



## **SPECIAL MOBILITY STRAND**

### **SYSTEM IDENTIFICATION OF BRIDGES USING AMBIENT VIBRATION MEASUREMENTS AND NUMERICAL SIMULATIONS**

**(CASE STUDIES)**

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**Tirana, April 2019**

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## ***CASE STUDY 1 – THE BRIDGE OVER RIVER BOSNIA IN SARAJEVO***

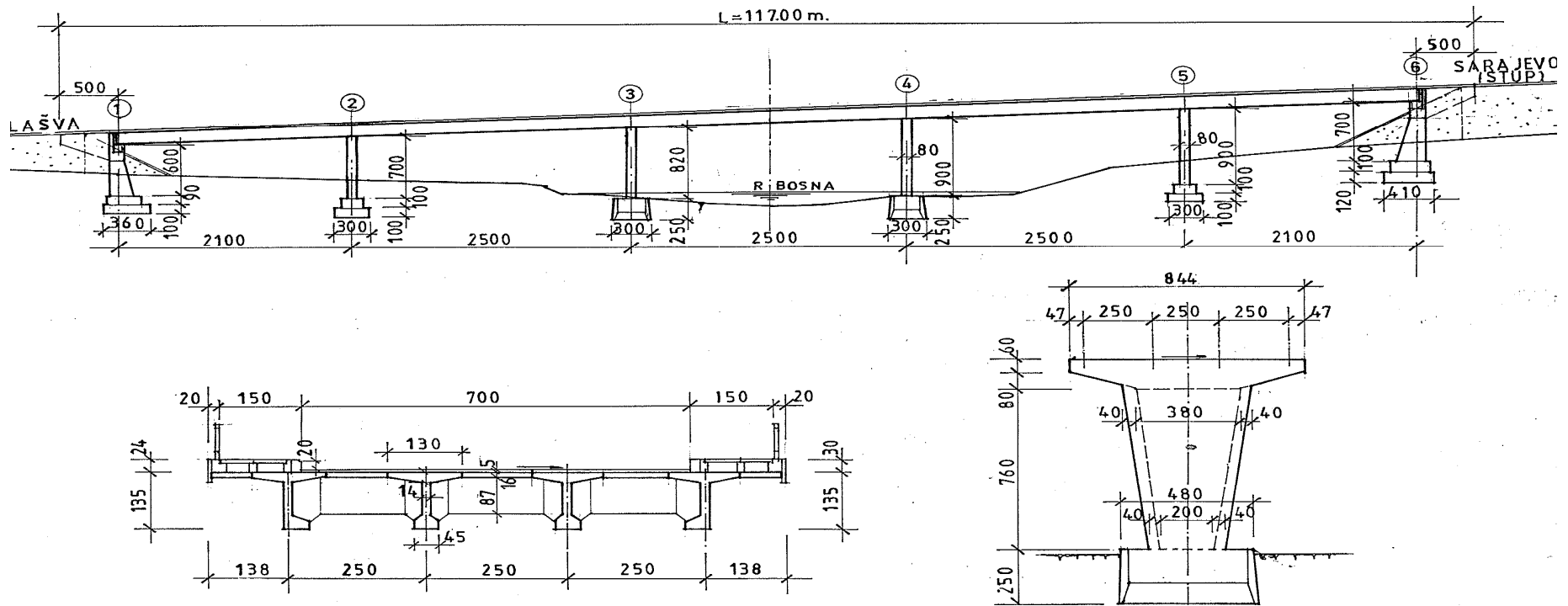


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## Elevation and cross-sections of the bridge



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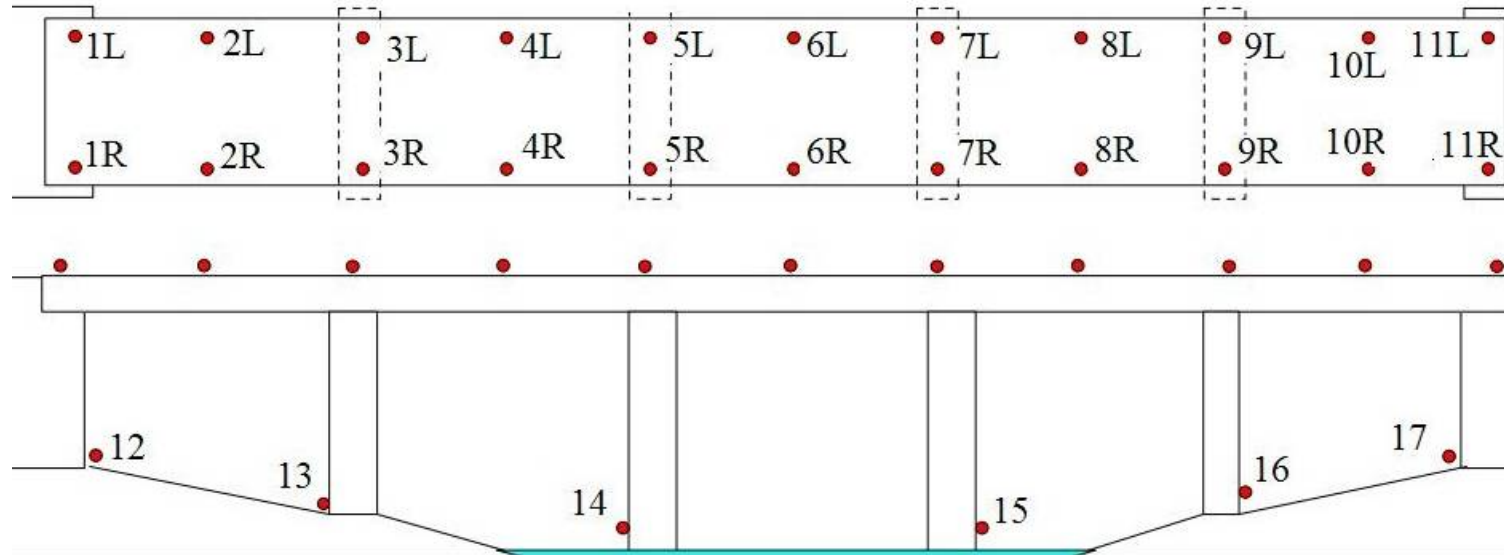


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## Measurements setup



Setup	Moveable stations	Base stations
M1	4R, 5R, 7R, 8R	6R
M2	2R, 3R, 9R, 10R	6R
M3	1R, 2R, 10R, 11R	6R
M4	4L, 5L, 6L, 7L	6R
M5	3L, 4L, 8L, 9L	6R
M6	1L, 2L, 10L, 11L	6R
M7	12, 13, 16, 17	6R
M8	12, 13, 16, 17	6R



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## Test equipment



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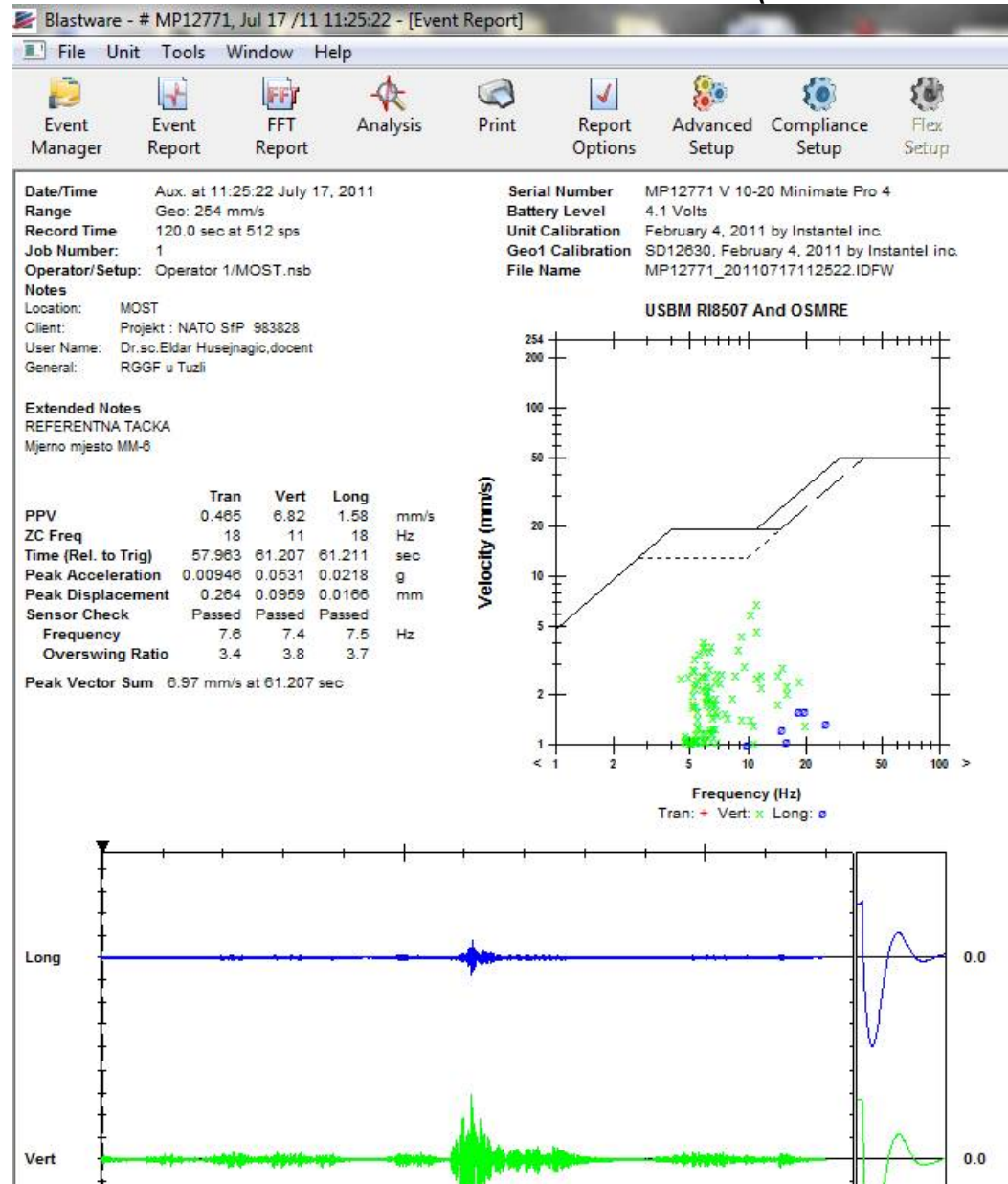


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# Measurement on base station 6R (middle of the span)



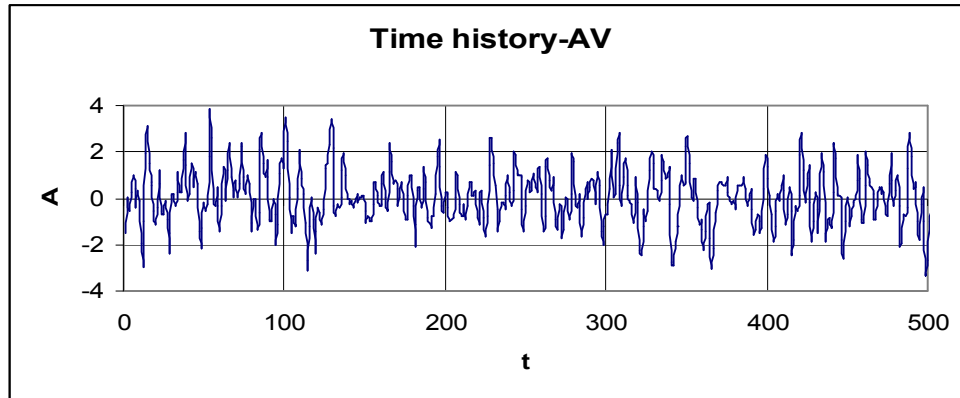
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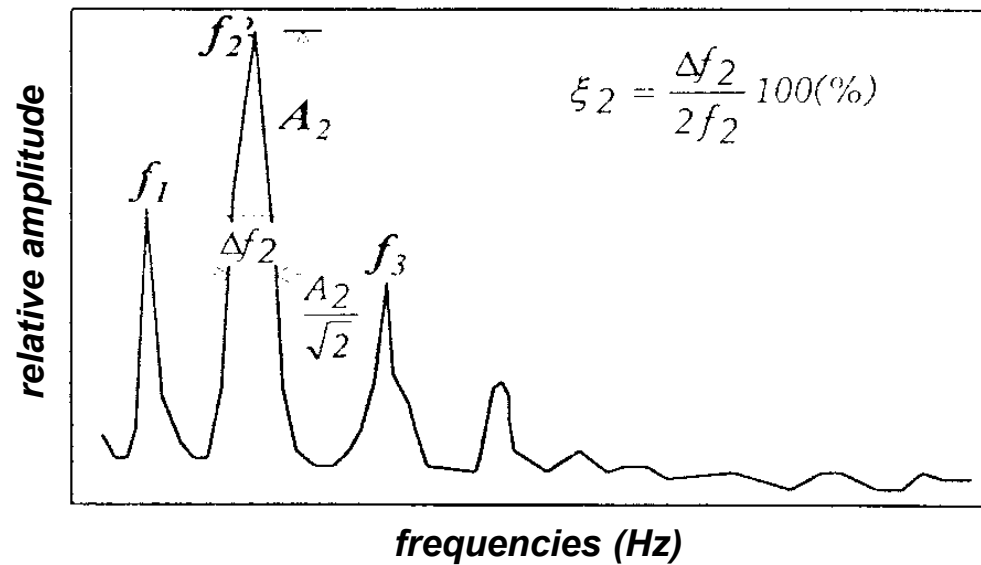




Ambient vibration testing procedure consists of real time recording of the vibrations and processing of the records by means of the Fast Fourier Transform , i. e. obtaining of Fourier Amplitude Spectra.



$$X(f) = \int_{-\infty}^{+\infty} x(t)e^{-2\pi if} dt$$

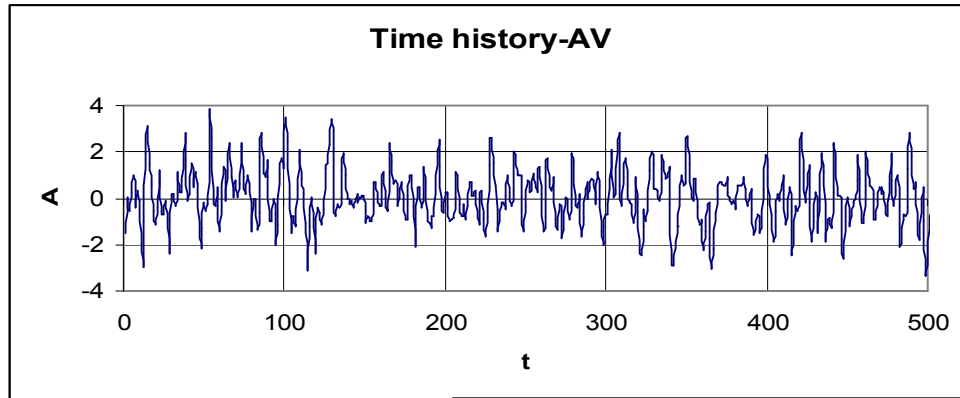


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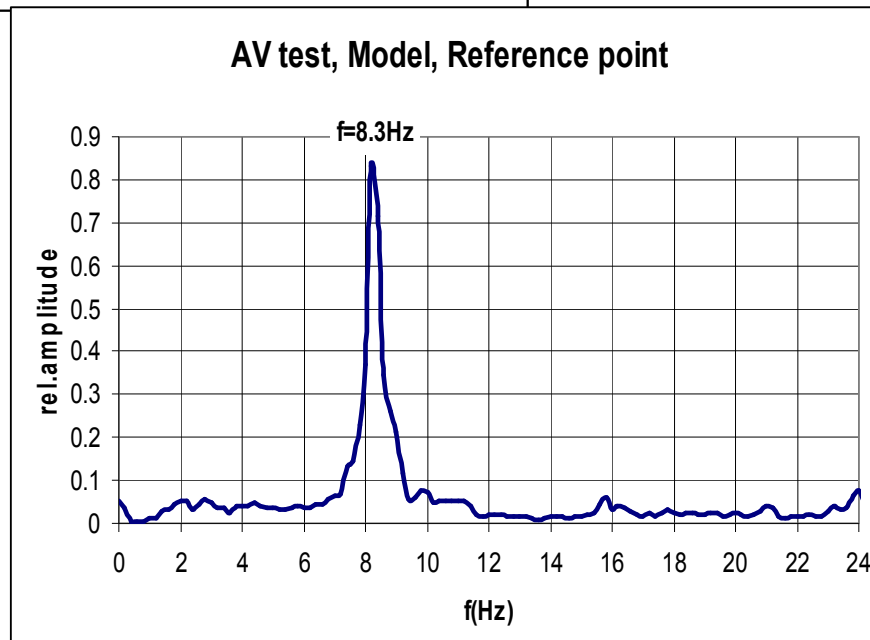
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The peaks of the amplitude spectrum occur at the predominant frequencies of the time function  $x(t)$ , which due to the flat spectrum of the excitation represent the natural frequencies of the structure.



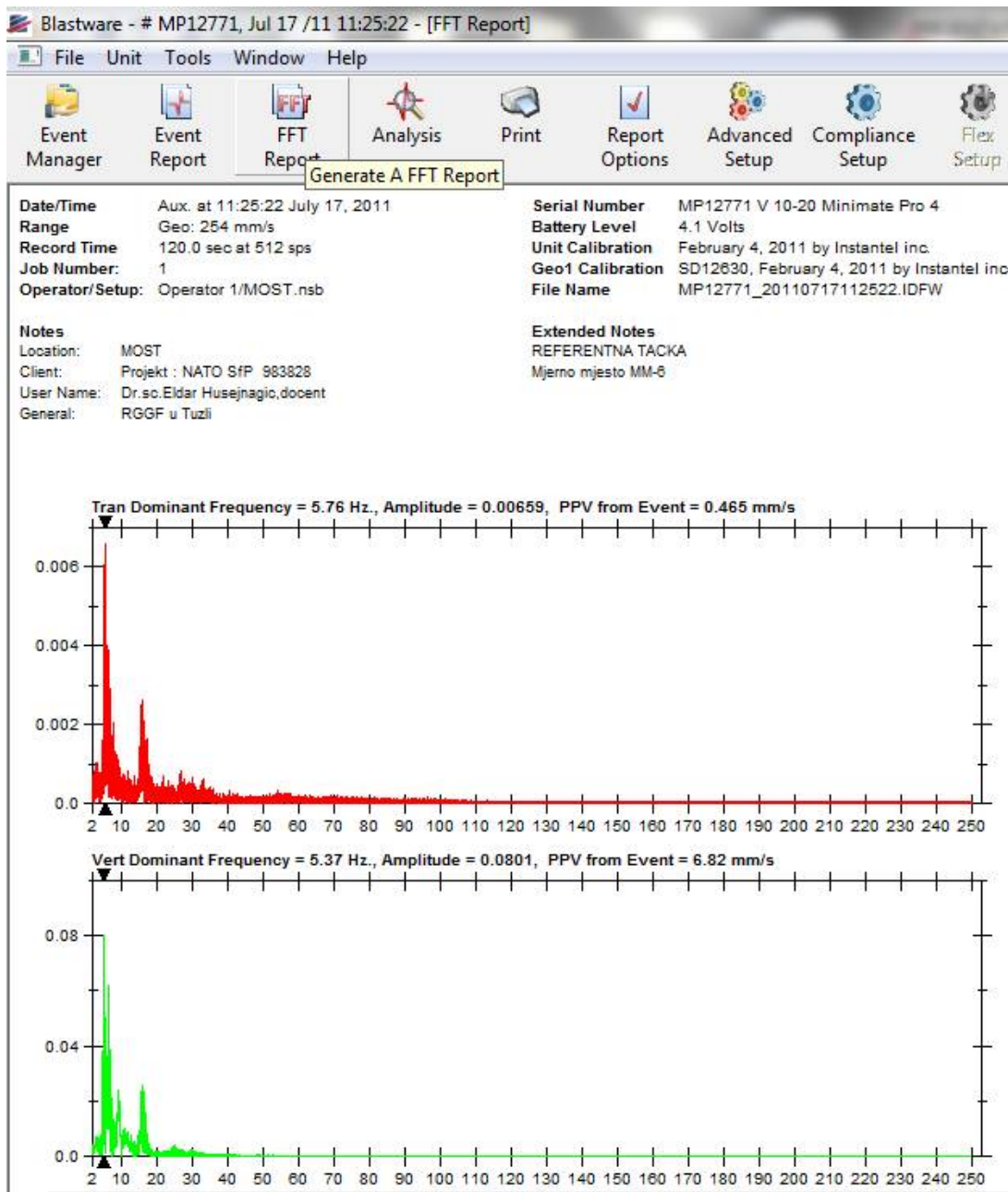
$$X(f) = \int_{-\infty}^{+\infty} x(t)e^{-2\pi if} dt$$



