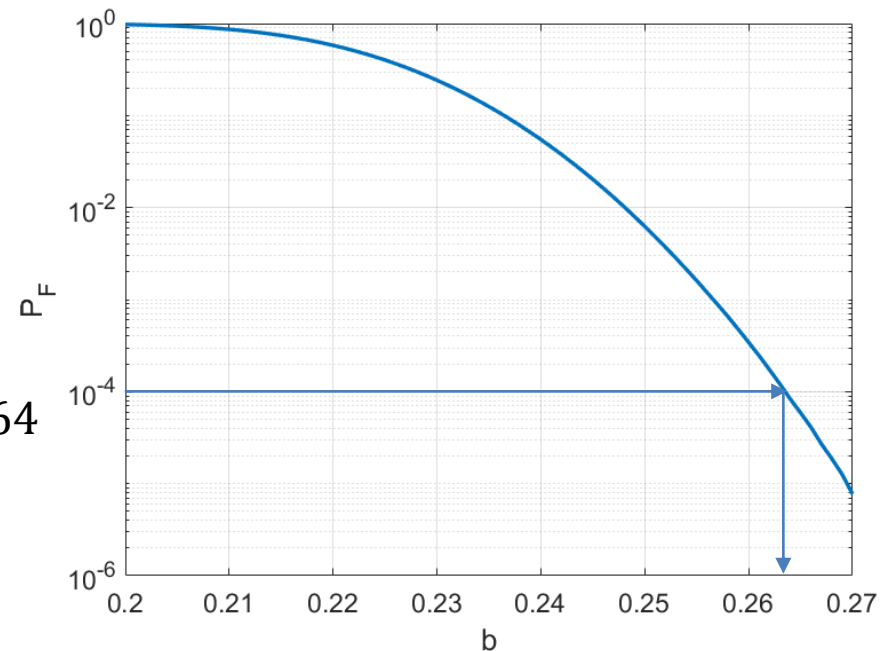


The design requirement now is the target reliability of the system

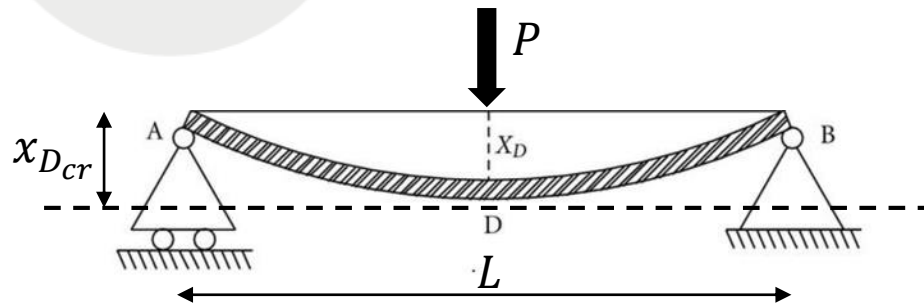
$$R^* = 1 - P_F^*$$

Or equivalently the target failure probability  $P_F^*$

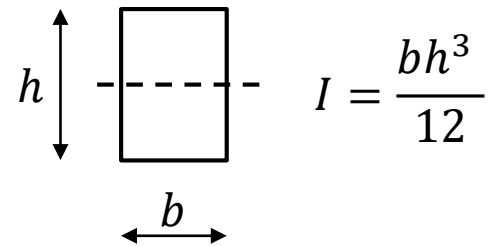
For example:  $P_F^* = 10^{-4} \Rightarrow b = 0.264$





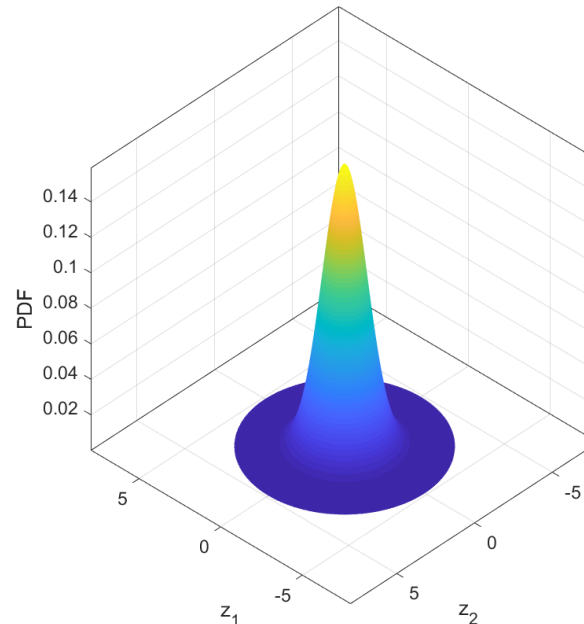


Cross section:

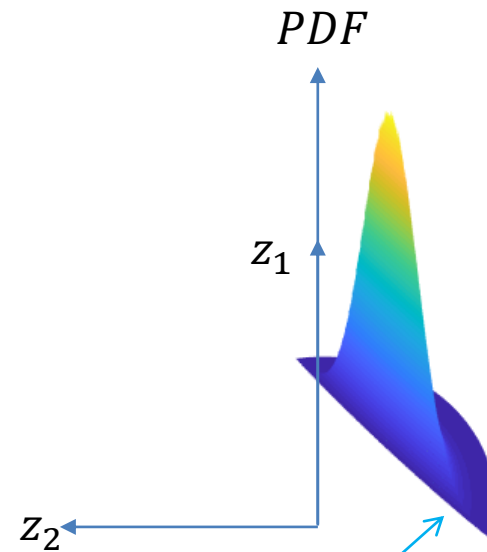
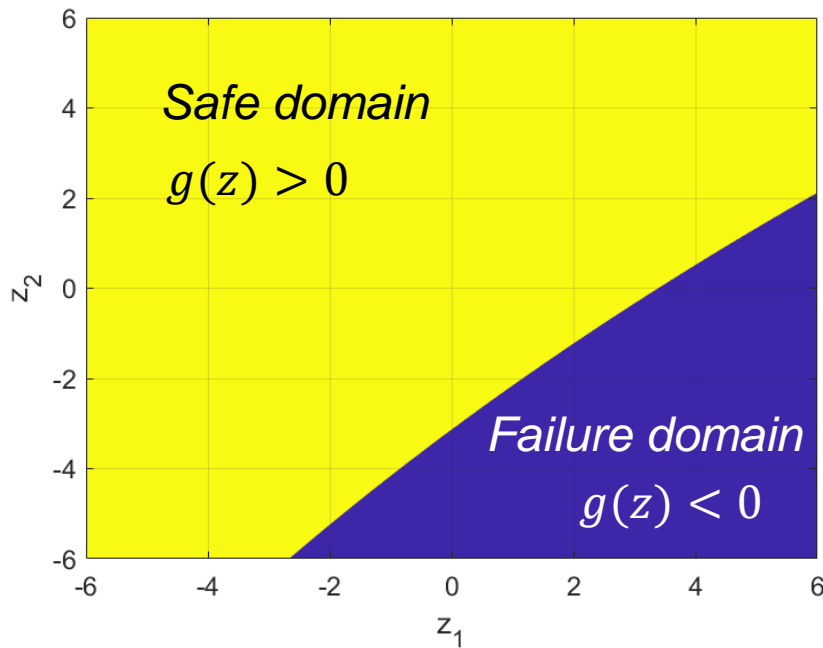