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*Measurement on base station 6R (middle of the span)*

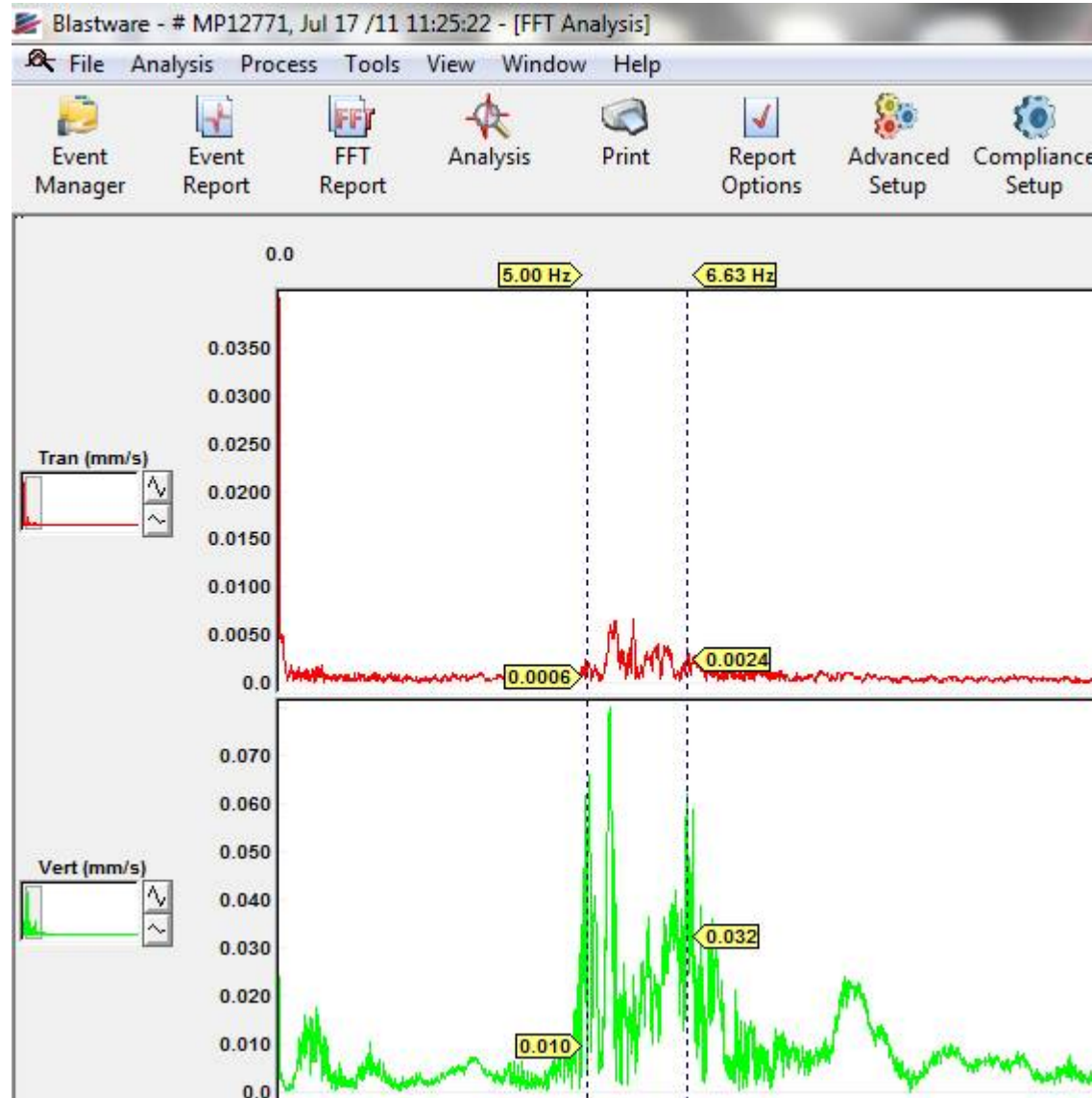


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## Measurement on base station 6R (middle of the span)

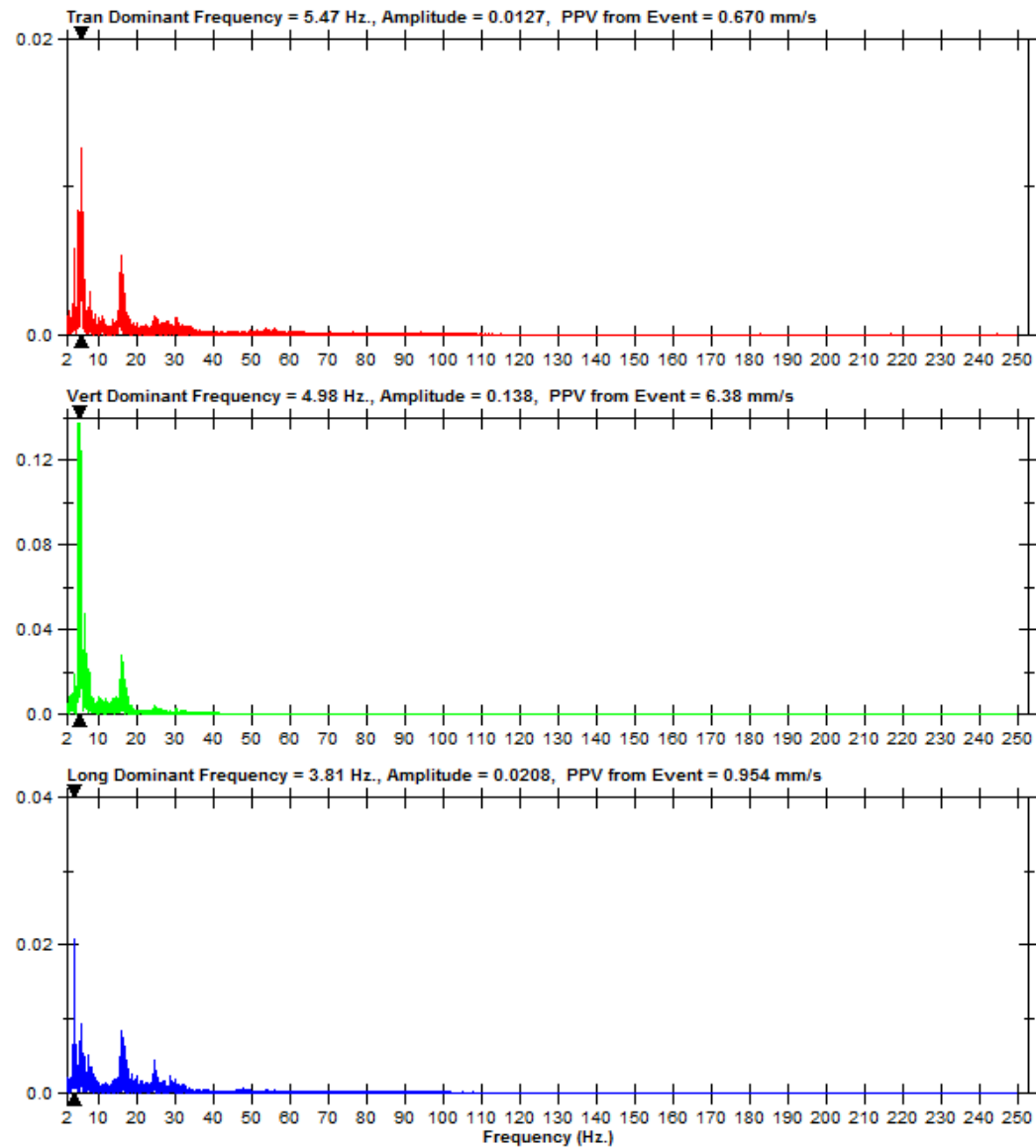


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## Measurement on base station 6R (middle of the span)

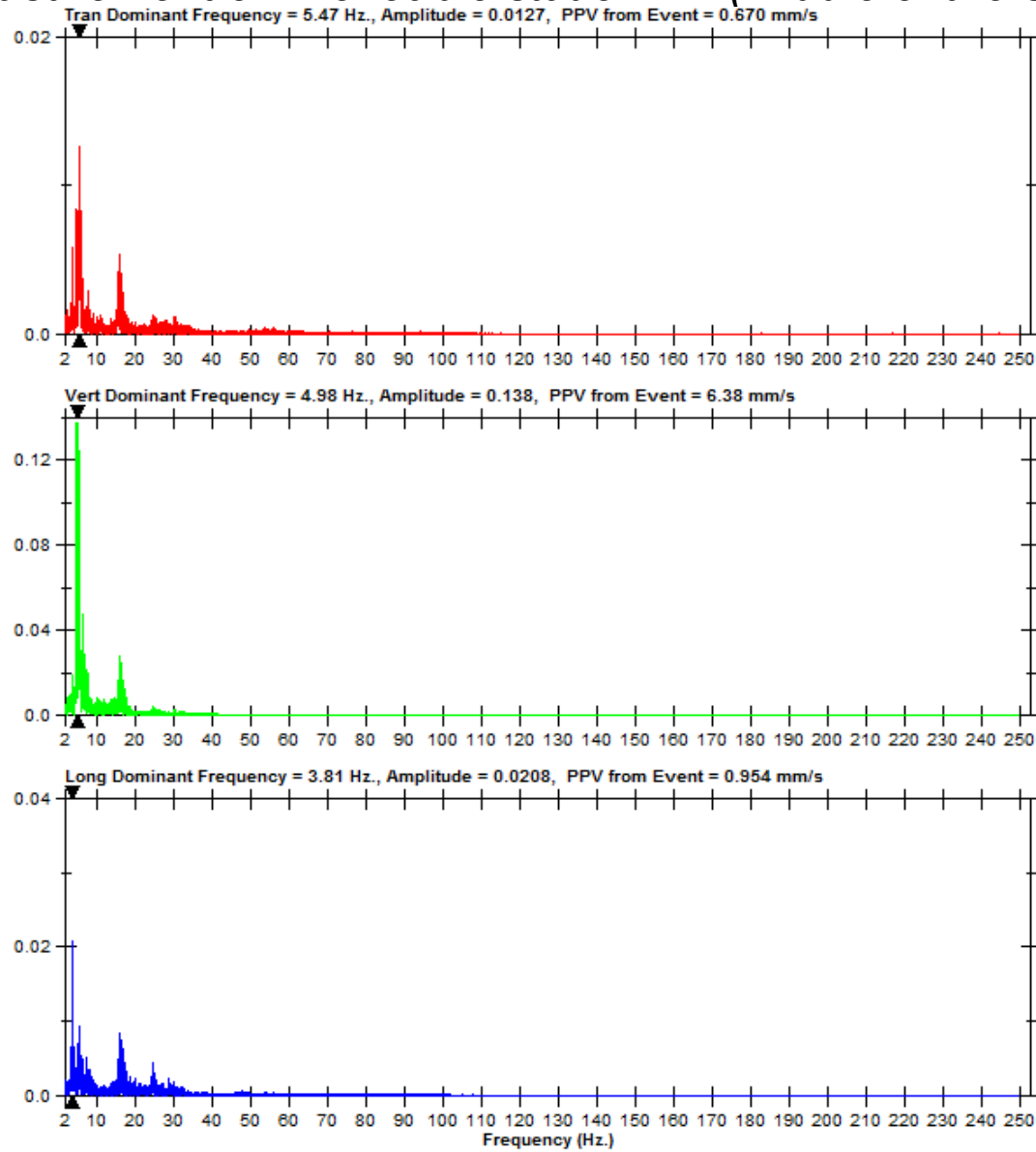


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## Measurement on moveable station 4R (middle of the span)

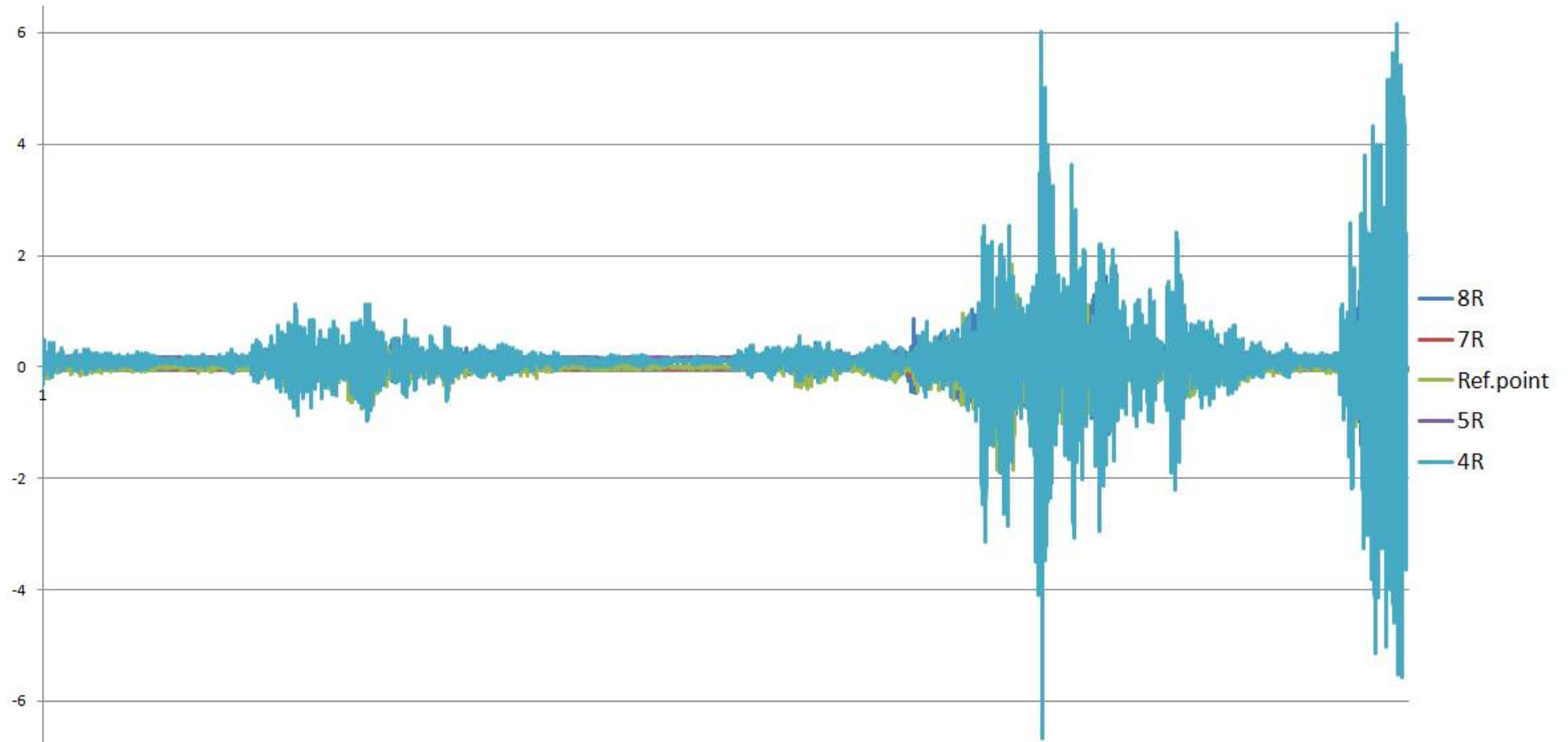


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## Comparison of vertical channels



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## *Measured dominant frequency*

Measuring points	Trans. Freq. (Hz)	Vert. Freq. (Hz)	Long. Freq. (Hz)
M1 4R, 5R, 6R, 7R, 8R	5.62, 5.63, 5.47, 5.62, 5.63	5.45, 5.60, 4.98, 3.81, 5.61	5.61, 5.60, 3.81, 3.81, 3.81
M2 2R, 3R, 6R, 9R, 10R	5.77, 5.97, 16.4, 5.97, 6.00	7.69, 5.50, 4.97, 5.43, 7.58	19.6, 5.43, 3.73, 5.43, 6.16
M3 1R, 2R, 6R, 10R, 11R	5.76, 5.75, 5.57, 5.75, 5.75	7.85, 7.86, 4.95, 5.73, 5.73	21.7, 5.56, 3.85, 5.56, 5.56
M4 6R, 4L, 5L, 6L, 7L	5.76, 5.76, 5.76, 5.49, 5.76	5.38, 5.74, 5.76, 5.36, 17.2	5.48, 5.48, 5.48, 5.48, 3.88
M5 6R, 3L, 4L, 8L, 9L	5.54, 6.48, 5.75, 7.74, 5.02	5.02, 5.54, 5.78, 5.02, 5.54	3.86, 5.54, 5.54, 17.2, 5.54
M6 6R, 1L, 2L, 10L, 11L	16.3, 6.70, 19.3, 5.67, 8.24	6.85, 20.3, 6.70, 8.17, 20.9	3.92, 7.95, 19.50, 6.29, 6.29
M7 6R, 12, 13, 16, 17	4.95, 14.1, 4.99, 2.01, 2.00	4.99, 2.27, 4.99, 2.00, 2.01	16.1, 5.50, 5.50, 2.01, 2.02
M8 6R, 12, 13, 16, 17	6.84, 16.6, 5.84, 2.00, 2.00	6.84, 2.39, 17.1, 2.00, 2.00	3.91, 6.28, 6.37, 2.00, 2.00



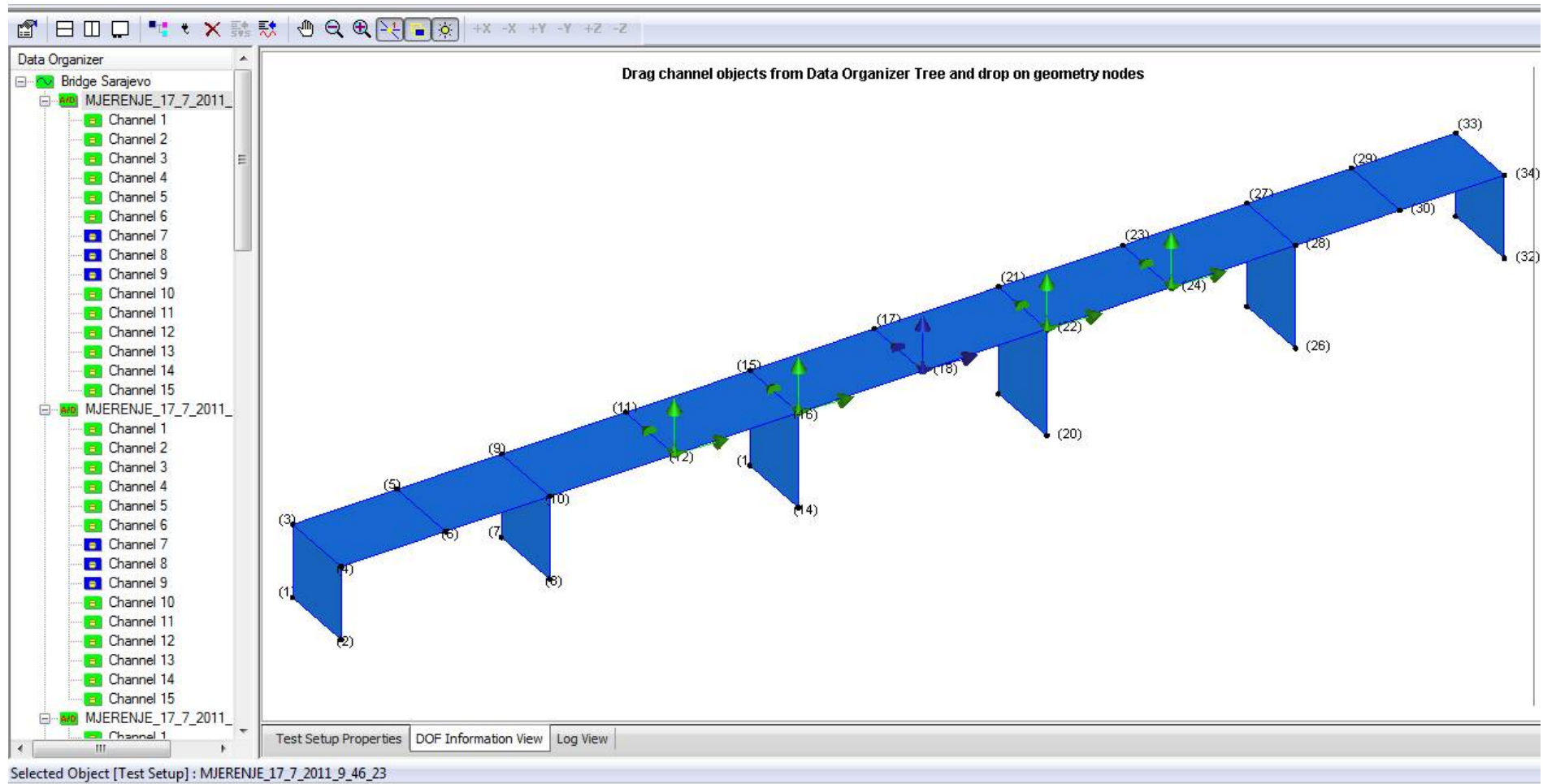
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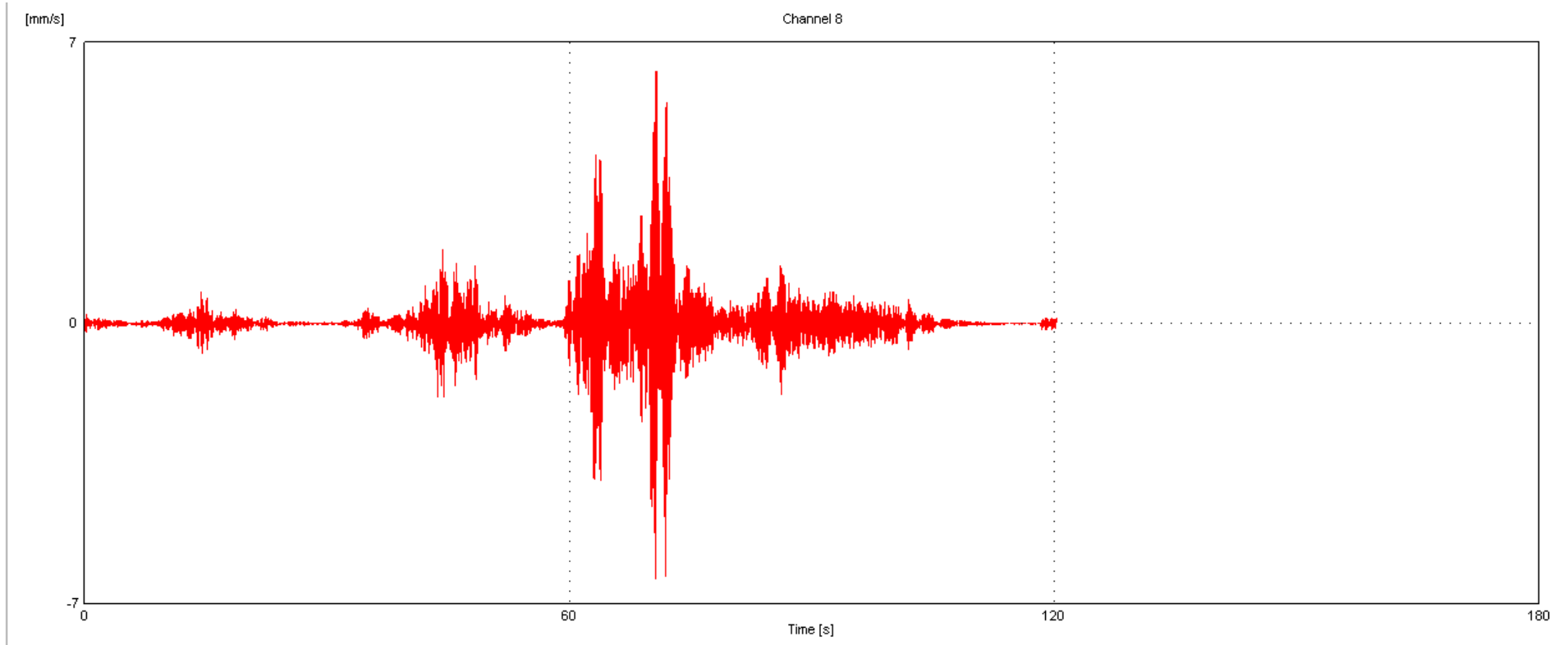


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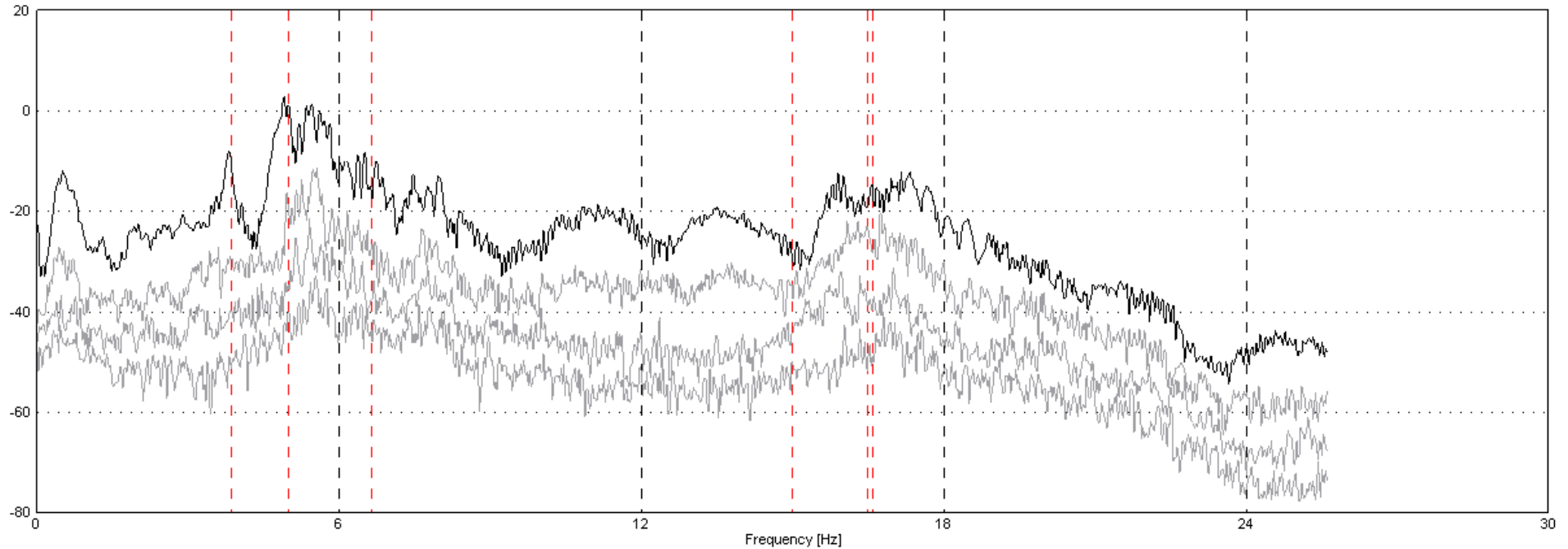
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# ARTEMIS

[dB] (1 mm/s)<sup>2</sup> / Hz

Frequency Domain Decomposition - Peak Picking  
Singular Values of Spectral Density Matrices  
of Test Setup: MJERENJE\_17\_7\_2011\_9\_46\_23

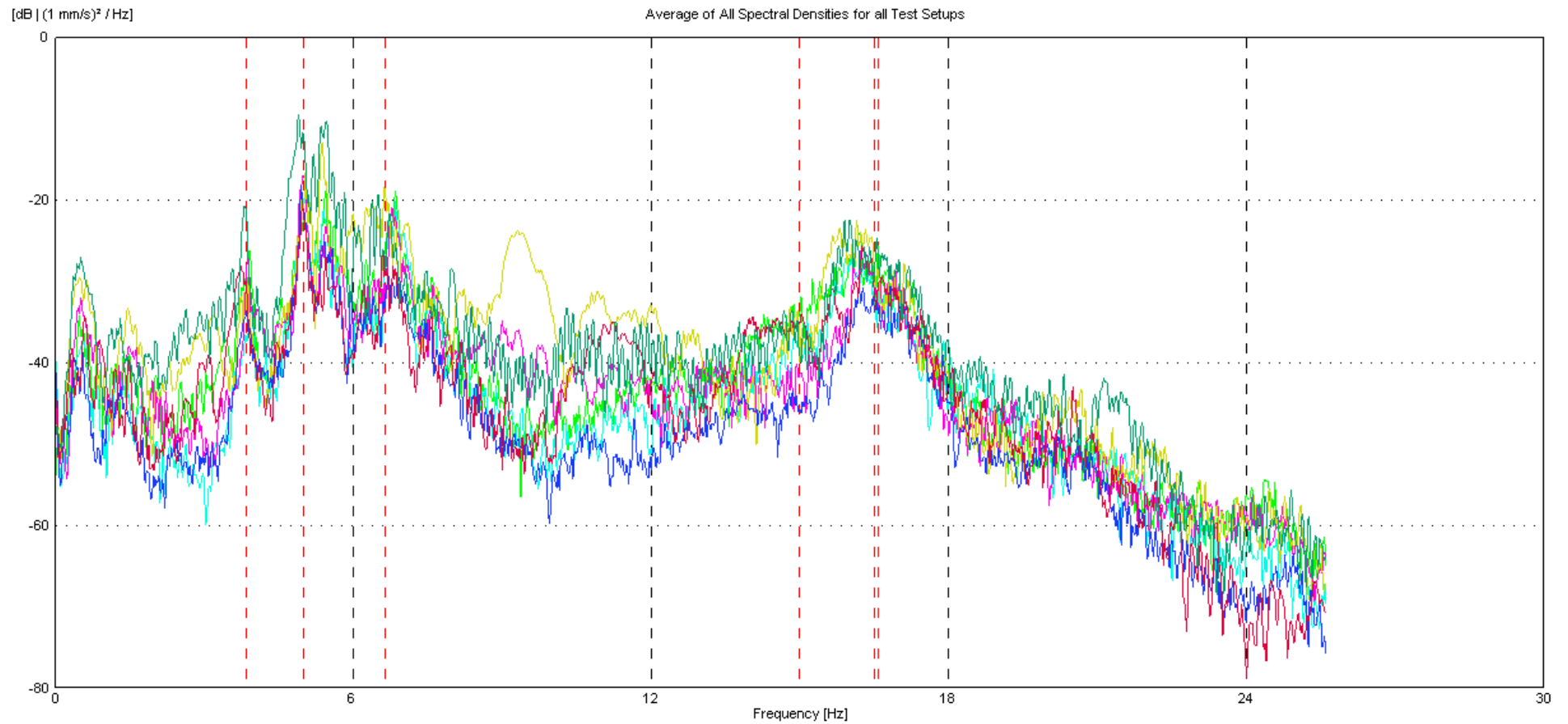


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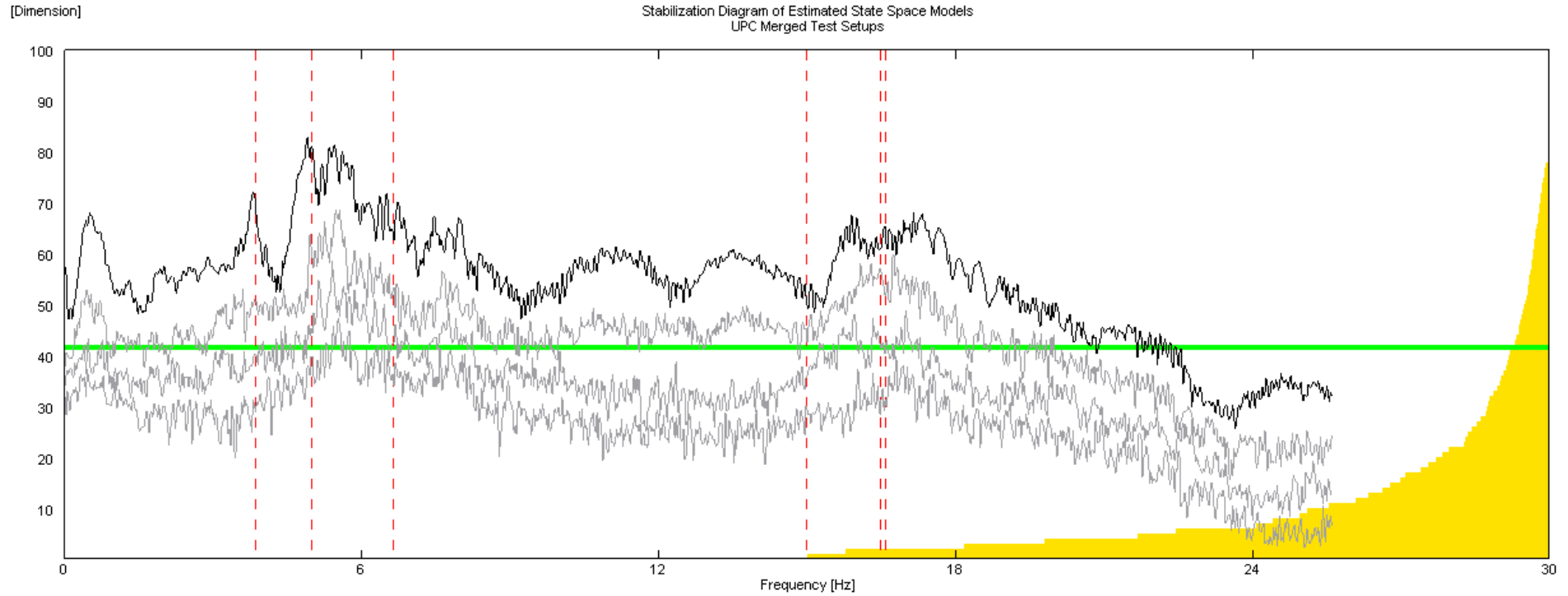


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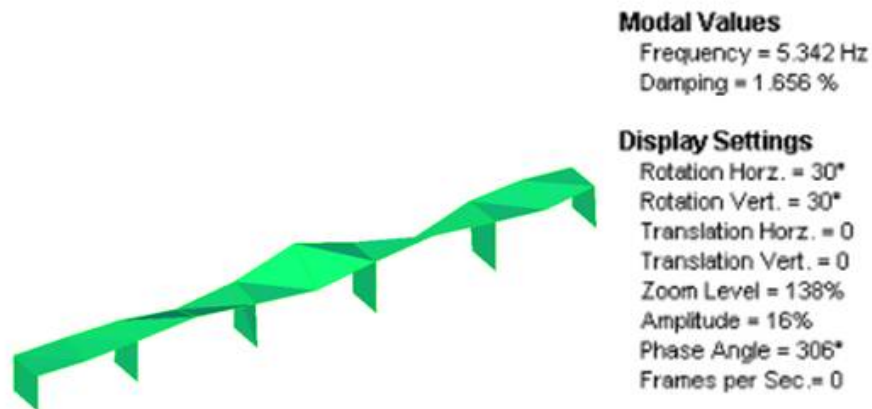
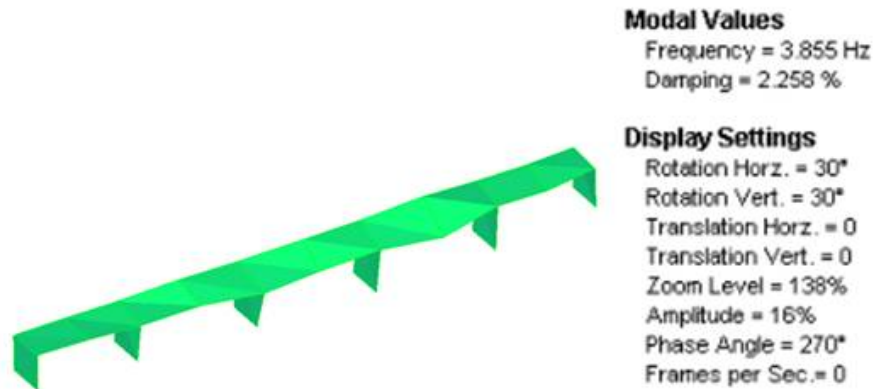


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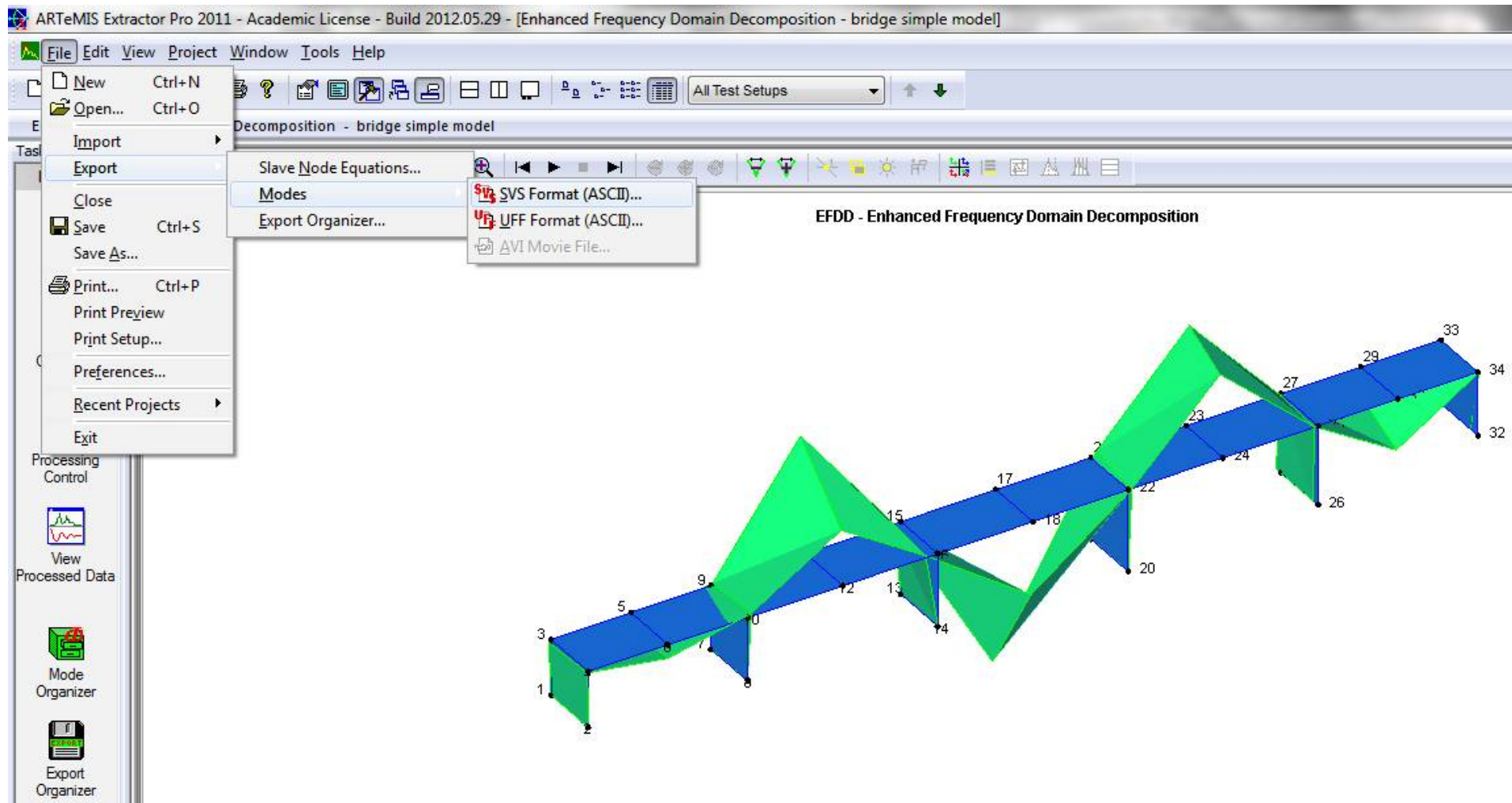


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# Transfer data to another program