### Probabilistic Model

Random variable	Distribution	Mean value	C.o.V
$P$	Normal	100,000	5%
$E$	Normal	$30 \cdot 10^9$	2.5%



For a given value of  $b = 0.26$



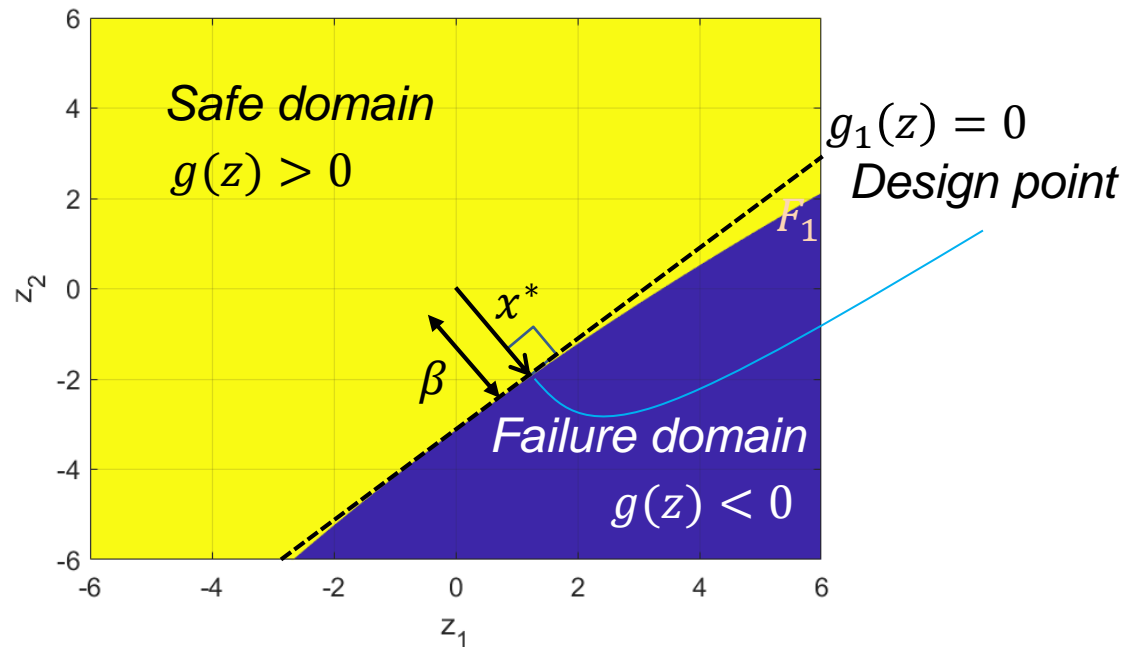
This volume represents the failure probability  $P_F$

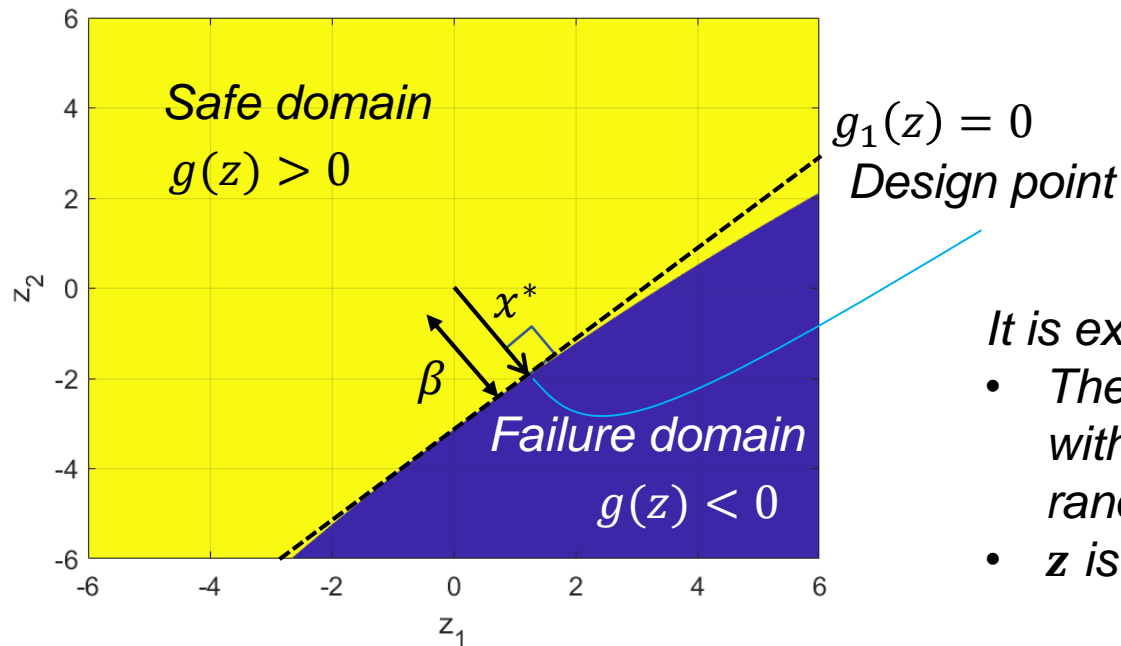
**How to calculate it?**

The failure domain is approximated by a linear half-space  $F_1$ .

The “design point” is the point in  $F_1$  with minimal distance to the origin, i.e. with minimal Euclidean norm.

The maximum of the PDF in  $F_1$  is at the design point.





The approximation is given by

$$P_F \approx \widehat{P}_F = \Phi(-\beta)$$

It is exact when:

- The limit state function is linear with respect to the vector of random variables  $z$
- $z$  is Gaussian distributed

For  $b = 0.26$ , the approximation gives

$$P_F \approx \widehat{P}_F = \Phi(-2.243) = 0.0124$$

How to determinate  $\beta$ ?

1. Guess  $\mathbf{z}^{(0)}$ . Set  $i = 0$ .

2. Calculate  $g(\mathbf{z}^{(i)})$  and  $\nabla g(\mathbf{z}^{(i)})$

3. Calculate an improved guess of  $\beta$  with

$$\mathbf{z}^{(i+1)} = \nabla g(\mathbf{z}^{(i)}) \frac{\nabla g(\mathbf{z}^{(i)})^T \mathbf{z}^{(i)} - g(\mathbf{z}^{(i)})}{\nabla g(\mathbf{z}^{(i)})^T \nabla g(\mathbf{z}^{(i)})}$$