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# Transfer data to another program

```

PROJECT
  bridge simple model

ESTIMATOR
  EFDD

CREATION: DATE / TIME
  05-02-2019 12:59:48

FREQUENCY [HZ]: MEAN / SDEV
  5.061297e+000 1.615336e-001

DAMPING [%]: MEAN / SDEV
  4.747341e-001 3.778914e-001

MODE SHAPE: NODE / X-ABS / X-ANG / Y-ABS / Y-ANG / Z-ABS / Z-ANG
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  2 9.431071e-005 7.459833e-001 1.709870e-004 -2.433685e+000 1.960708e-004 -2.314426e+000
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  16 5.509119e-002 -1.662650e-001 7.442271e-003 -1.112156e+000 6.211388e-003 -7.789988e-001
  17 1.309099e-002 -1.039611e-001 1.062308e-002 2.644106e+000 5.702300e-001 8.182932e-002
  18 1.150952e-002 1.594058e-001 1.031973e-002 1.823201e+000 2.716287e-001 -3.137015e-002
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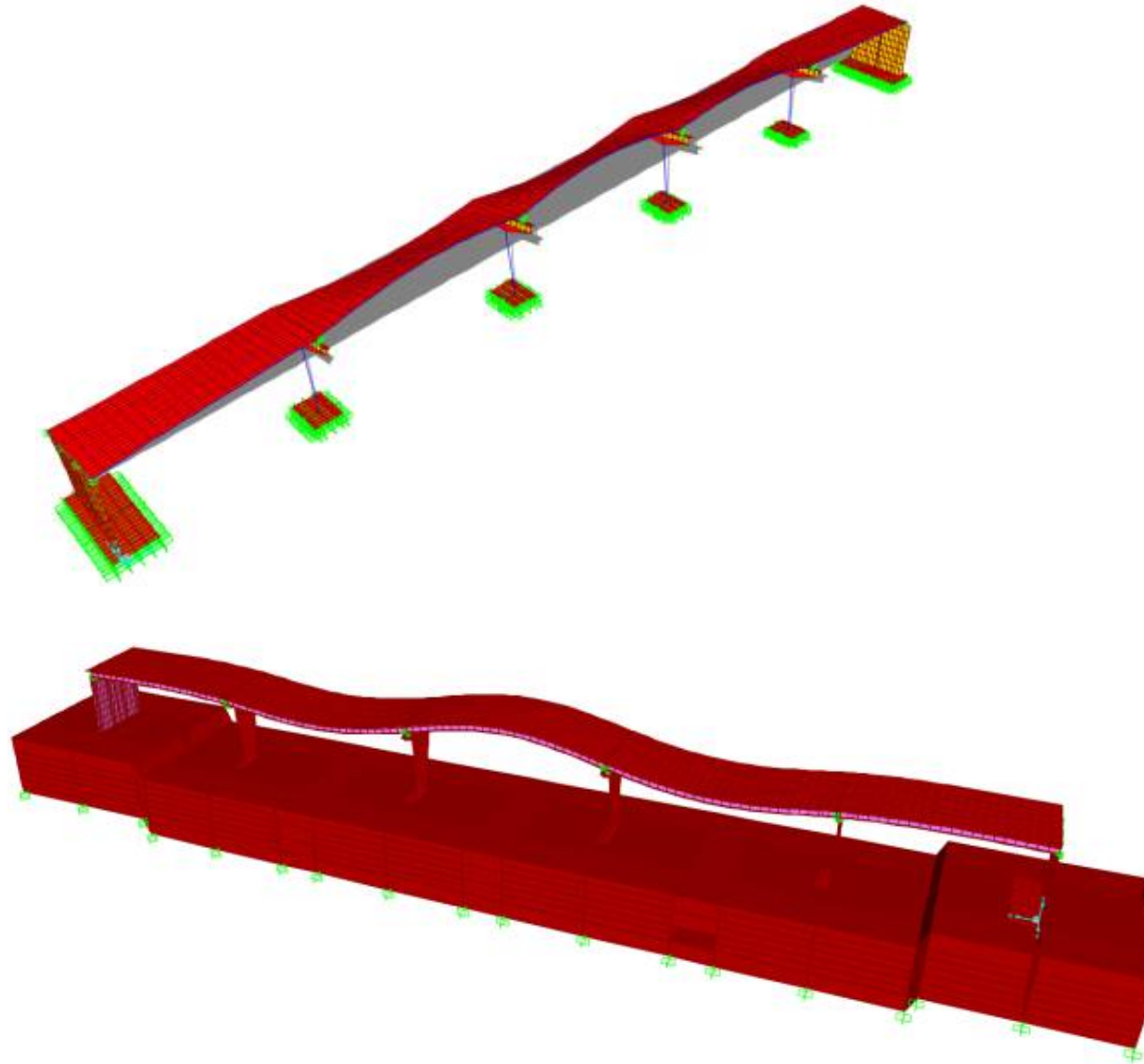
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## Finite Element Models (FEMs)

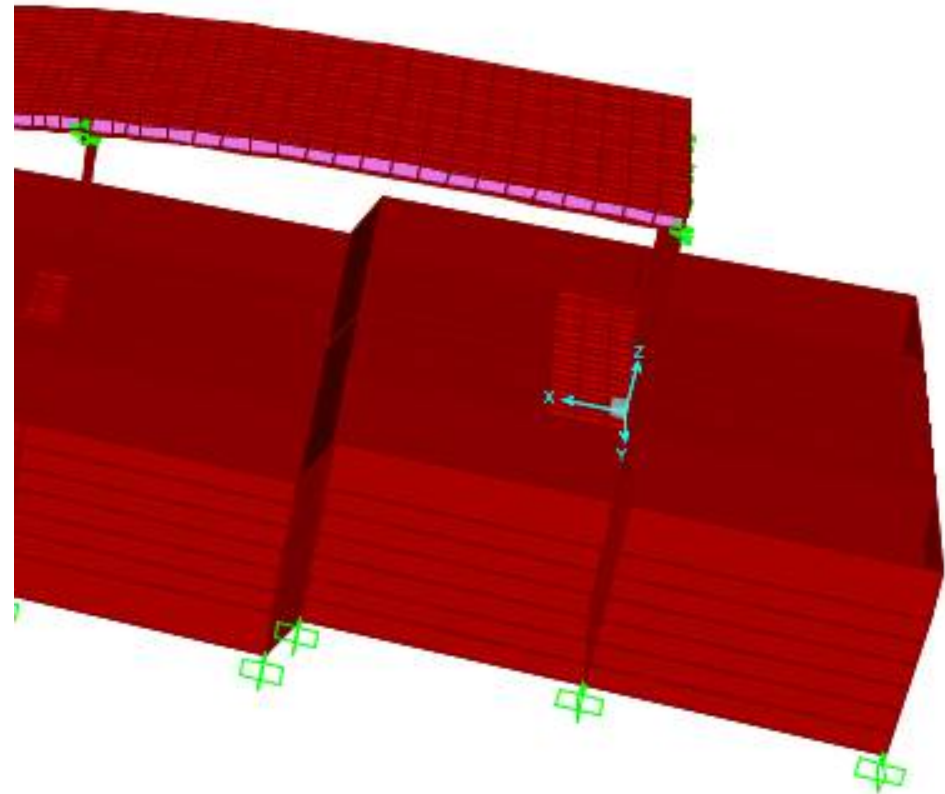
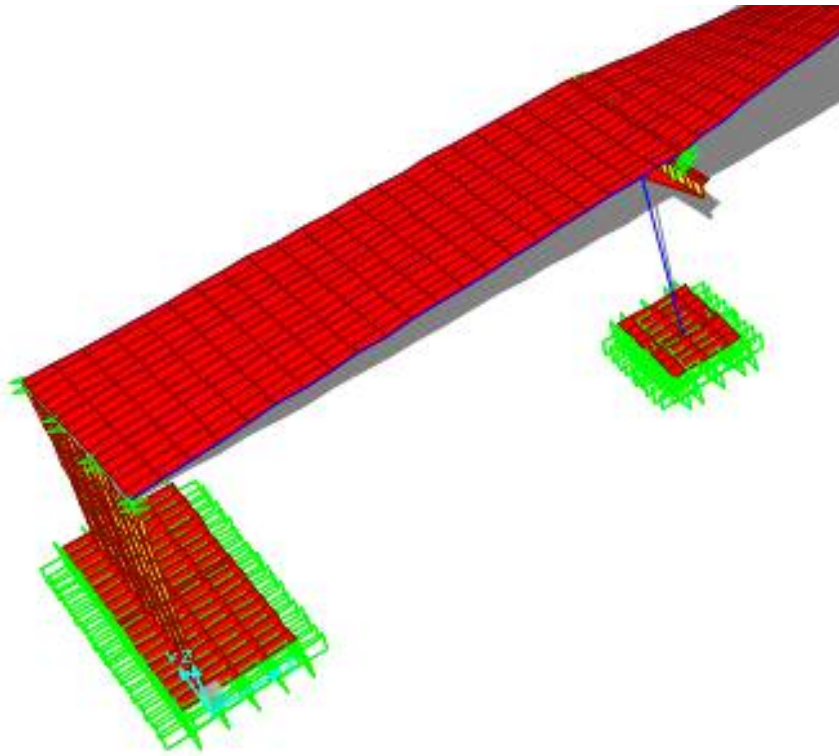


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## Review of the FEMs

S1-NB1-M1	S1-NB1-M2	S1-NB2-M2	S1-NB3-M2
S2-NB1-M1	S2-NB1-M2	S2-NB2-M2	S2-NB3-M2
S3-NB1-M1	S3-NB1-M2	S3-NB2-M2	S3-NB3-M2
S4-NB1-M1	S4-NB1-M2	S4-NB2-M2	S4-NB3-M2
S5-NB1-M1	S5-NB1-M2	S5-NB2-M2	S5-NB3-M2
S6-NB1-M1	S6-NB1-M2	S6-NB2-M2	S6-NB3-M2
SOIL	NEOPREN ELASTOMERIC BEARING		CONCRETE STRENGTH
<p>S1- absolute stiff</p> <p>S2 – 10 x k (S4)</p> <p>S3 – 5 x k (S4)</p> <p>S4 – empirical stiffness of soil (k = 15000kN/m<sup>2</sup>) has been selected based on the experience with similar soils</p> <p>S5 – layered soil (LS) with modulus E determined by (PGSM)</p> <p>S6 – LS with 10% of modulus E</p>	<p>NB1 – designed stiffness (DS)</p> <p>NB2 – 1.5 x DS</p> <p>NB3 - stiff</p>		<p>M1 – designed strength (f<sub>ck</sub> = 30MPa, E<sub>cm</sub> = 31GPa)</p> <p>M2 – theoretical strength after 45 years' service (E<sub>c0</sub> = 38,5GPa)</p>



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### *Modal frequencies*

	LONGITUDINAL MODE	TRANSVERSE MODE	BENDING MODE	TORSIONAL MODE
Ambient Vibration Measurements	-	3.855	4.971	5.342
FEMs				
S1-NB1-M1	2.654 (2)	2.803 (3)	3.673 (4)	3.896 (6)