4. Calculate

$$\beta^{(i+1)} = \sqrt{(\mathbf{z}^{(i+1)})^T \mathbf{z}^{(i+1)}}$$

5. If  $|\beta^{(i+1)} - \beta^{(i)}| < 10^{-3}$  then stop. Else  $i = i + 1$  and go to step 2.



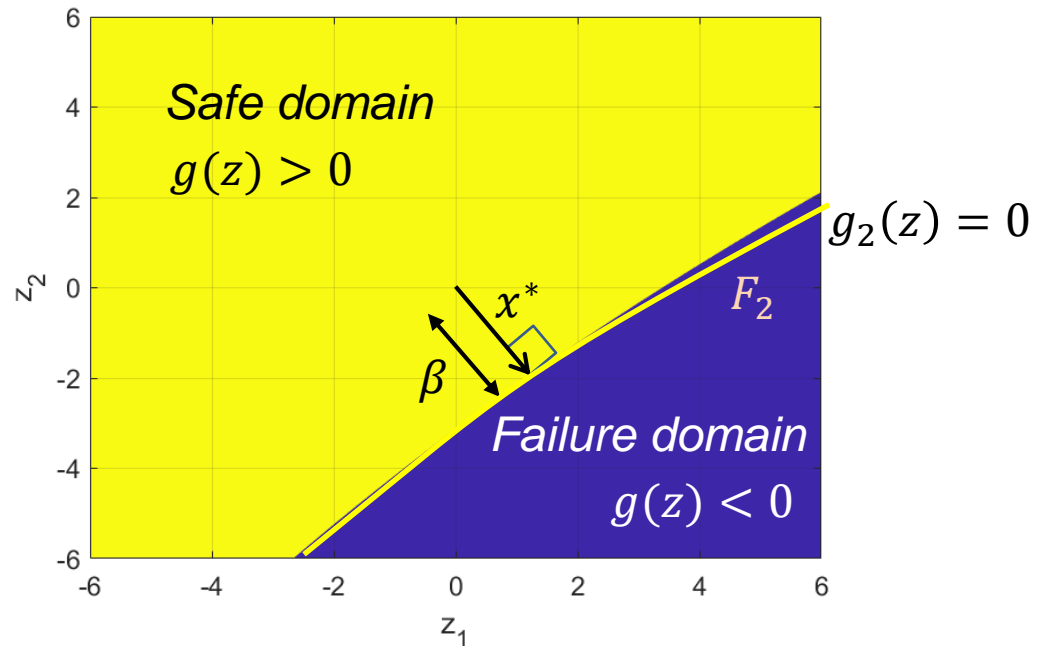
- *The estimator does not depend of the order of  $\widehat{P}_F$*
- *Under particular conditions leads to the exact solution*



- *The linearization introduce an error*
- *It is found that is not accurate in high dimensions*
- *It is necessary to find the design point*
  - *It might be expensive in high dimensions*

*It intends to improve FORM taking into account the curvature of limit state function at the design point.*

*The failure boundary is approximated by an hyper-paraboloid with limit state function  $g_2$ .*



*The SORM approximation is given by*

$$P_F \approx \widehat{P}_F = \Phi(-\beta) \prod_{i=2}^n (1 + c_i \beta)^{-\frac{1}{2}}, \quad \beta \rightarrow \infty$$

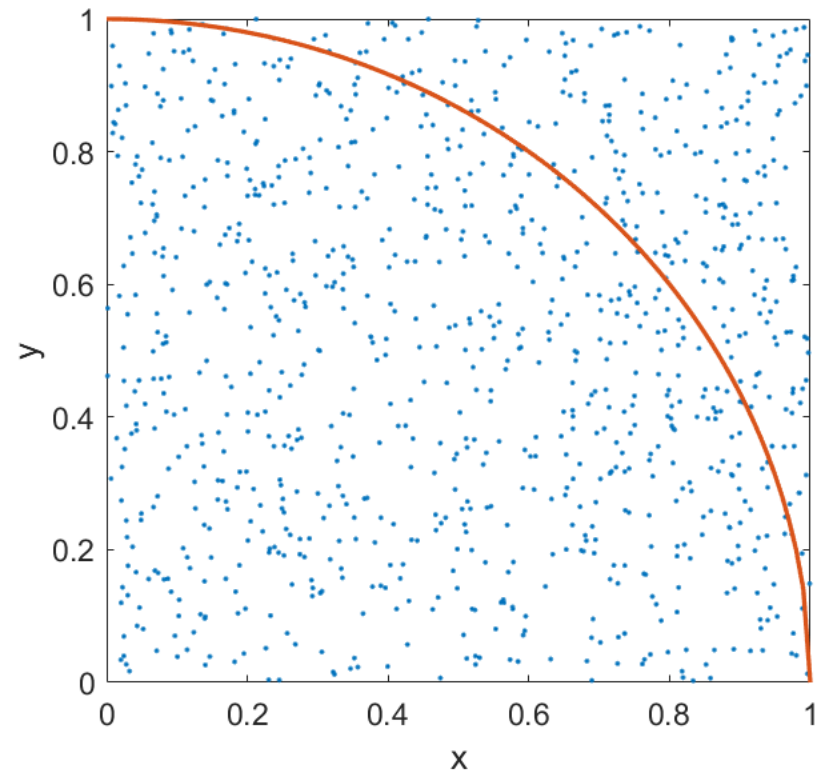
*Where  $c_i$ ,  $i = 2, \dots, n$  are the principal curvatures of the paraboloid at the design point.*

*It is also assumed that  $-c_i < 1/\beta$  for all  $i = 2, \dots, n$*

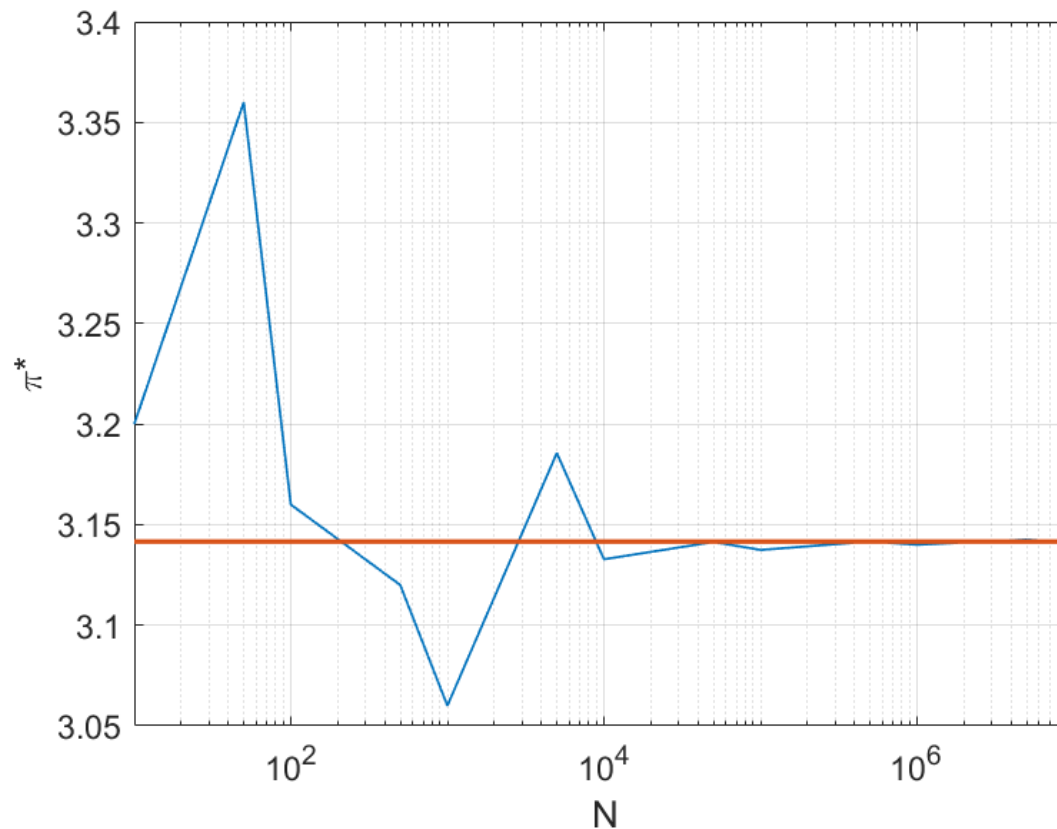


*How to calculate the area of a circle?  
And implicitly  $\pi$ ?*

- *Simulate  $N$  random numbers into a unit square with area  $A = 1$*
- *Draw a  $\frac{1}{4}$  of a unit-radius circle with area  $A_1 = \pi/4$*
- *Count the points inside the circle  $N_1$*
- *The ratio  $\frac{A_1}{A} = \frac{N_1}{N}$*

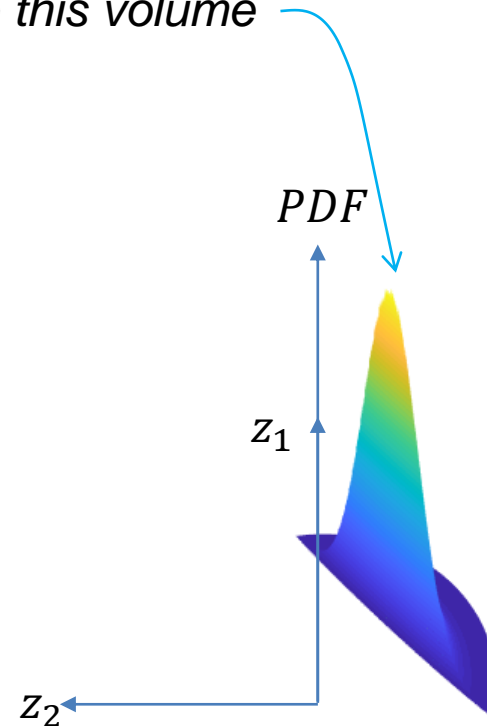


*How is affected the estimation of  $\pi \approx \pi^*$  by the number of simulations?*



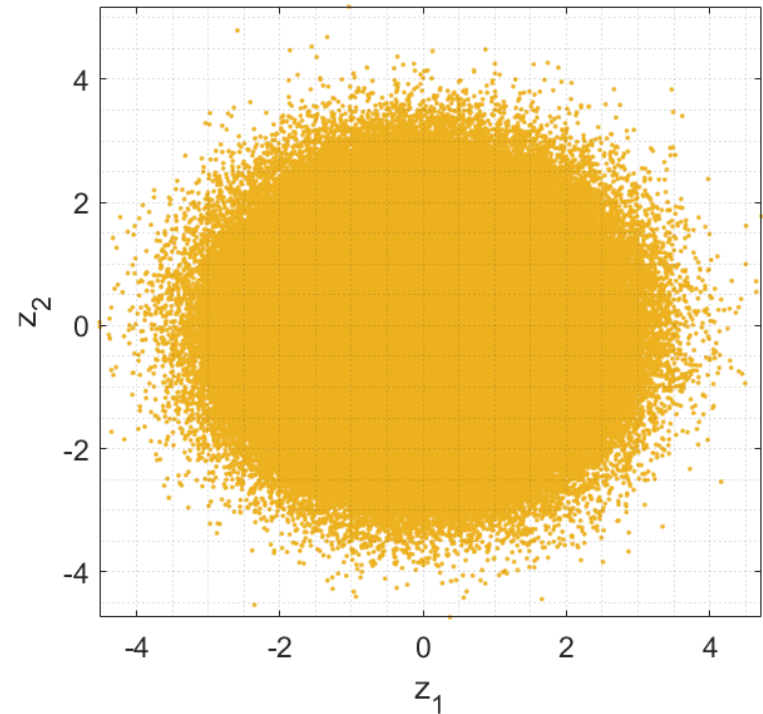
*We can use the same approach to calculate this volume*

- *A large number  $N$  of realizations  $\hat{\mathbf{z}}$  of basic random variables is simulated using  $q(\mathbf{z})$*
- *The failure probability estimator  $\widehat{P}_F$  is obtained by counting the number of realizations in the failure domain*



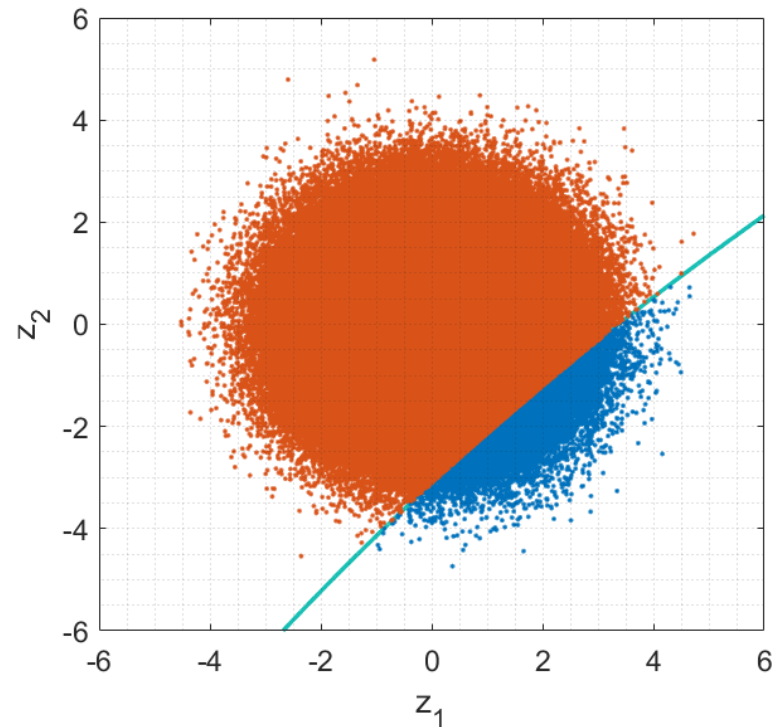
### Procedure

- *$N$  realizations of standard normal random variables are simulated*
  - *This is the only step where the information regarding the distribution of the random variables is included*



### Procedure

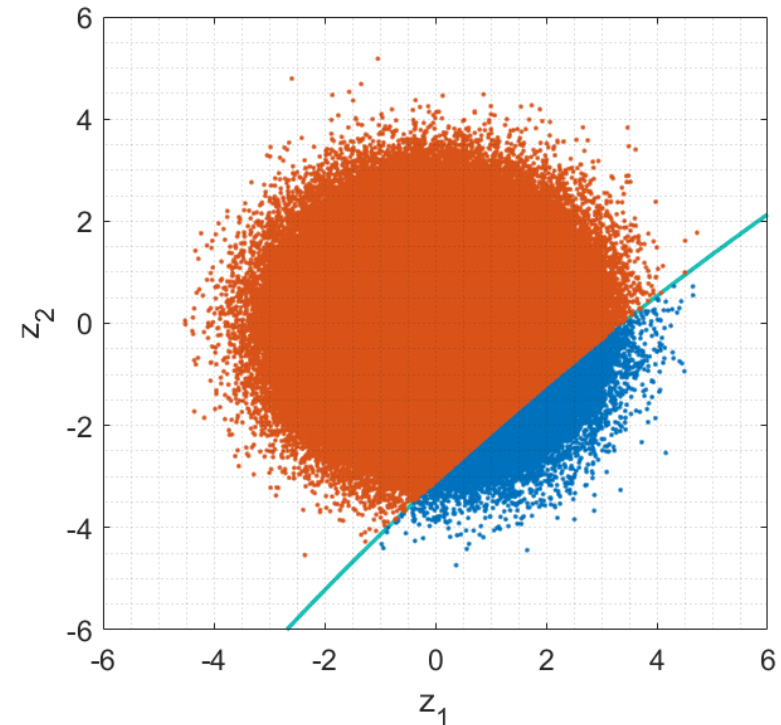
1.  *$N$  realizations of standard normal random variables are simulated*
  - *This is the only step where the information regarding the distribution of the random variables is included*
2. *Identify the number  $N_1$  of realizations in the failure domain*
  - *This is the only step where the information regarding the limit state function is included*