S2-NB1-M1	2.442 (1)	2.454 (2)	3.654 (3)	3.810 (6)
S3-NB1-M1	2.267 (2)	2.148 (1)	3.651 (4)	3.616 (3)
S4-NB1-M1	1.567 (2)	1.444 (1)	3.630 (4)	2.967 (3)
S5-NB1-M1	2.523 (2)	2.312 (1)	3.907 (6)	3.711 (5)
S6-NB1-M1	2.459 (2)	1.969 (1)	3.884 (6)	3.405 (4)
S1-NB1-M2	2.751 (1)	<b>3.641 (2)</b>	3.798 (5)	4.377 (6)
S2-NB1-M2	2.512 (1)	2.522 (2)	3.828 (3)	3.949 (6)
S3-NB1-M2	2.323 (2)	2.198 (1)	3.824 (4)	3.737 (3)
S4-NB1-M2	1.586 (2)	1.448 (1)	3.794 (6)	3.030 (3)
S5-NB1-M2	2.614 (2)	2.369 (1)	4.081 (6)	3.806 (5)
S6-NB1-M2	2.542 (2)	2.011 (1)	4.054 (6)	3.483 (3)
S1-NB2-M2	2.971 (1)	<b>3.731 (2)</b>	3.825 (3)	4.443 (6)
S2-NB2-M2	2.666 (2)	2.556 (1)	3.860 (3)	4.065 (6)

## Modal frequencies

	LONGITUDINAL MODE	TRANSVERSE MODE	BENDING MODE	TORSIONAL MODE
Ambient Vibration Measurements	-	3.855	4.971	5.342
FEMs				
S3-NB2-M2	2.442 (2)	2.224 (1)	3.857 (3)	3.857 (4)
S4-NB2-M2	1.627 (2)	1.467 (1)	3.827 (6)	3.124 (3)
S5-NB2-M2	2.804 (2)	2.411 (1)	4.184 (6)	4.126 (5)
S6-NB2-M2	2.715 (2)	2.046 (1)	4.156 (6)	3.755 (4)
S1-NB3-M2	3.574 (1)	<b>4.246 (3) (fig.14a)</b>	4.136 (2)	<b>5.026 (5) (fig.14b)</b>
S2-NB3-M2	3.207 (2)	2.689 (1)	4.261 (3)	4.383 (4)
S3-NB3-M2	2.915 (2)	2.317 (1)	4.253 (4)	4.143 (3)
S4-NB3-M2	1.965 (2)	1.528 (1)	4.198 (4)	3.320 (3)
S5-NB3-M2	3.407 (2)	2.513 (1)	<b>4.639 (3)(fig.14c)</b>	4.847 (3)
S6-NB3-M2	3.239 (2)	2.146 (1)	4.609 (4)	4.318 (3)

(n) marks in parenthesis denote modes of certain models

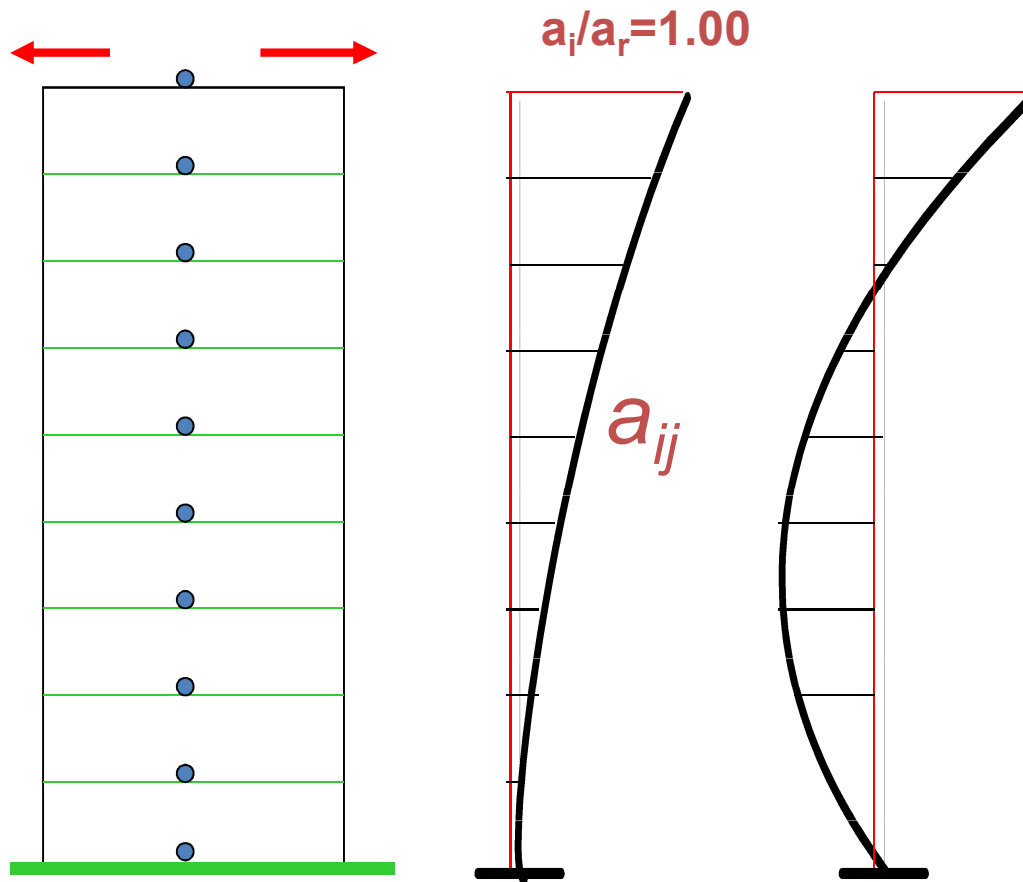


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## Comparison of the modes parameters (mode shapes) identified by AVM and FEMs



**Normalized amplitudes at  
selected points (levels) for  
each particular mode  
shape**

$$a_{i,j} = \frac{|X_i(f_j)|}{|X_r(f_j)|}$$



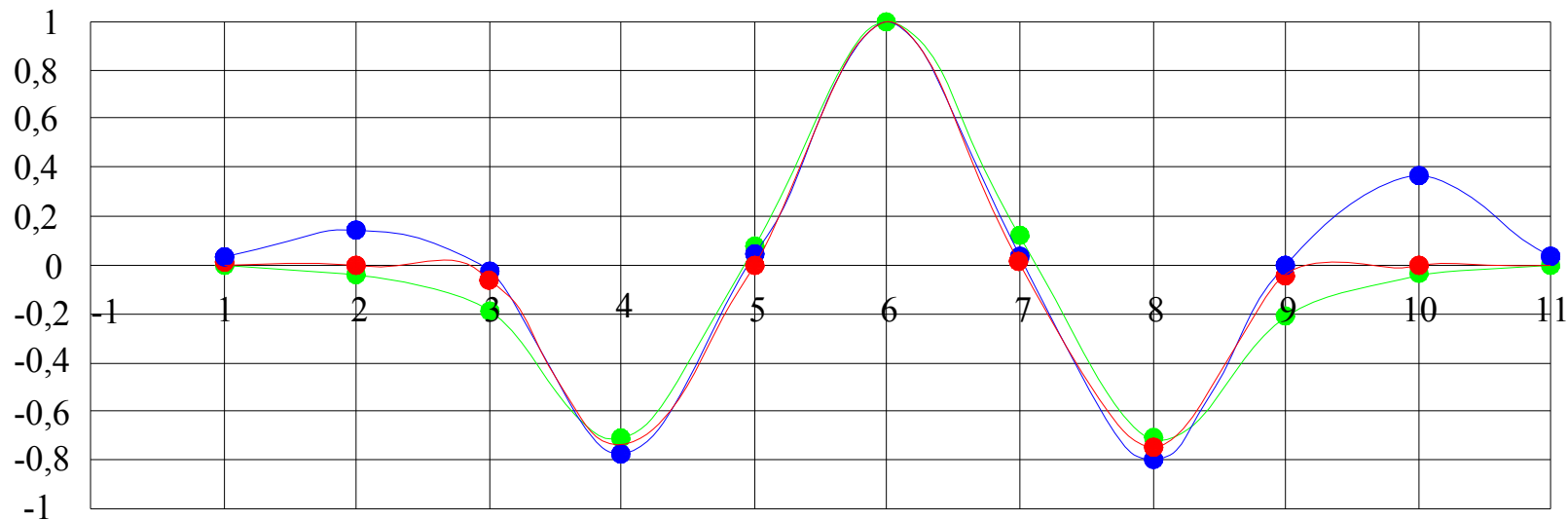
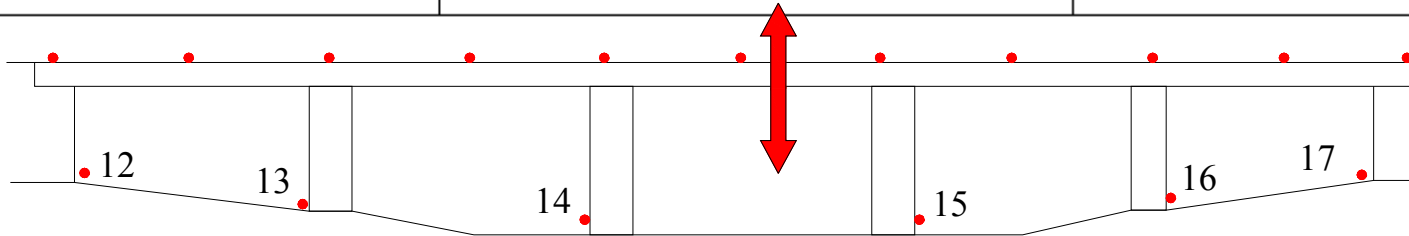
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## Experimentally and mathematically identified first vertical mode shapes

	FIRST TRANSVERSE MODE	FIRST VERTICAL MODE
AMBIENT VIBRATION TEST	3.855	4.971
ANALYTICAL MODEL AM1	3.641	3.798
ANALYTICAL MODEL AM2	2.513	4.639



—●— AVM      —●— AM1      —●— AM2



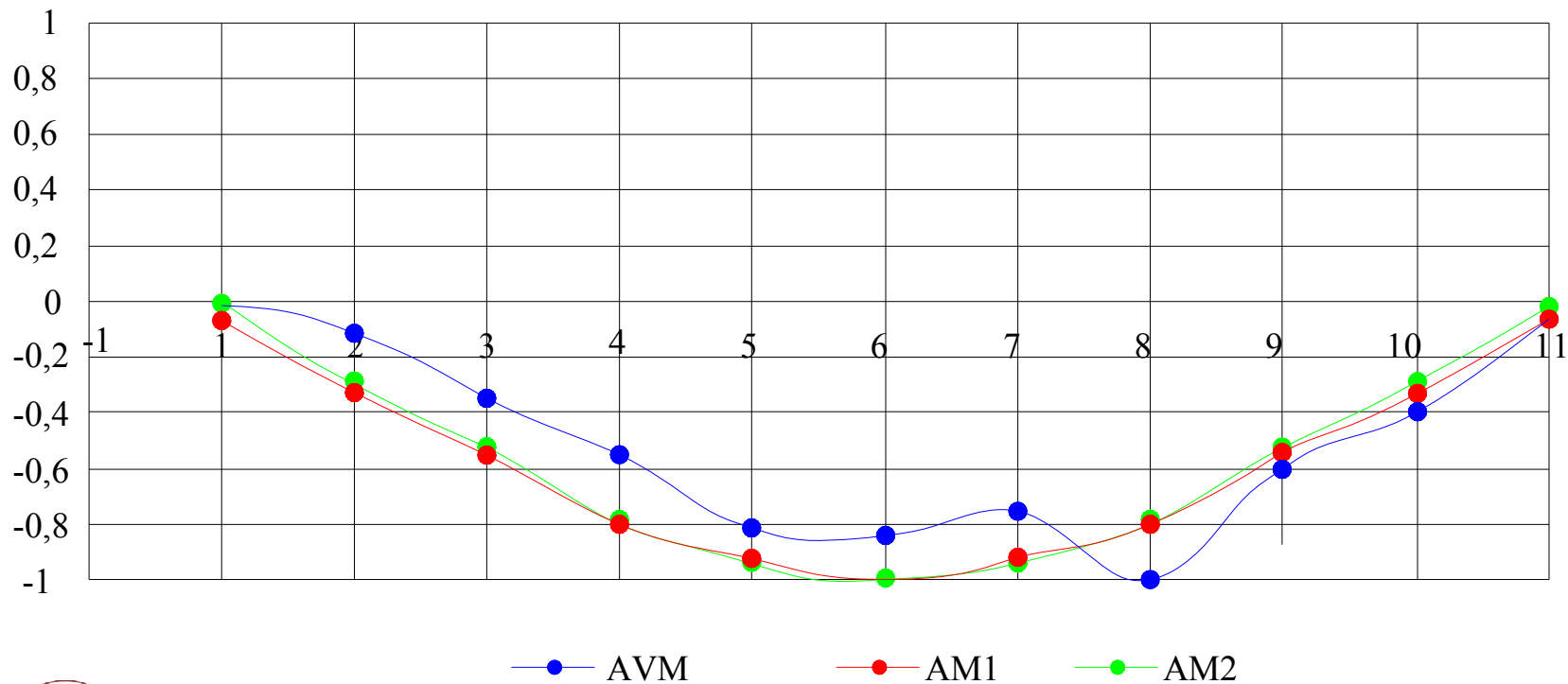
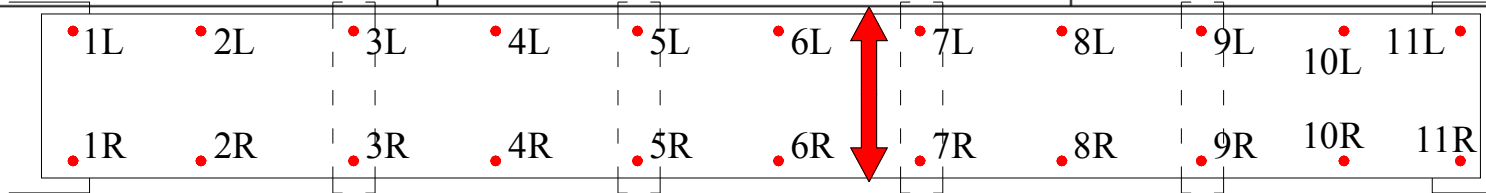
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## Experimentally and mathematically identified first transverse mode shapes