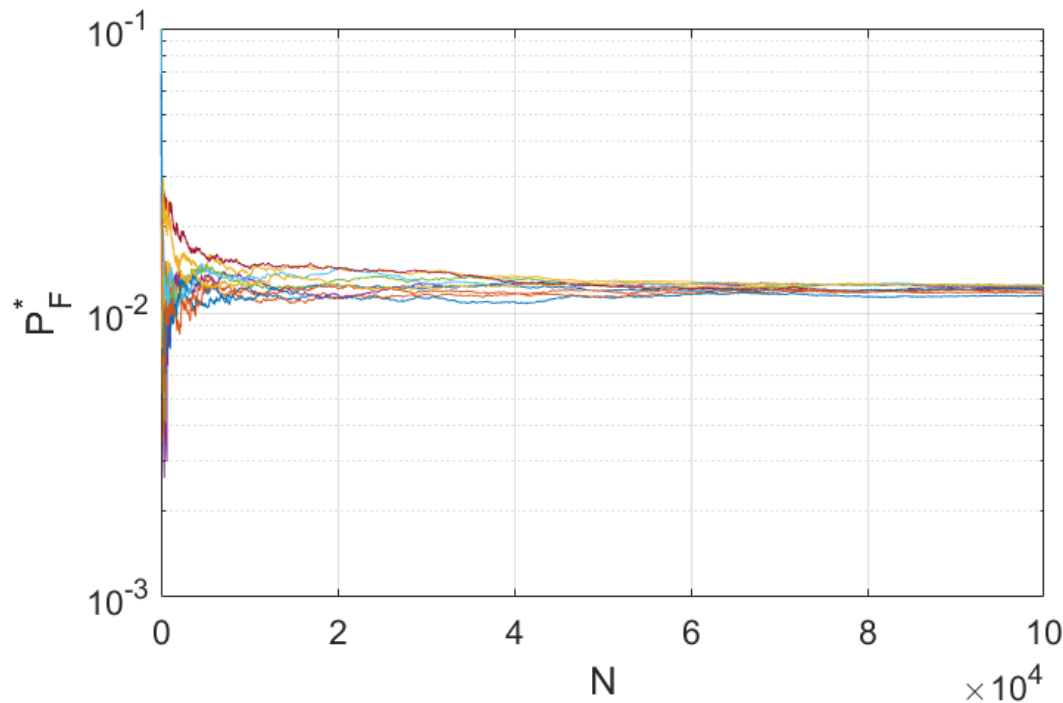
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1. *N* realizations of standard normal random variables are simulated
  - This is the only step where the information regarding the distribution of the random variables is included
2. Identify the number  $N_1$  of realizations in the failure domain
  - This is the only step where the information regarding the limit state function is included
3. The estimator is given by

$$\widehat{P}_F = \frac{N_1}{N}$$



In our example, using  $b = 0.26$ , how  $N$  affects the variability of the estimator  $\widehat{P}_F$ ?