	FIRST TRANSVERSE MODE	FIRST VERTICAL MODE
AMBIENT VIBRATION TEST	3.855	4.971
ANALYTICAL MODEL AM1	3.641	3.798
ANALYTICAL MODEL AM2	2.513	4.639



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## ***CASE STUDY 2 – THE TWIN BRIDGE “GOCE DELCEV” IN SKOPJE***

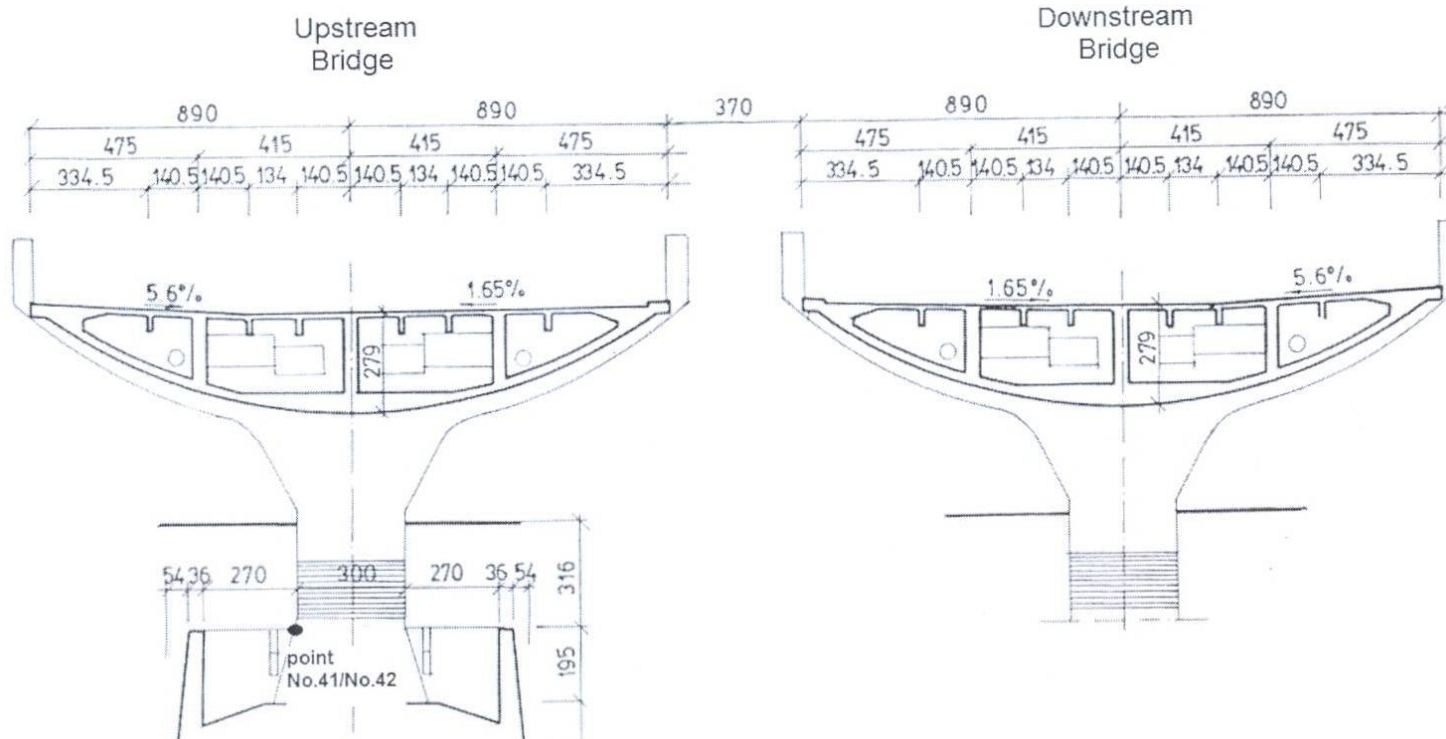
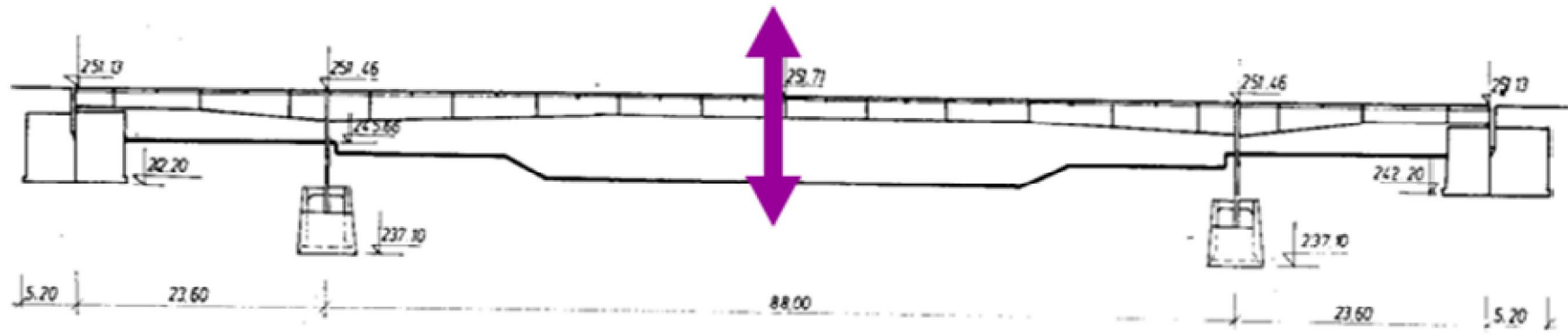


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## Elevation and cross-sections of the bridge



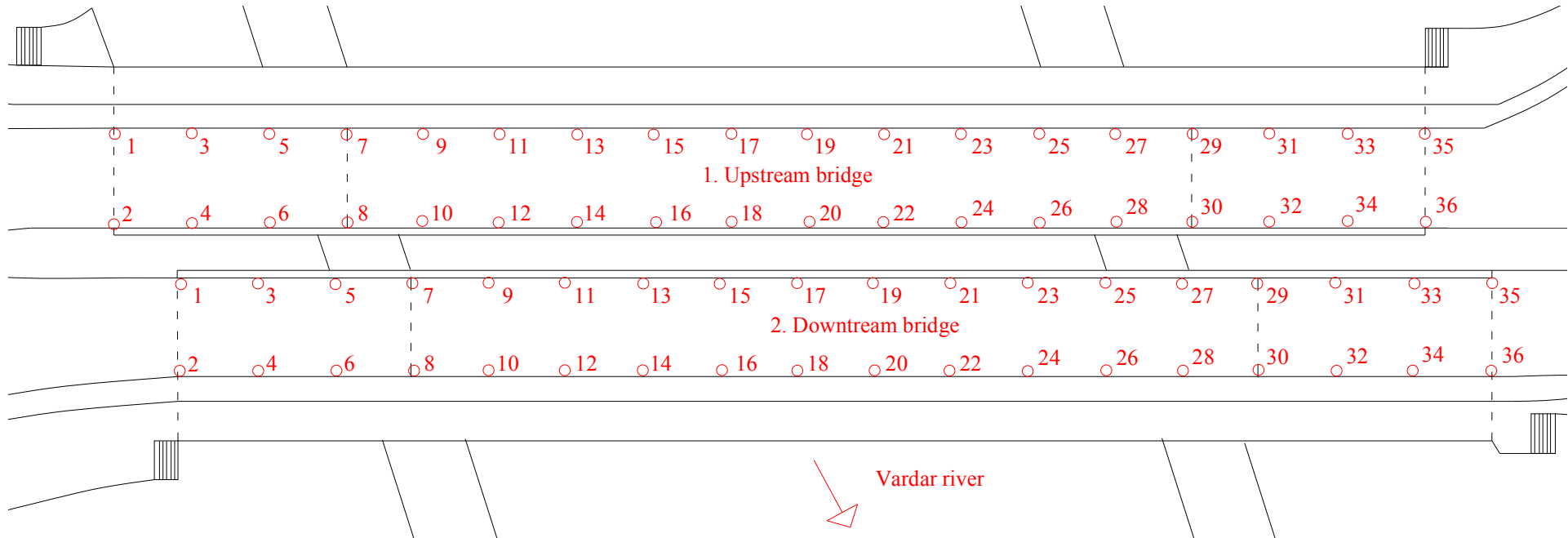
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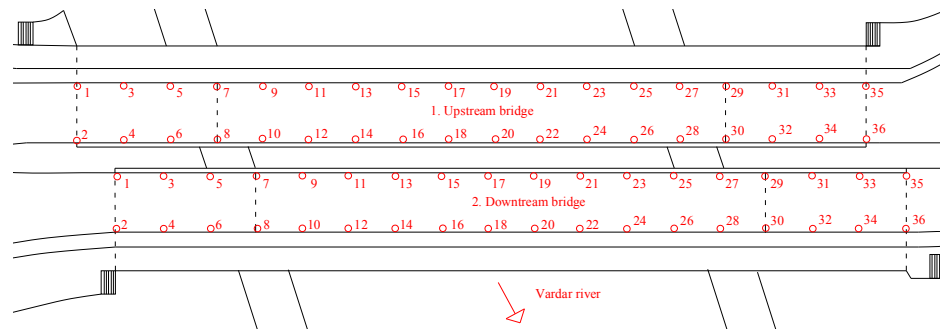
# Measurements setup



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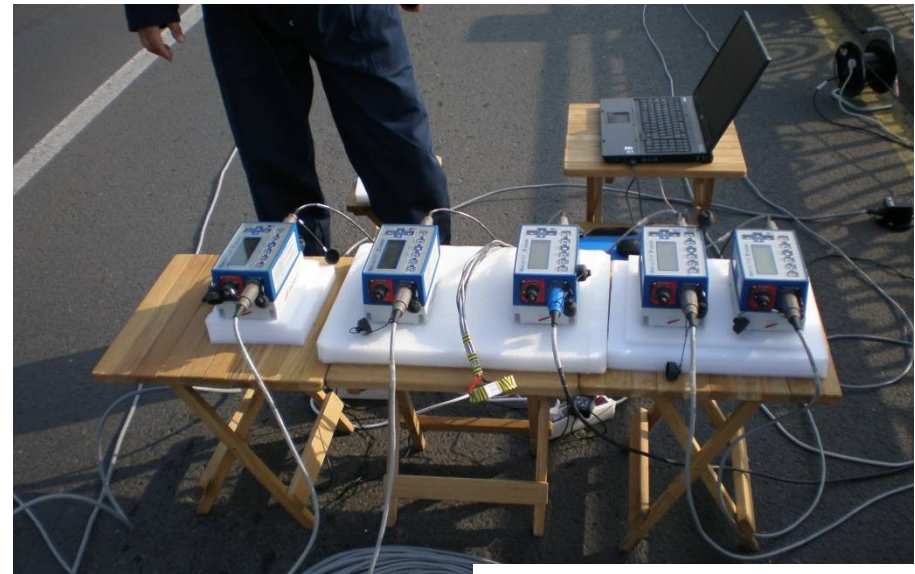
Setup	Moveable stations	Base stations
M1	37,38	16R
M2	1,2,3,4	16R
M3	1,2,3,4	16R
M4	5,6,7,8	16R
M5	9,10,11,12	16R
M6	13,14,15	16R
M7	17,18,19,20	16R
M8	21,22,23,24	16R
M9	25,26,27,28	16R
M10	29,30,31,32	16R
M11	33,34,35,36	16R
M12	33,34,35,36	16R
M13	39,40	16R
M14	41,42	16R

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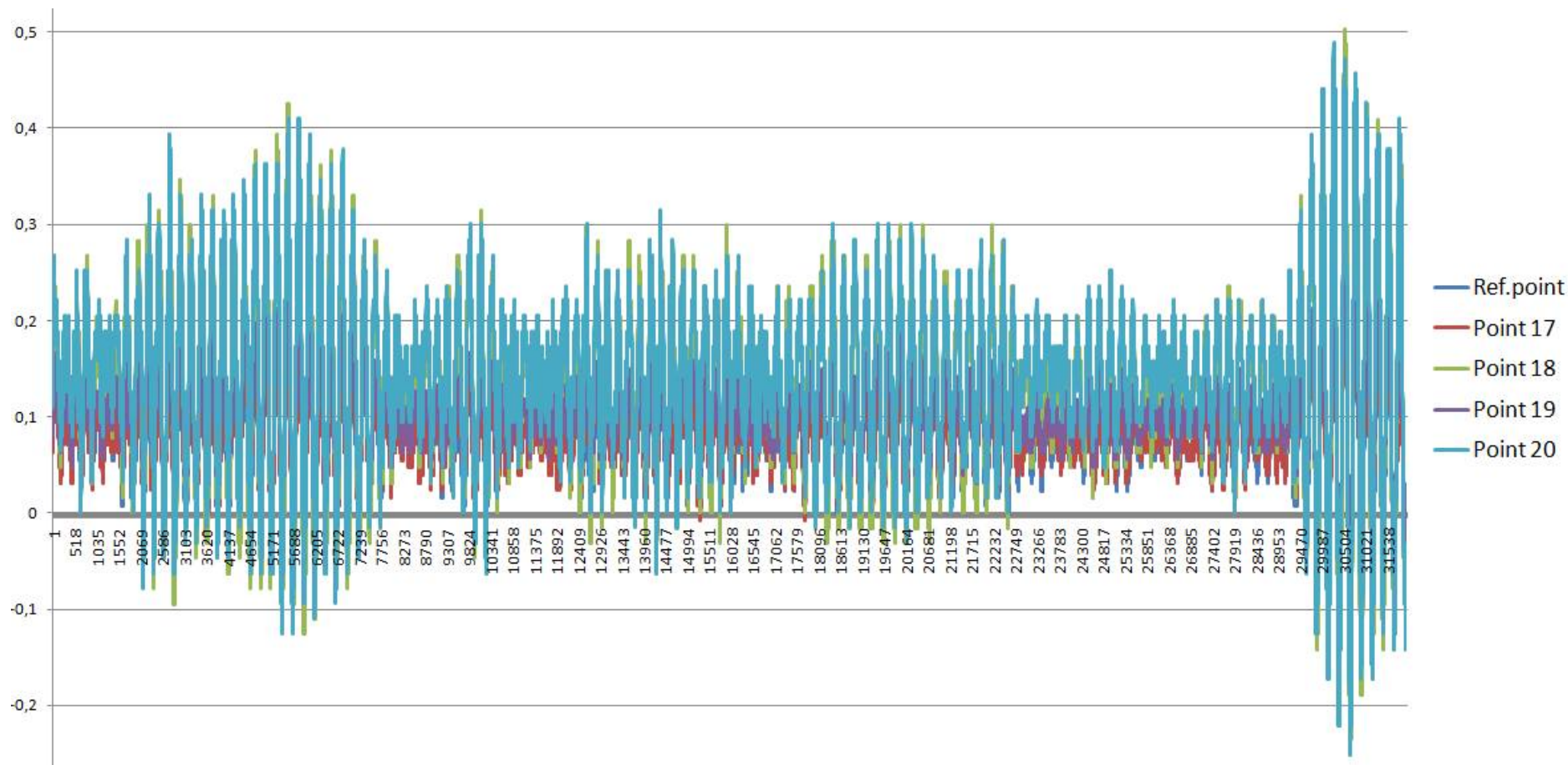


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# Transversal chanel

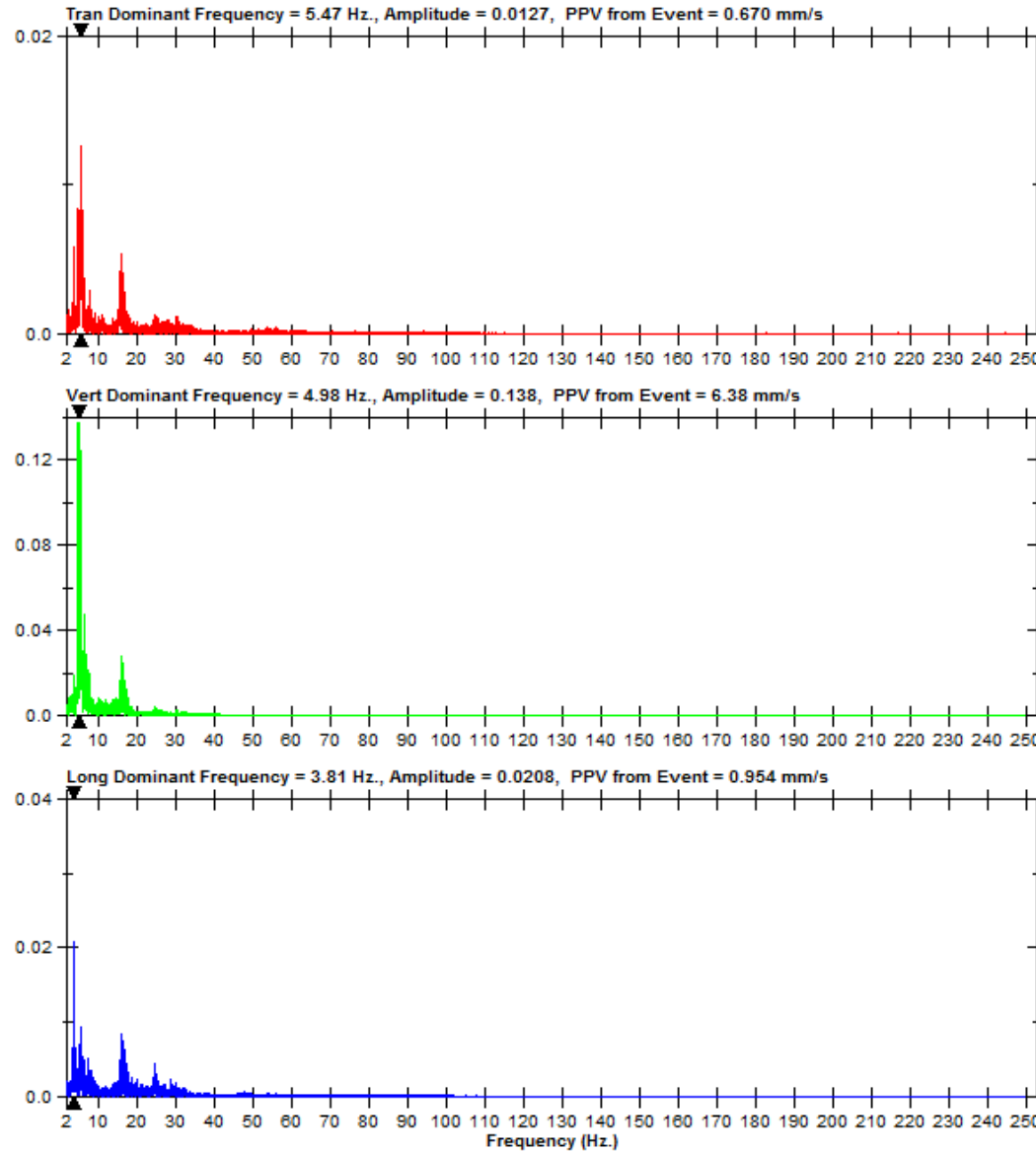


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# Measurement on base station 16R

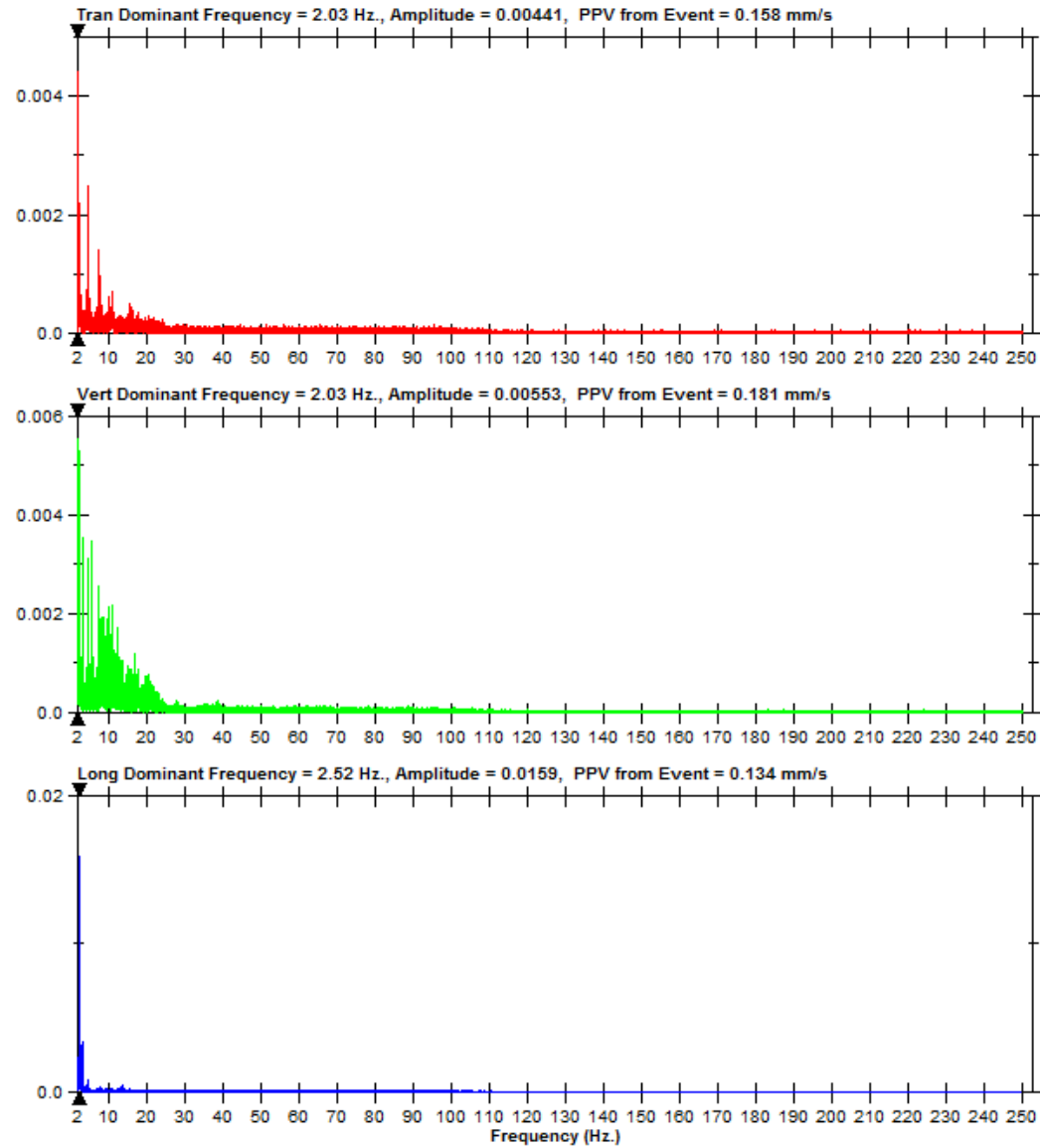


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# Measurement on moveable station



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## Measured dominant frequency

Measuring points	1 <sup>st</sup> freq. (Hz)	2 <sup>nd</sup> freq. (Hz)	3 <sup>rd</sup> freq. (Hz)
16R, 1, 2, 3, 4	1.30V, 2.00VTL, 1.98L, 1.30V, 1.98	1.98VT, 2.88L, -, 1.99VTL, -	-, 3.31L, -, 2.86L, -
16R, 5, 6, 7, 8	1.28V, 2.03VT, 2.03VT, 2.03VT.	2.03VT, 2.92V, 2.92L, 2.92L, 2.92L	4,27V, -, -, -, -
16R, 9, 10, 11, 12	1.29V, 1.29V, 1.29V, 1.30V, 1.30V	2.05VT, 2.06VT, 2.06VT, 2.05VT.	-, -, -, 2.95L, -
16R, 13, 14, 15	1.28V, 1.28V, 1.28V, 1.28V	2.02VT, 2.02VT, 2.02VT, 2.02VT	-, 2.91L, -, 2.91L
16R, 17, 18, 19, 20	1.29V, 1.29V, 1.29V, 1.29V, 1.28V	2.03VT, 2.03T, 2.03VT, 2.03T, 2.03T	4,23V, 3.34L, -, 3.35L, 3.35L
16R, 21, 22, 23, 24	1.28V, 1.28V, 1.28V, 1.28V, 1.28V	2.02VT, 2.02VT, 2.02VT, 2.02VT.	-, 2.90L, -, 2.91L, 2.91L
16R, 25, 26, 27, 28	1.28V, 1.28V, 1.28V, 1.28V, 1.28V	2.00VT, 2.00VTL, 2.00VT, 2.00VT.	-, 2.88L, 2.88L, 2.88L, 2.88L
16R, 29, 30, 31, 32	1.27V, 1.80VTL, 1.80VT, 1.80V, -	2.10VT, 2.10VTL, 2.10VT, 2.10VT.	-, 2.88L, 2.88L, 2.91L, 2.91L
16R, 33, 34, 35, 36	1.28V, 1.28V, 1.28V, 1.28L, 2.00L	2.02VT, 2.02VTL, 2.02VTL, 2.02TL.	-, 2.84L, -, 2.84L, -
16R, 37, 38	1.27V, 4.20VTL, 2.00T	2.01VT, -, 2.14V	4.23V, -, 8.88L
16R, 39, 40	1.29V, 2.90L, 2.07V	1.97VT, 7.83T, 4.63T	-, 13.7V, 11.8L

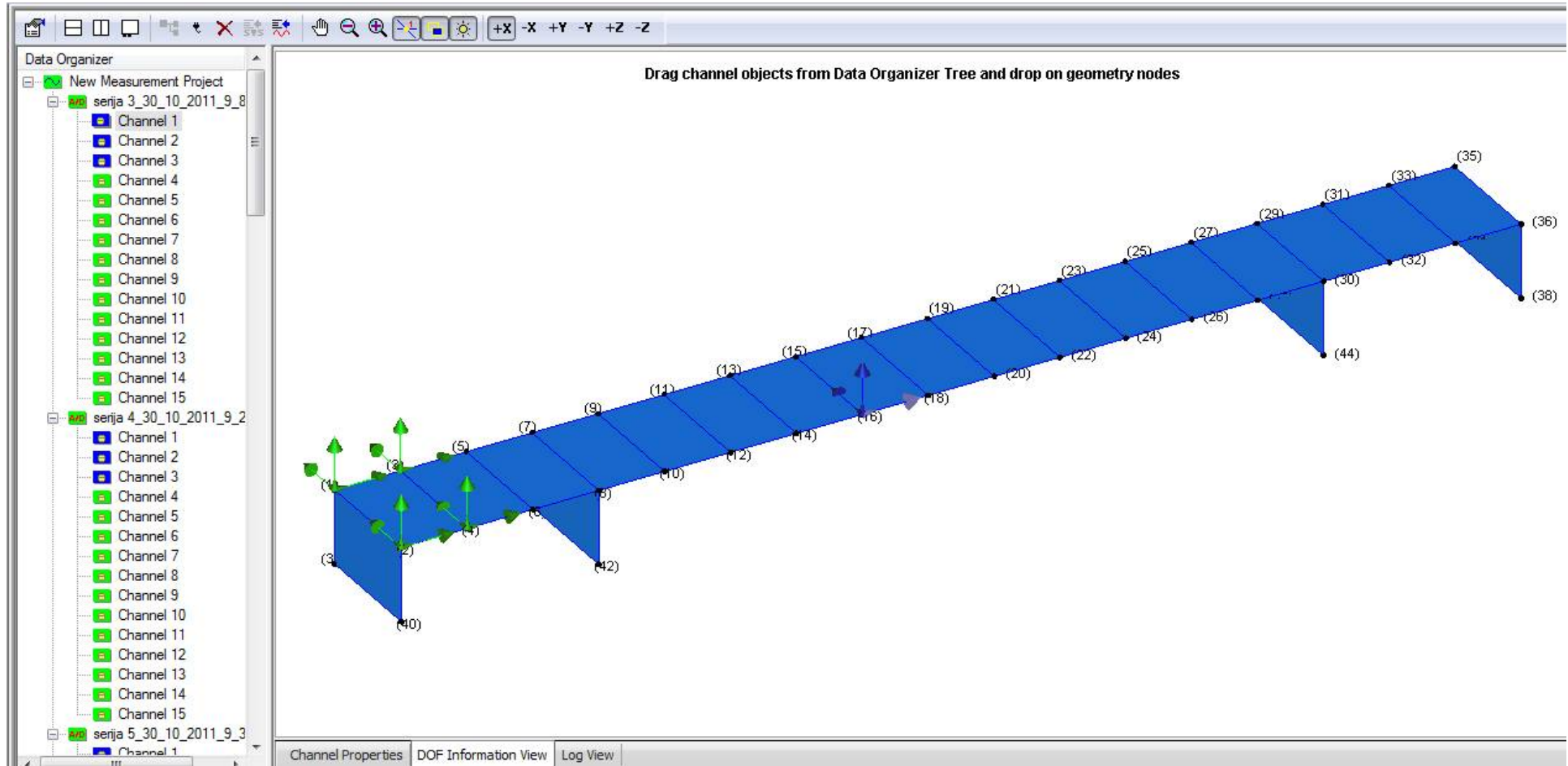
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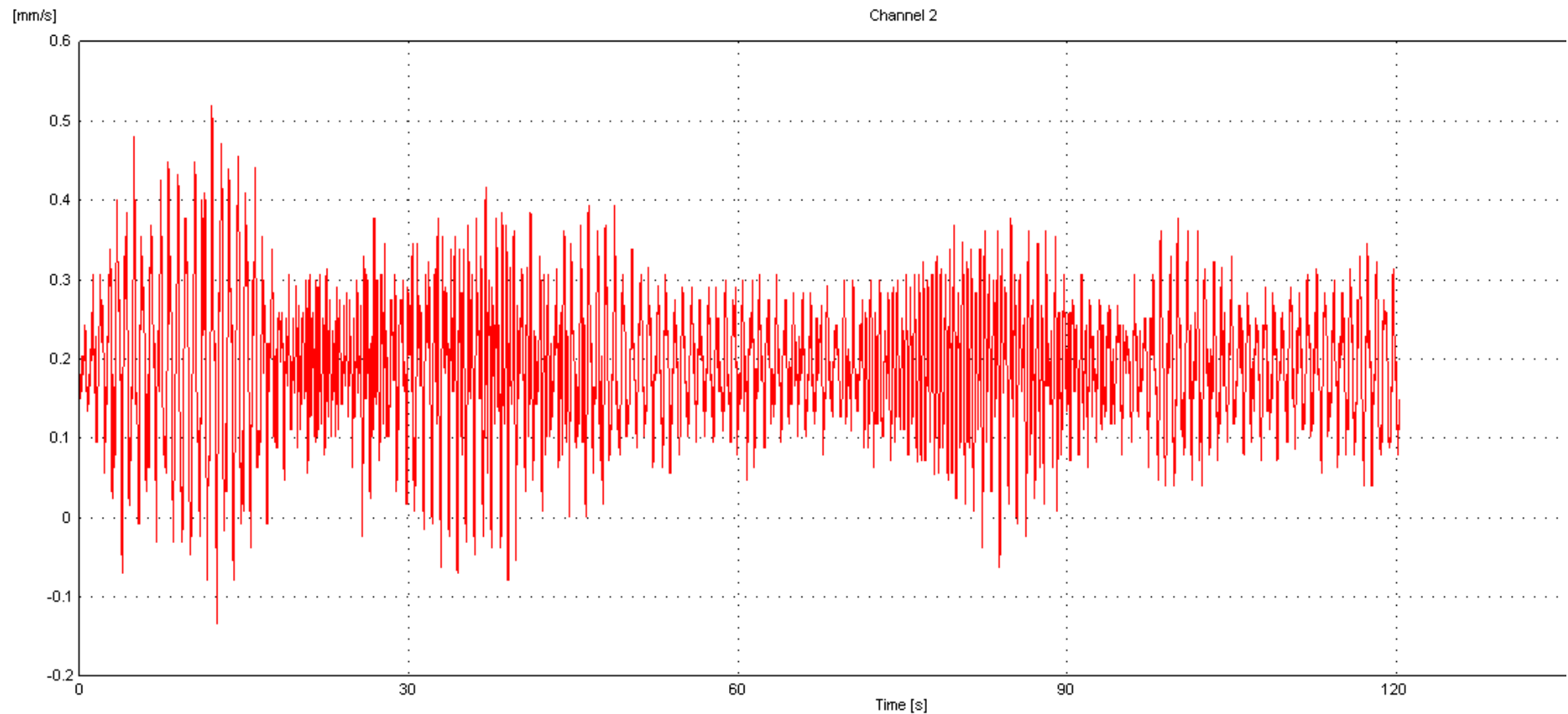


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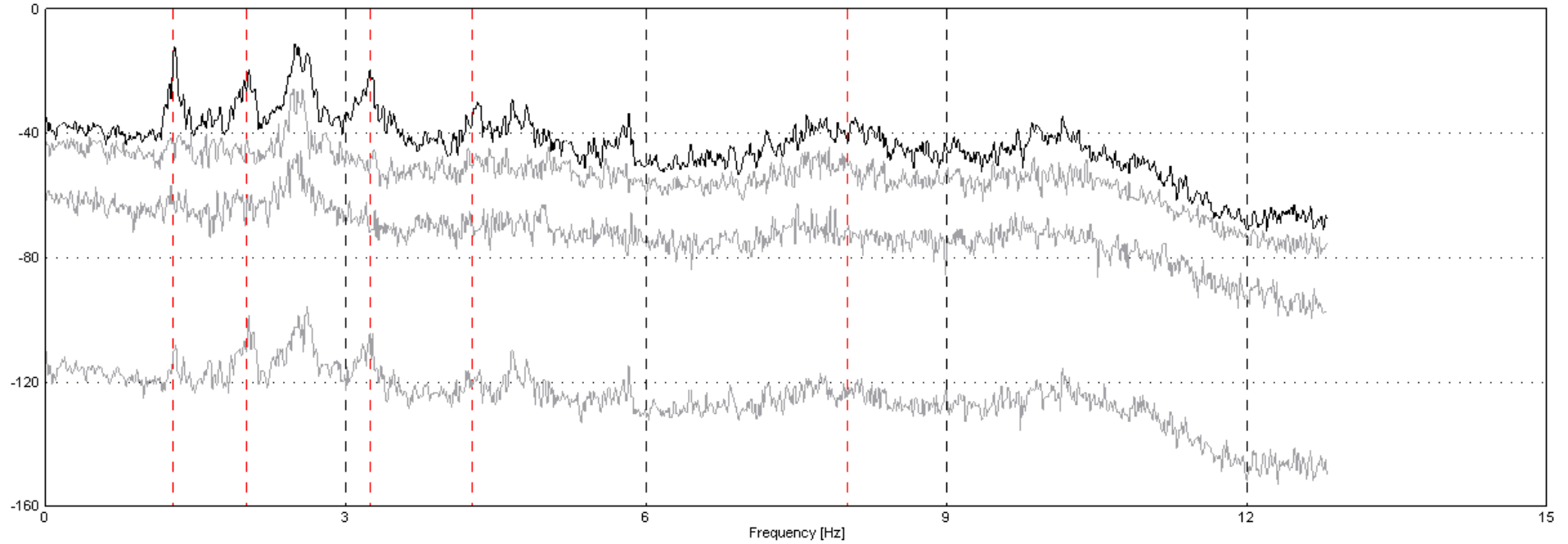
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# ARTEMIS

[dB] (1 mm/s)<sup>2</sup> / Hz

Frequency Domain Decomposition - Peak Picking  
Singular Values of Spectral Density Matrices  
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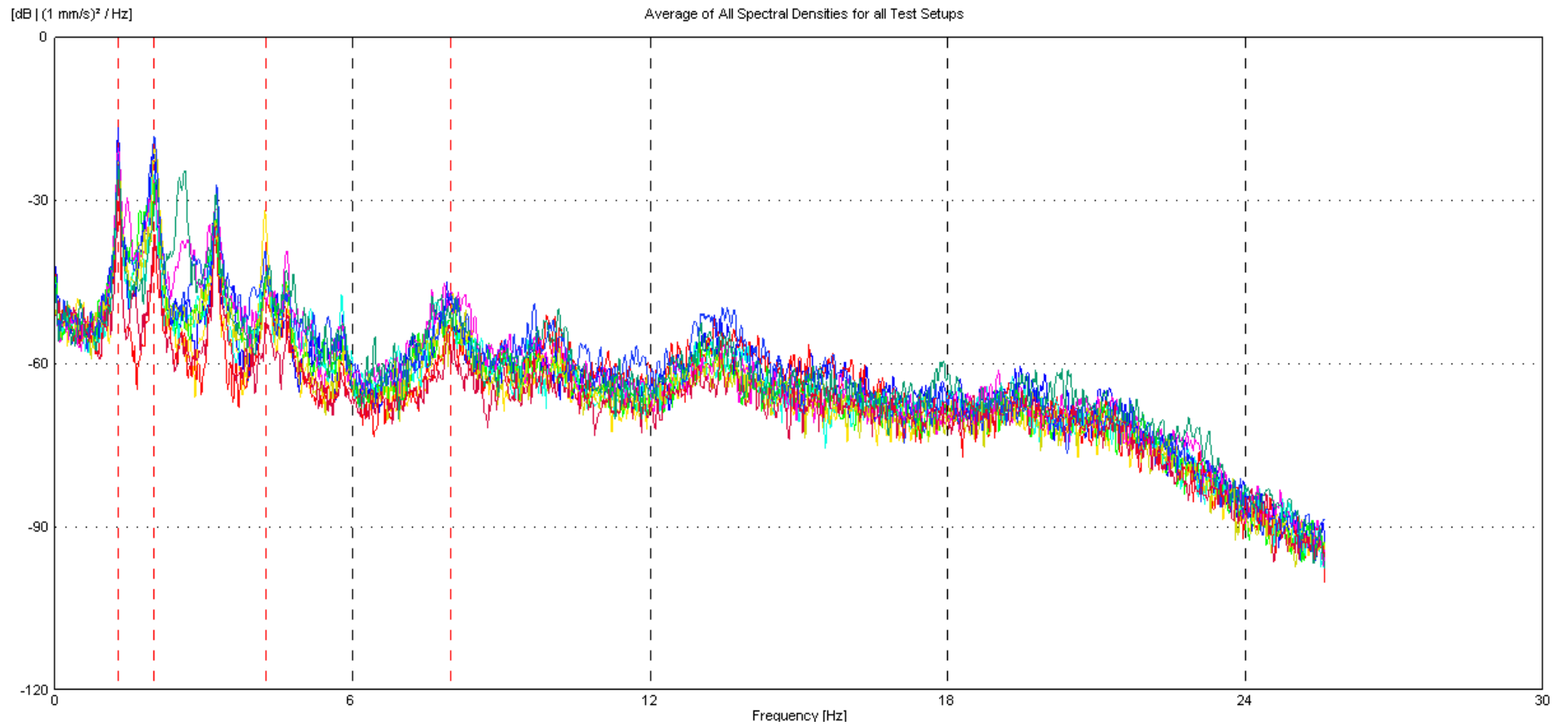


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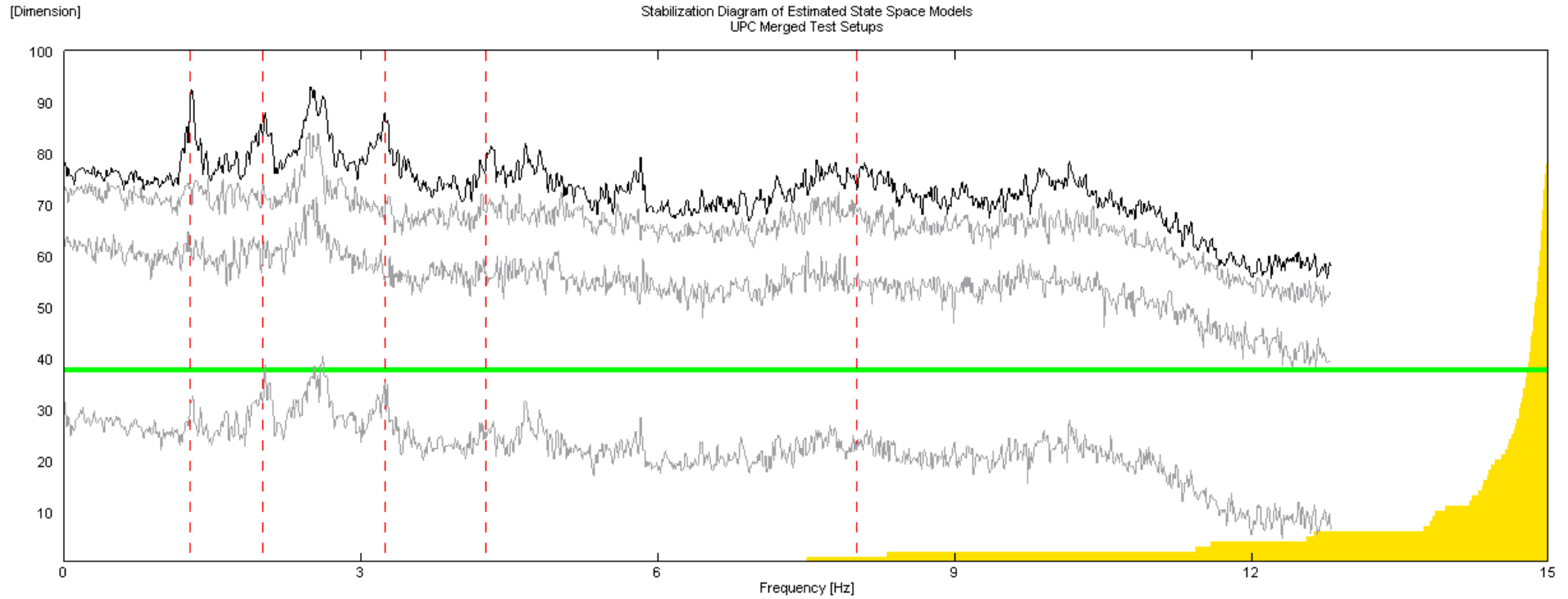


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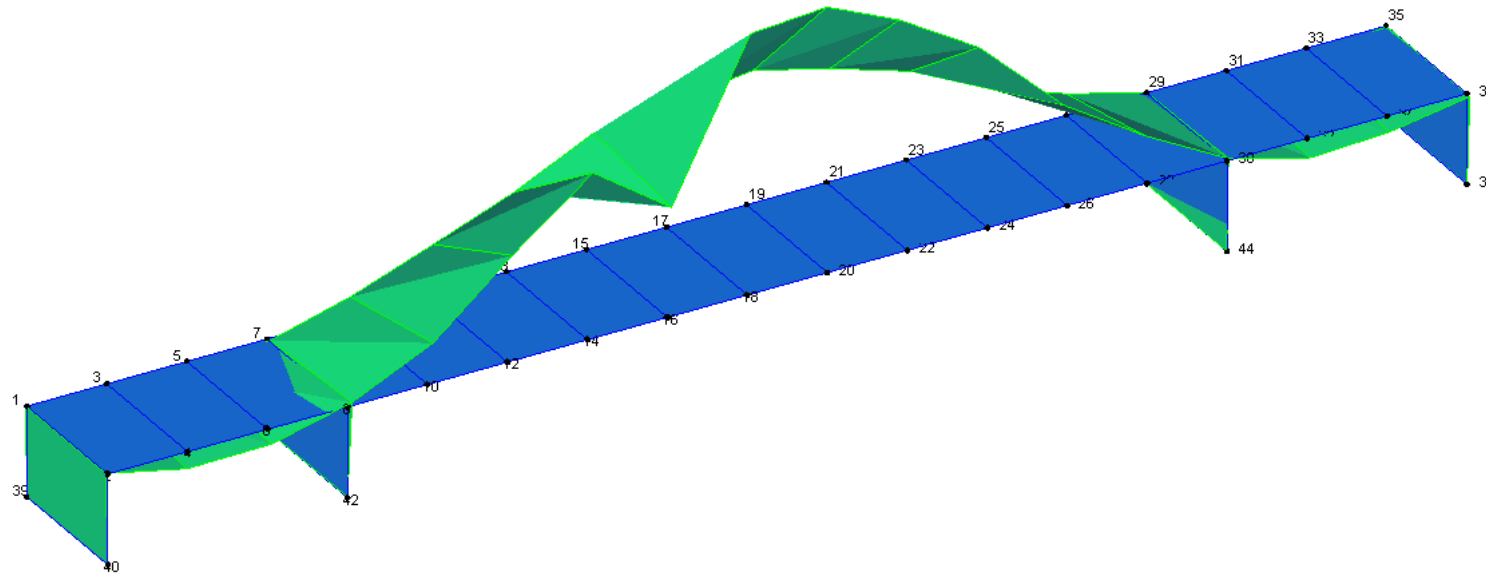


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# 1st vertical mode



## Modal Values

Frequency = 1.273 Hz

Damping = 0.9538 %

## Display Settings

Rotation Horz. = 30°

Rotation Vert. = 29°

Translation Horz. = 0

Translation Vert. = 0

Zoom Level = 140%

Amplitude = 100%

Phase Angle = 125°

Frames per Sec. = 0

## Undeformed Geometry

— Lines

■ Surfaces

## Deformed Geometry

— Lines

■ Surfaces

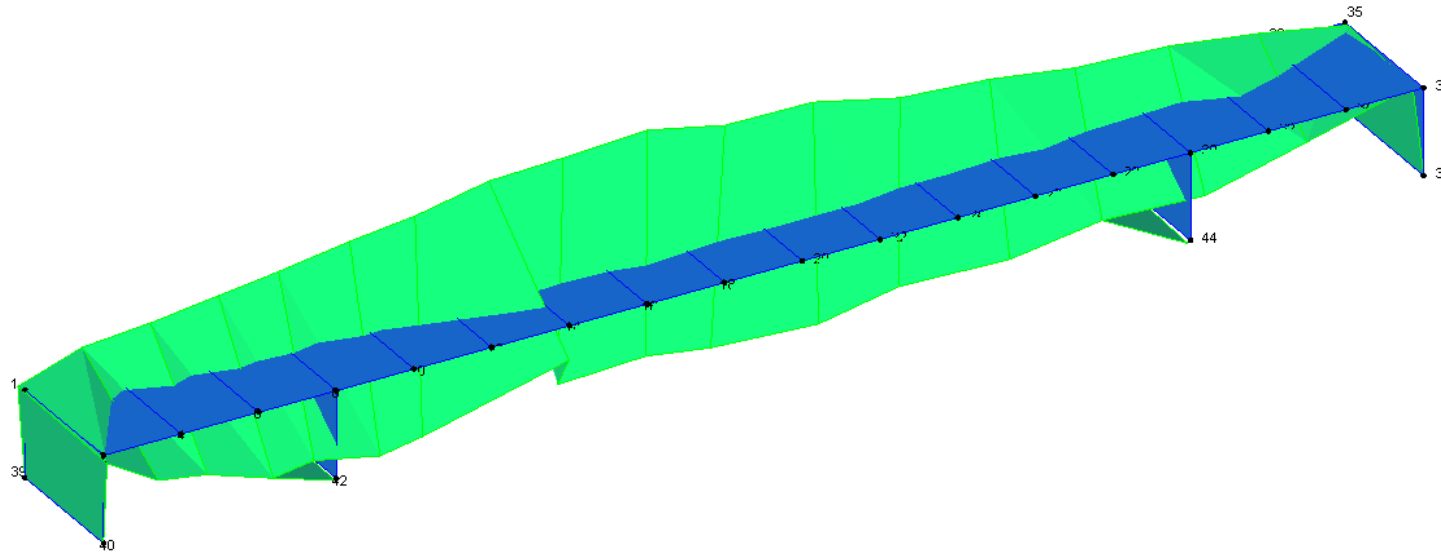


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# 1st transverse mode



## Modal Values

Frequency = 2 Hz  
Damping = 1.516 %

## Display Settings

Rotation Horz. = 30°  
Rotation Vert. = 29°  
Translation Horz. = 0  
Translation Vert. = 0  
Zoom Level = 140%  
Amplitude = 100%  
Phase Angle = 306°  
Frames per Sec. = 0

## Undeformed Geometry

— Lines  
■ Surfaces

## Deformed Geometry

— Lines  
■ Surfaces



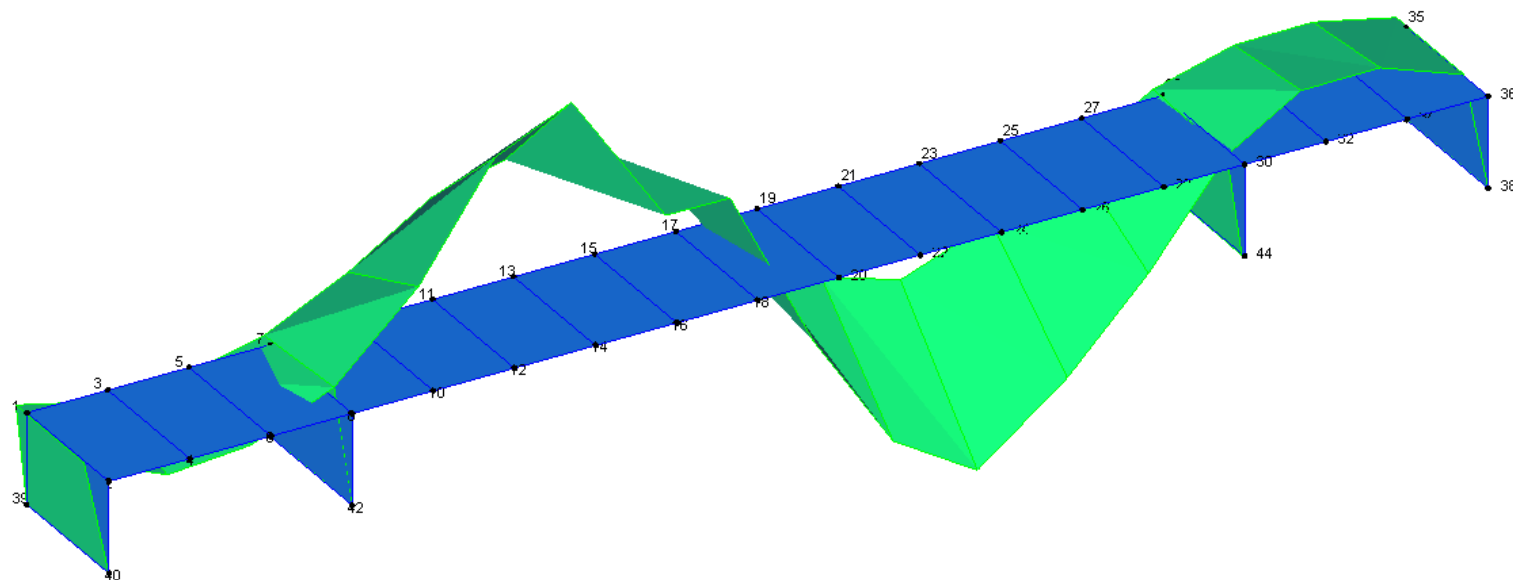
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## 2nd vertical mode



### Modal Values

Frequency = 3.235 Hz  
Damping = 1.094 %

### Display Settings

Rotation Horz. = 30°  
Rotation Vert. = 29°  