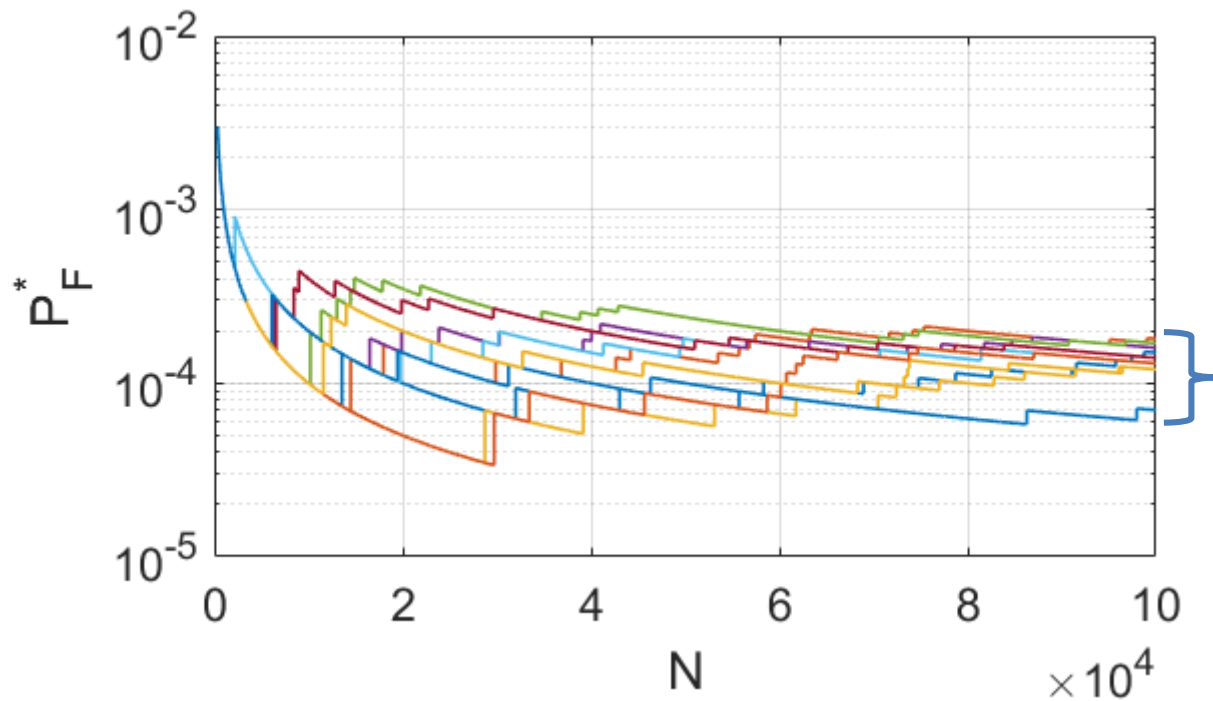


$$C.o.V(\widehat{P}_F) = \sqrt{\frac{1 - \widehat{P}_F}{N}}$$

If  $\widehat{P}_F = 0.0124$  then

$N$	$C.o.V(\widehat{P}_F)$
10	282%
100	89%
1,000	28%
10,000	9%
100,000	3%

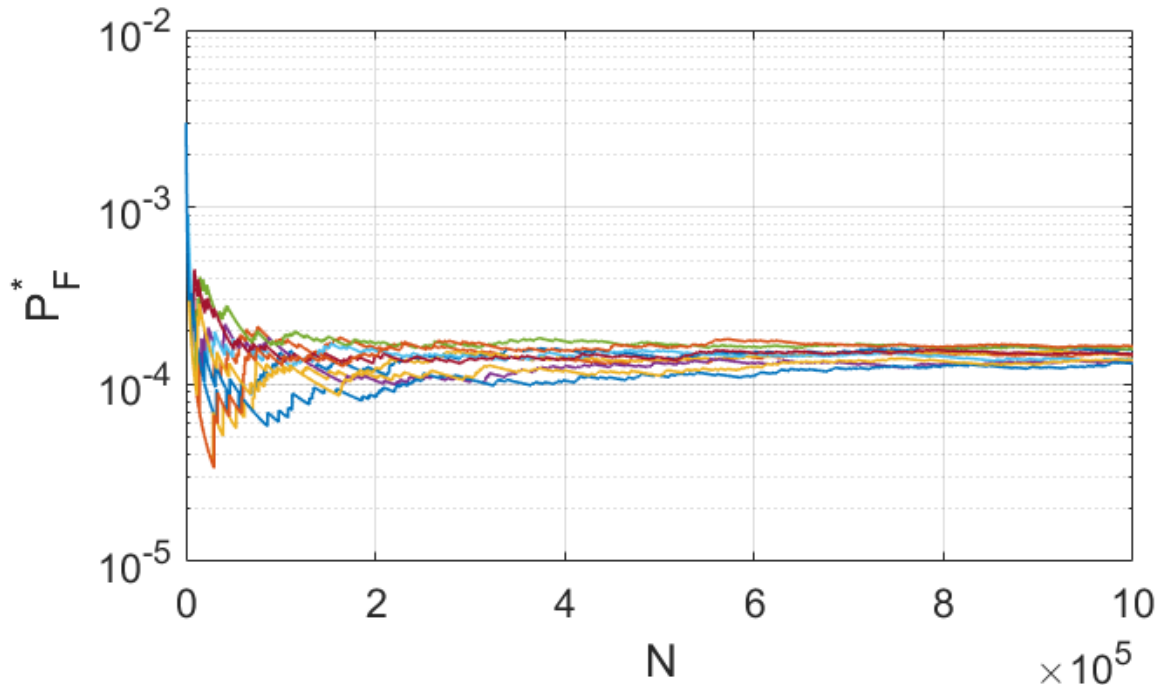
In our example, using  $b = 0.285$ , i.e.  $\widehat{P}_F = 1.5 \times 10^{-4}$ . How  $\widehat{P}_F$  affects  $C.o.V(\widehat{P}_F)$ ?



*It seems that there is not enough accuracy*



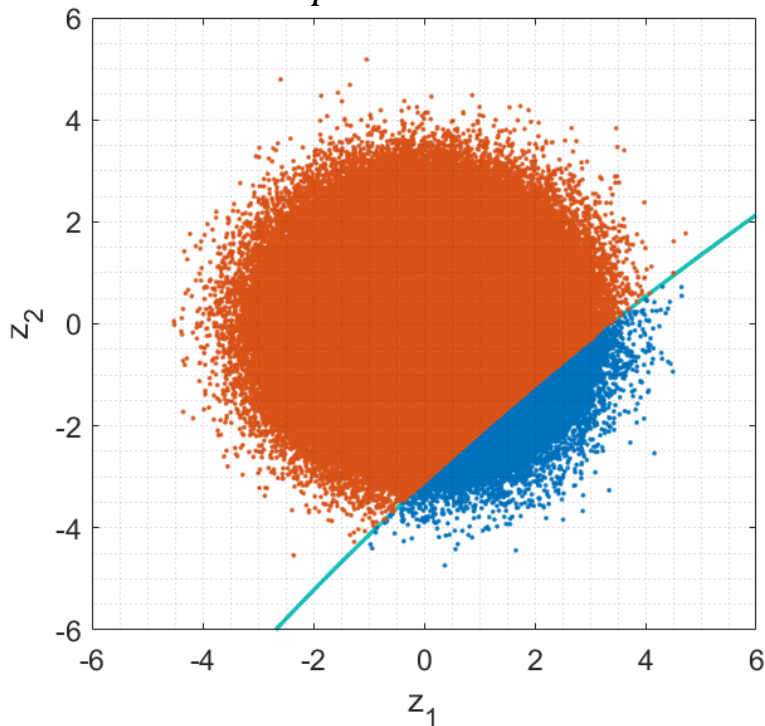
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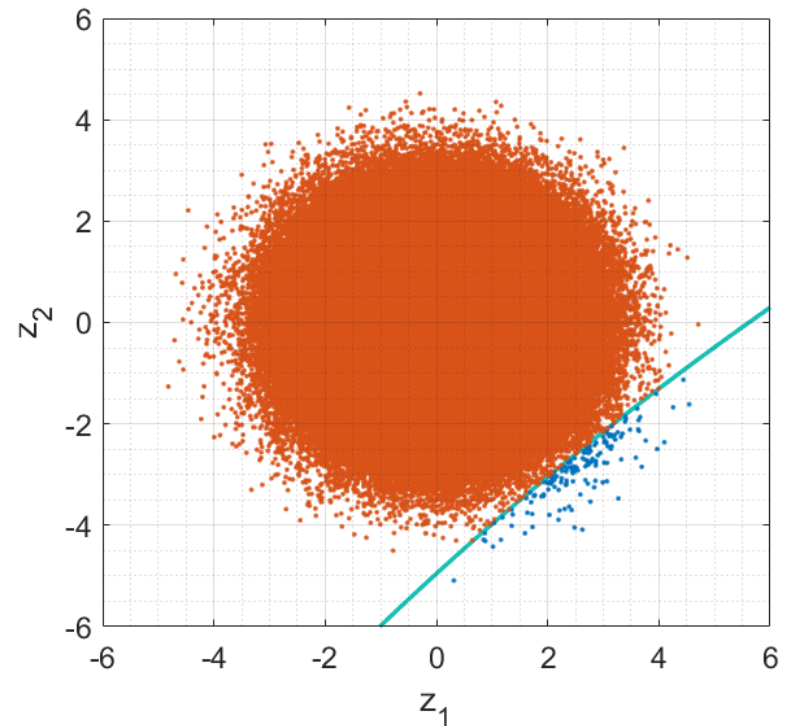
$N$	$C.o.V(\widehat{P}_F)$
10	2581%
100	816%
1,000	258%
10,000	82%
100,000	26%
1,000,000	8% ✓

$C.o.V(\widehat{P}_F) < 10\%$  is normally accepted

$$b = 0.260$$
$$\widehat{P}_F = 1.24 \times 10^{-2}$$



$$b = 0.285$$
$$\widehat{P}_F = 1.5 \times 10^{-4}$$



*When the limit state function is far from the origin is more difficult to obtain realizations in the failure domain*



- Independent of the *number* of *random variables*
- Independent of the *shape* of the *limit state function*
- The estimator is unbiased



- The number of samples required is proportional to  $1/P_F$

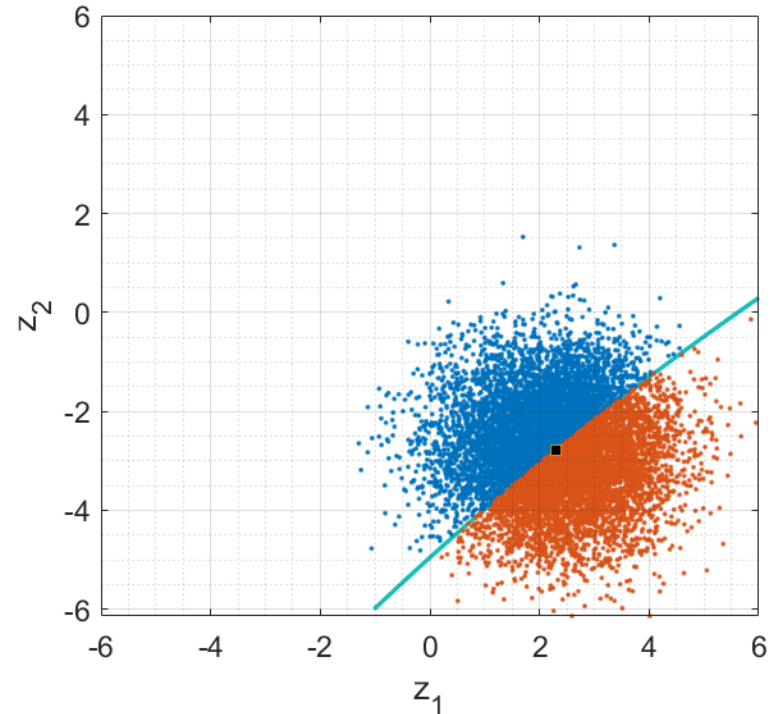
*The idea is to concentrate the realizations in an area with large contribution to  $\widehat{P}_F$*

$$P_F = \int_{g < 0} q(\mathbf{z}) d\mathbf{z} = \int_{g < 0} \frac{q(\mathbf{z})}{p(\mathbf{z})} p(\mathbf{z}) d\mathbf{z}$$

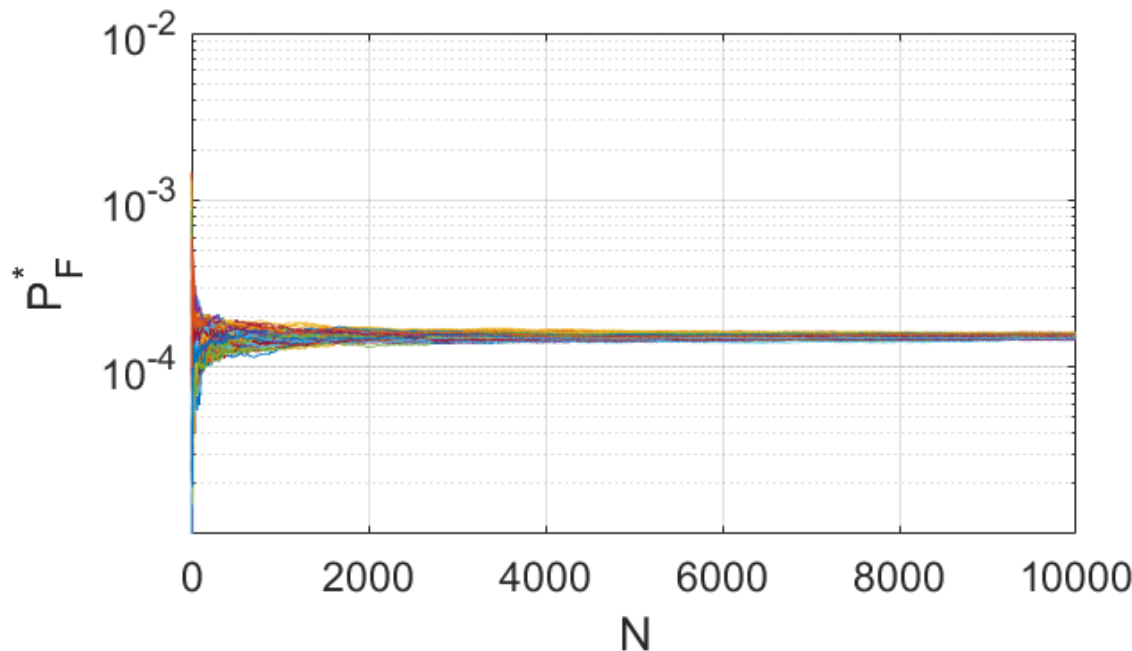
*Then, the estimator is given by*

$$\widehat{P}_F = \frac{1}{N} \sum_{k=1}^N \frac{q(\mathbf{z}'_k)}{p(\mathbf{z}'_k)} I(\mathbf{z}'_k \in F)$$

*Where  $\{\mathbf{z}'_k: k = 1, \dots, N\}$  are now samples drawn from  $p$  instead of  $q$*



In our example, using  $b = 0.285$ , i.e.  $\hat{P}_F = 1.5 \times 10^{-4}$ . How  $N$  affects the variability of the estimator  $\hat{P}_F$ ?



$N$	$C.o.V(\hat{P}_F)$ MCS	$C.o.V(\hat{P}_F)$ IS
10	2581%	65%
100	816%	19%
1,000	258%	7% ✓
10,000	82%	2% ✓

With 1,000 samples achieves the same accuracy than 1,000,000 samples using CMCS



- *Reduce dramatically the number of samples required by using CMCS*



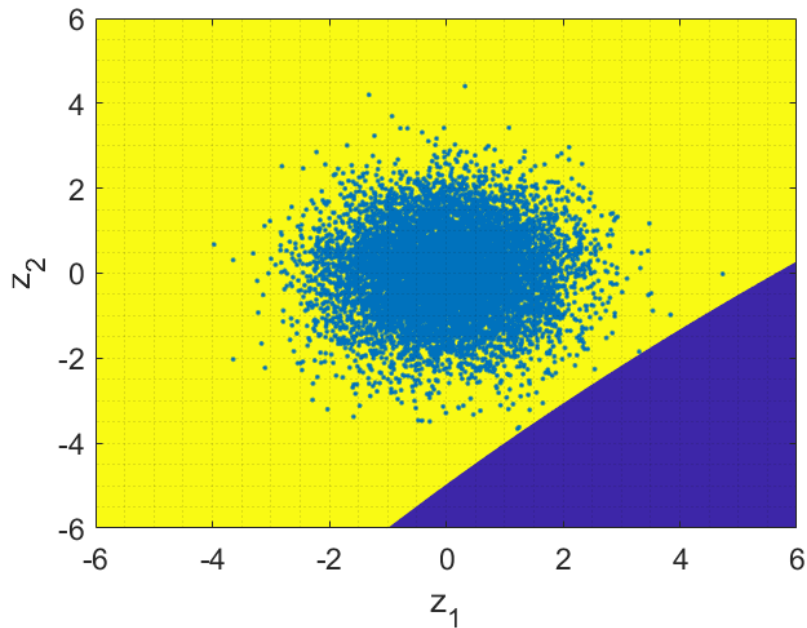
- *An incorrect selection of the importance sampling density function can lead to erroneous estimates of the reliability*

*The idea is to use asymptotic properties with a simple regression technique*

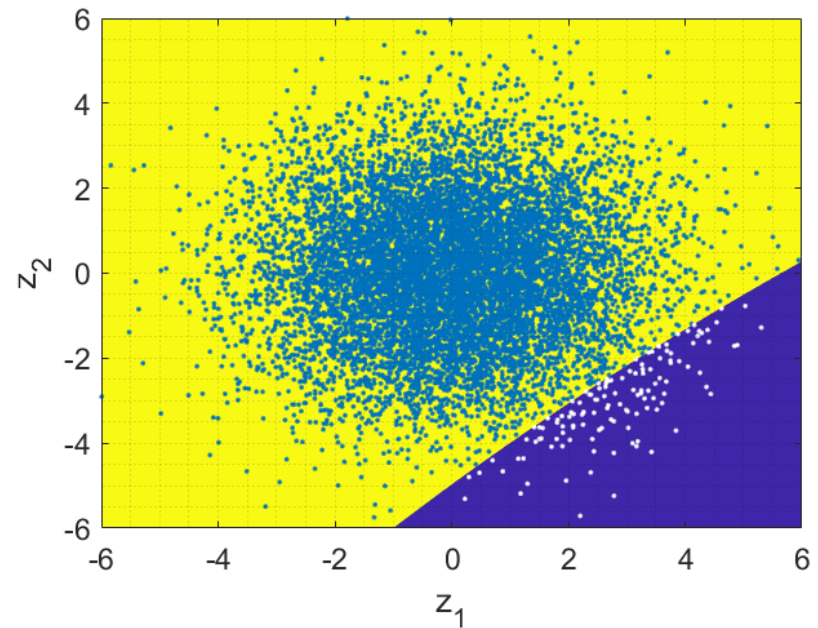
- CMCS is used to estimate the failure probability in each support point*
- The standard deviation for each support point is increased by a factor  $\frac{1}{f}$*
- Due to the larger standard deviation the failure probability is increased reducing the computational cost*
- The functional form is given by*

$$\beta(f) = A \cdot f + \frac{B}{f^c}$$

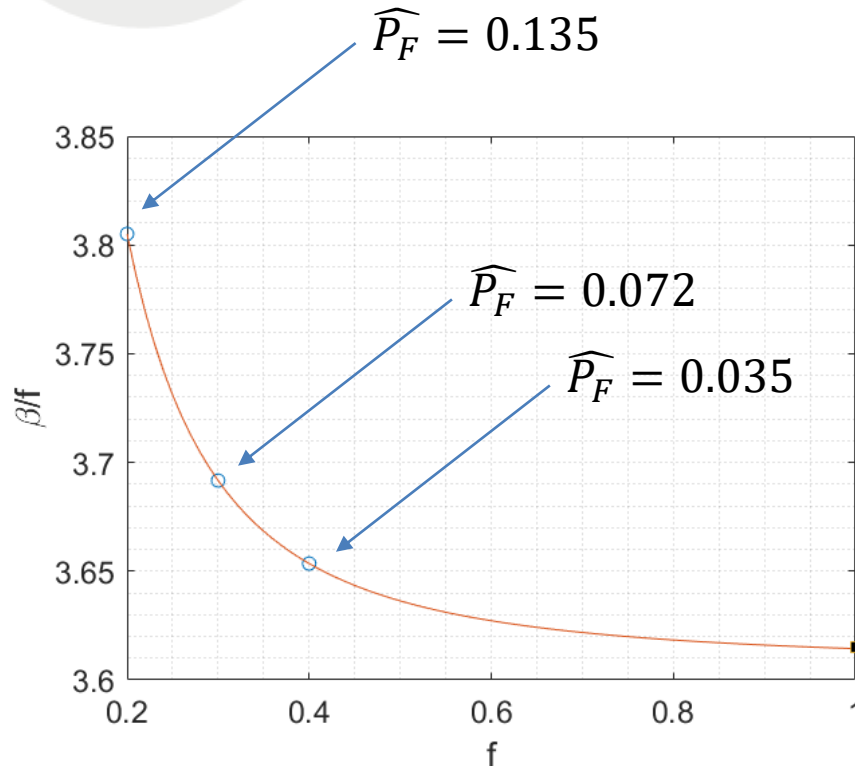
$f = 1$



$f = 0.6$







*The failure probabilities are much larger than the original implying a lower computational cost*

*Performing a regression, the following parameters are estimated*

$$A = 3.6078$$

$$B = 0.0066$$

$$C = 2.1087$$

*Then the functional form*

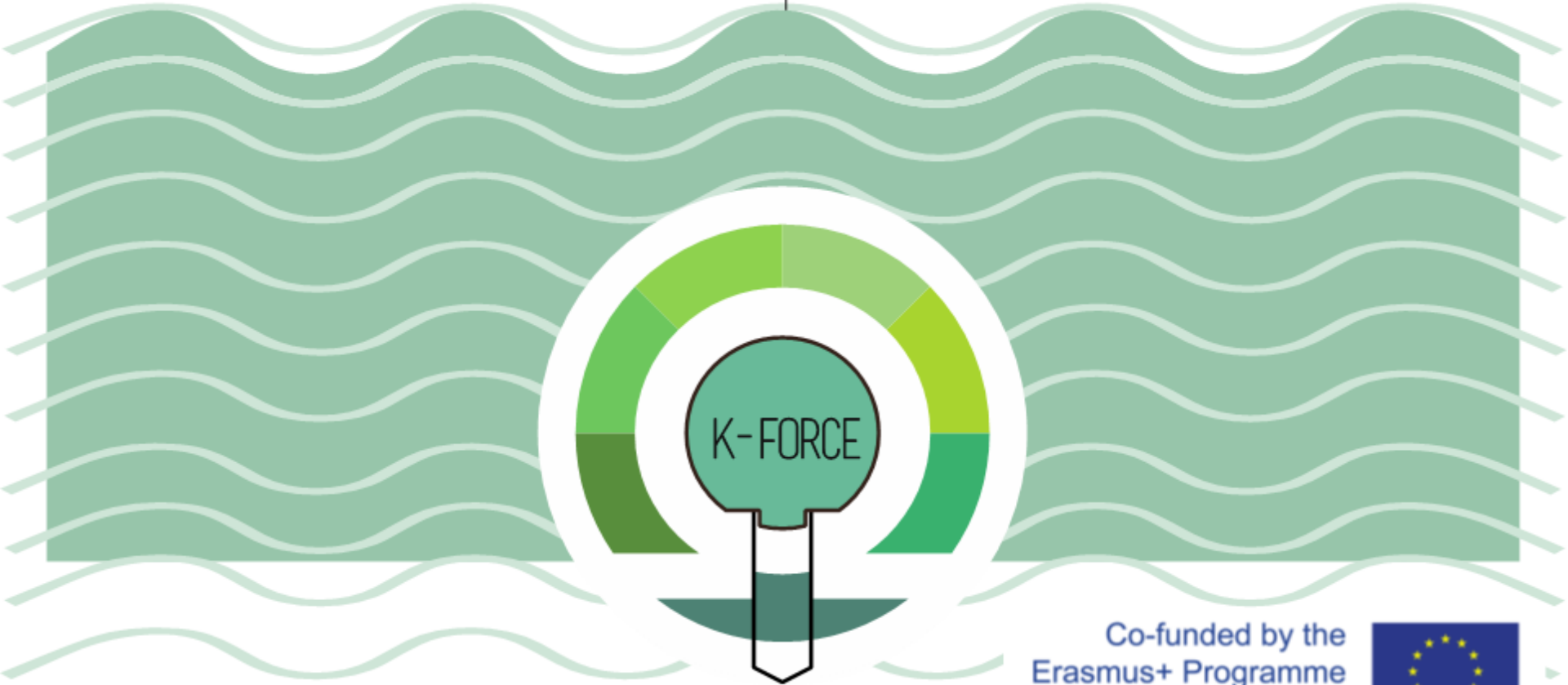
$$\beta(f) = A \cdot f + \frac{B}{f^C}$$

*Is evaluated for  $f=1$*

$$\beta(1) = 3.61$$

*And then the estimator is given by*

$$\widehat{P}_F = \Phi(-\beta(1)) = 1.5 \times 10^{-4}$$



Thank you  
for your attention  
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**Knowledge FOR Resilient soCiEty**