Translation Horz. = 0  
Translation Vert. = 0  
Zoom Level = 140%  
Amplitude = 100%  
Phase Angle = 306°  
Frames per Sec. = 0

### Undeformed Geometry

— Lines  
■ Surfaces

### Deformed Geometry

— Lines  
■ Surfaces

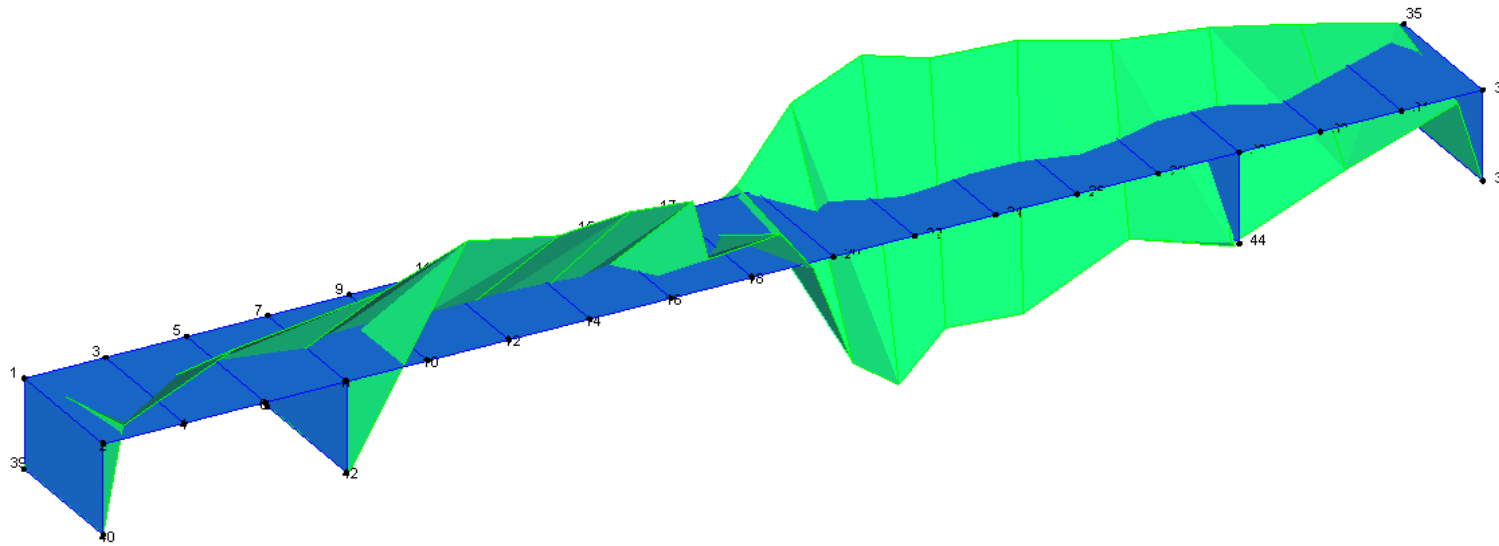


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## 2nd transverse mode



### Modal Values

Frequency = 4.65 Hz

Damping = [None]

### Display Settings

Rotation Horz. = 29°

Rotation Vert. = 28°

Translation Horz. = 0

Translation Vert. = 0

Zoom Level = 140%

Amplitude = 100%

Phase Angle = 125°

Frames per Sec. = 0

### Undeformed Geometry

— Lines

■ Surfaces

### Deformed Geometry

— Lines

■ Surfaces



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## Finite Element Models (FEMs)

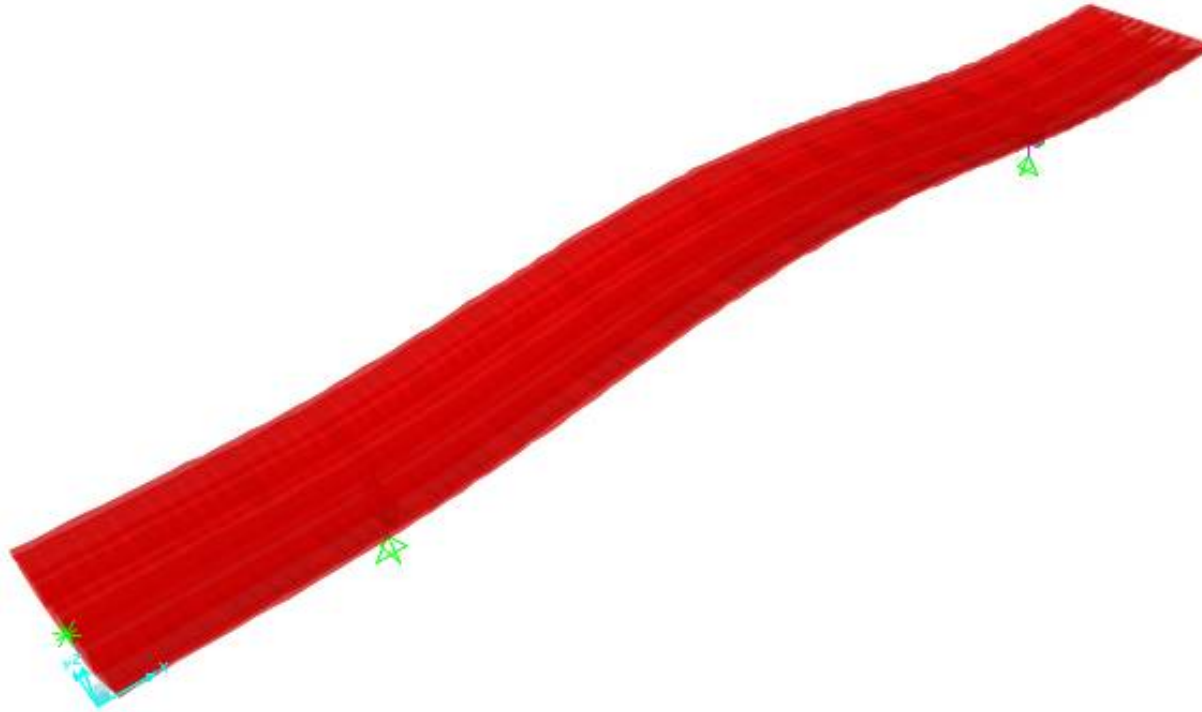


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## Mathematically identified 1<sup>st</sup> vertical mode



Modes	AVM	AM3
First vertical	1.273	1.273
First transverse	2.000	1.921
Second vertical	3.235	3.542
Second transverse	4.65	5.852

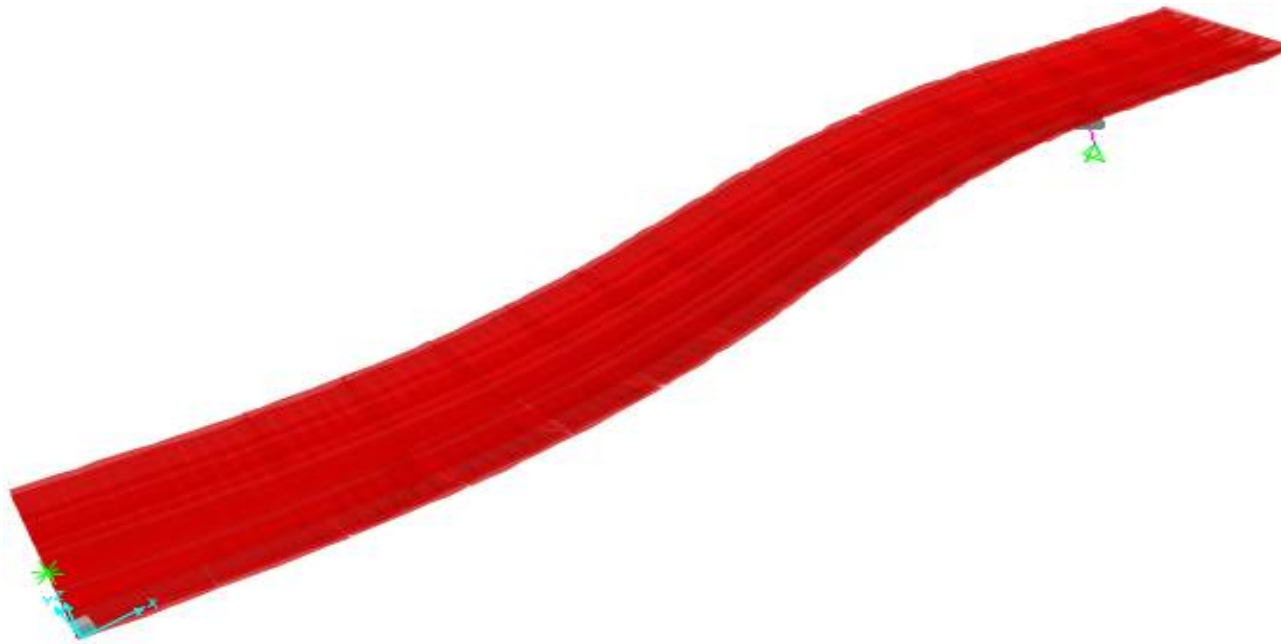


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## Mathematically identified 2nd transverse mode



Modes	AVM	AM3
First vertical	1.273	1.273
First transverse	2.000	1.921
Second vertical	3.235	3.542
Second transverse	4.65	5.852

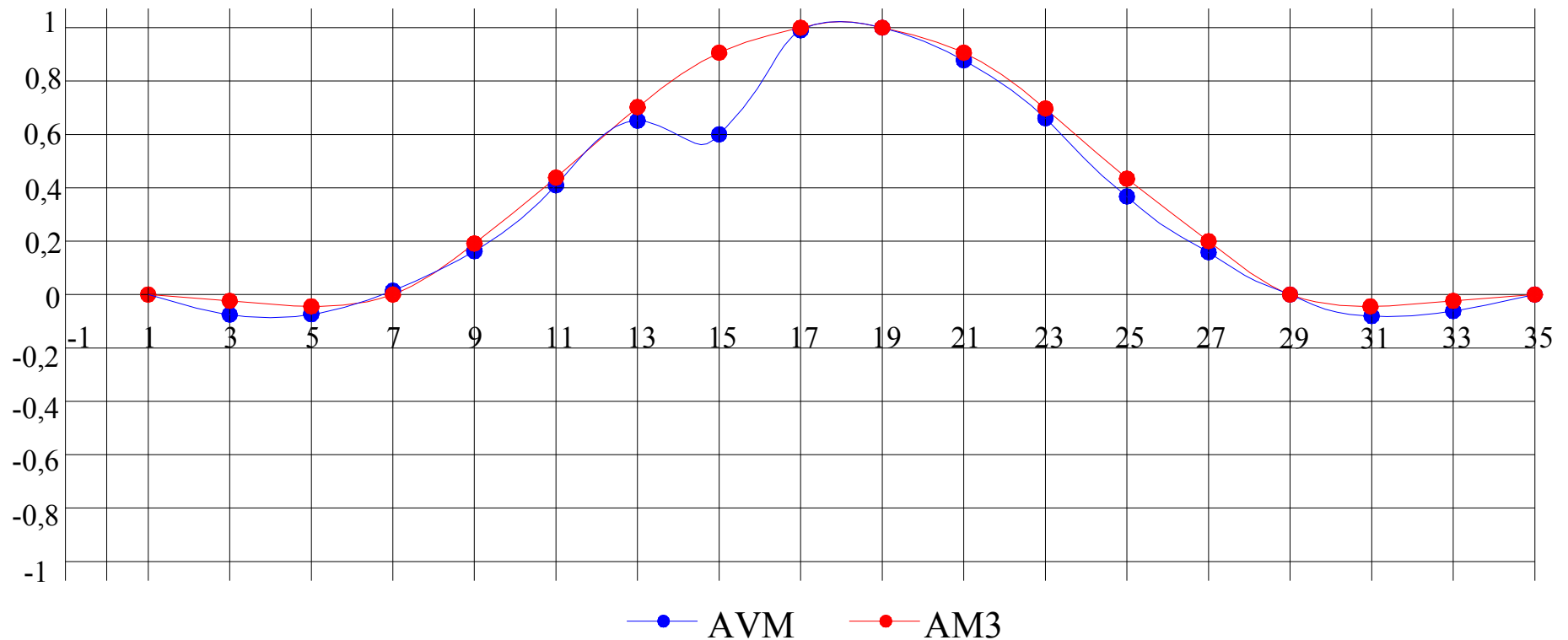
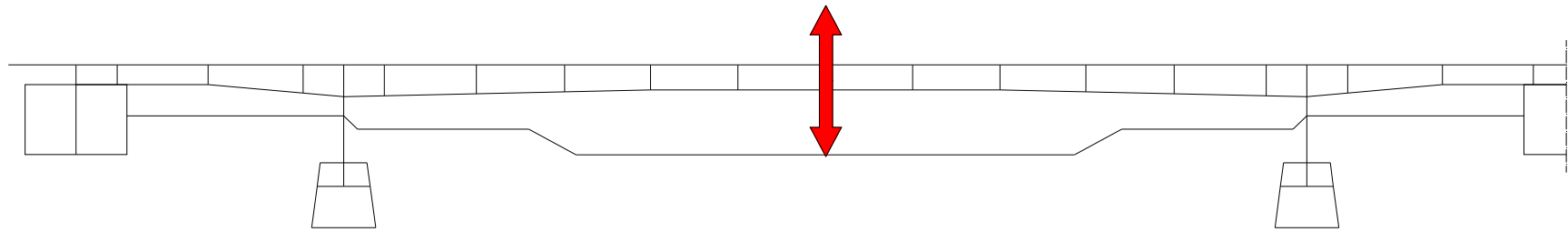


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# Experimentally and mathematically identified first vertical mode shapes

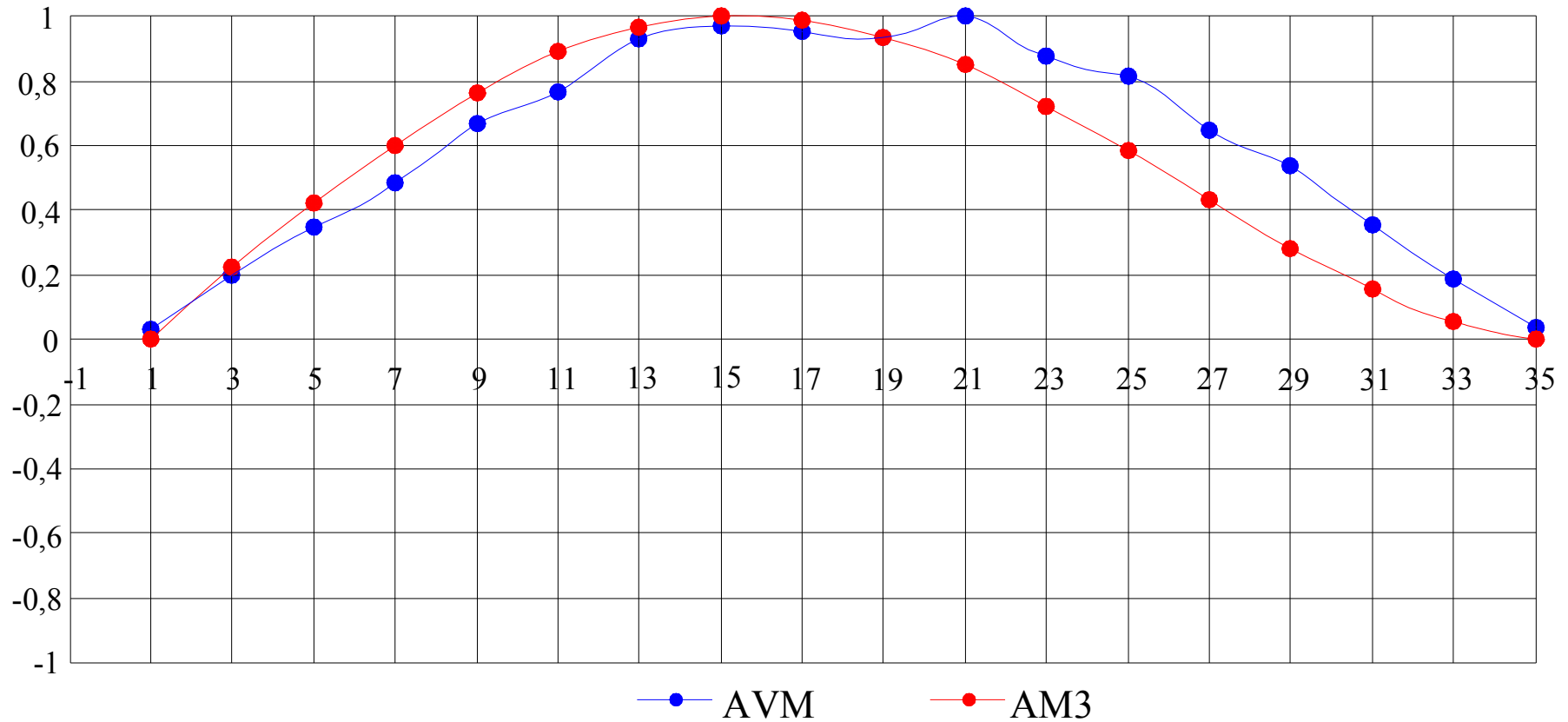
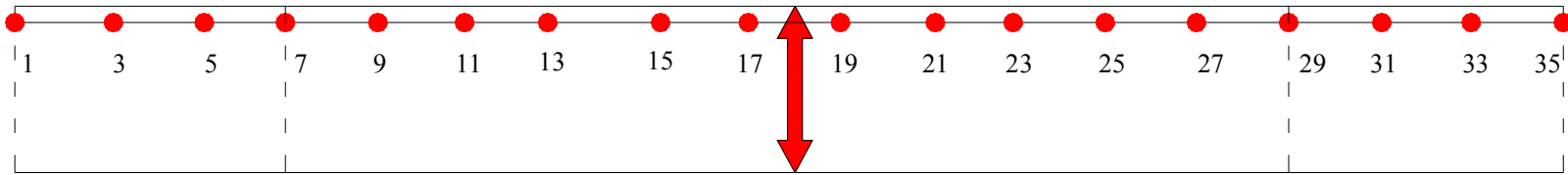


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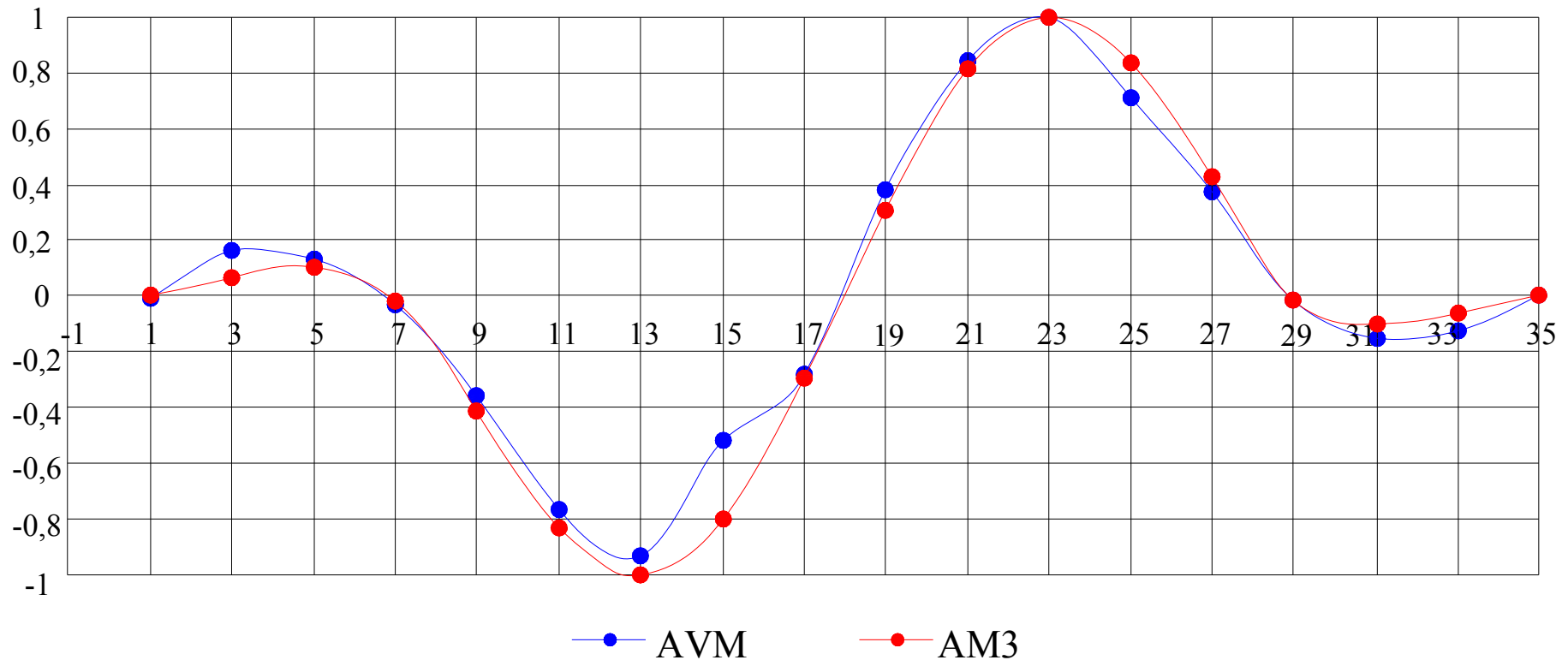
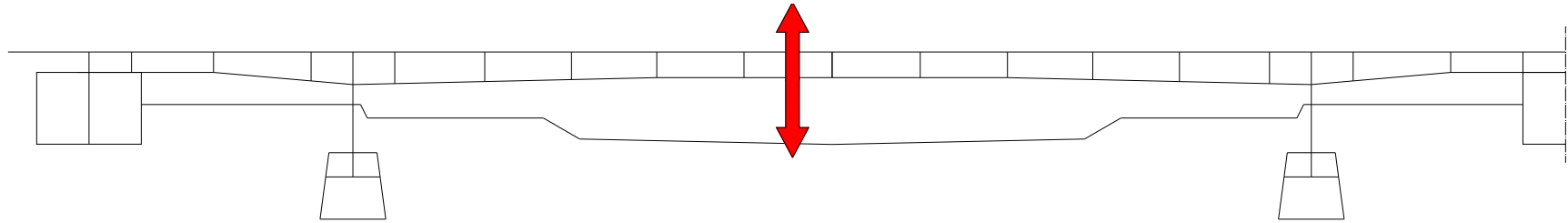
# Experimentally and mathematically identified first transverse mode shapes



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# Experimentally and mathematically identified second vertical mode shapes



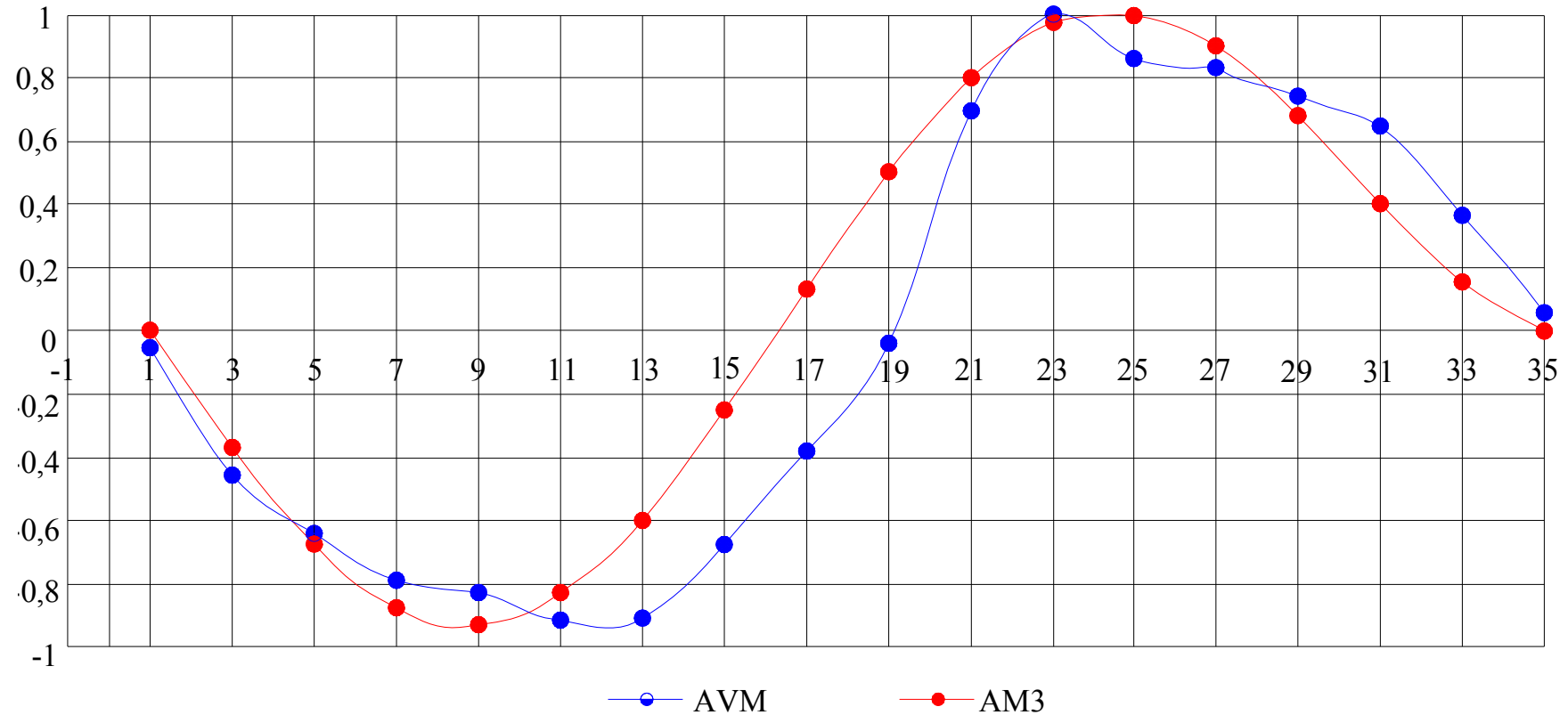
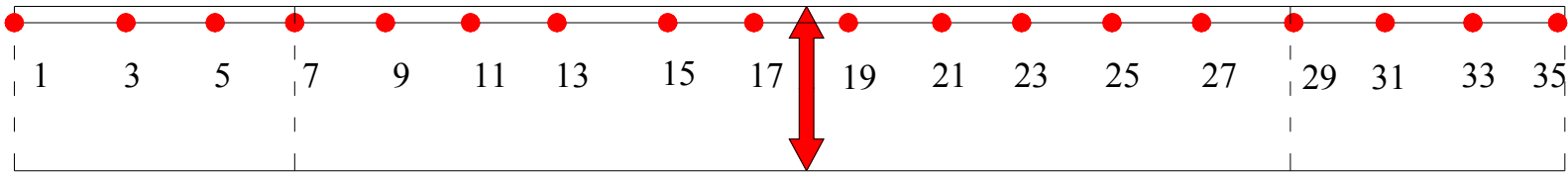
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## Experimentally and mathematically identified second transverse mode shapes



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## ***CASE STUDY 3 – THE CABLE - STAYED BRIDGE IN TUZLA***

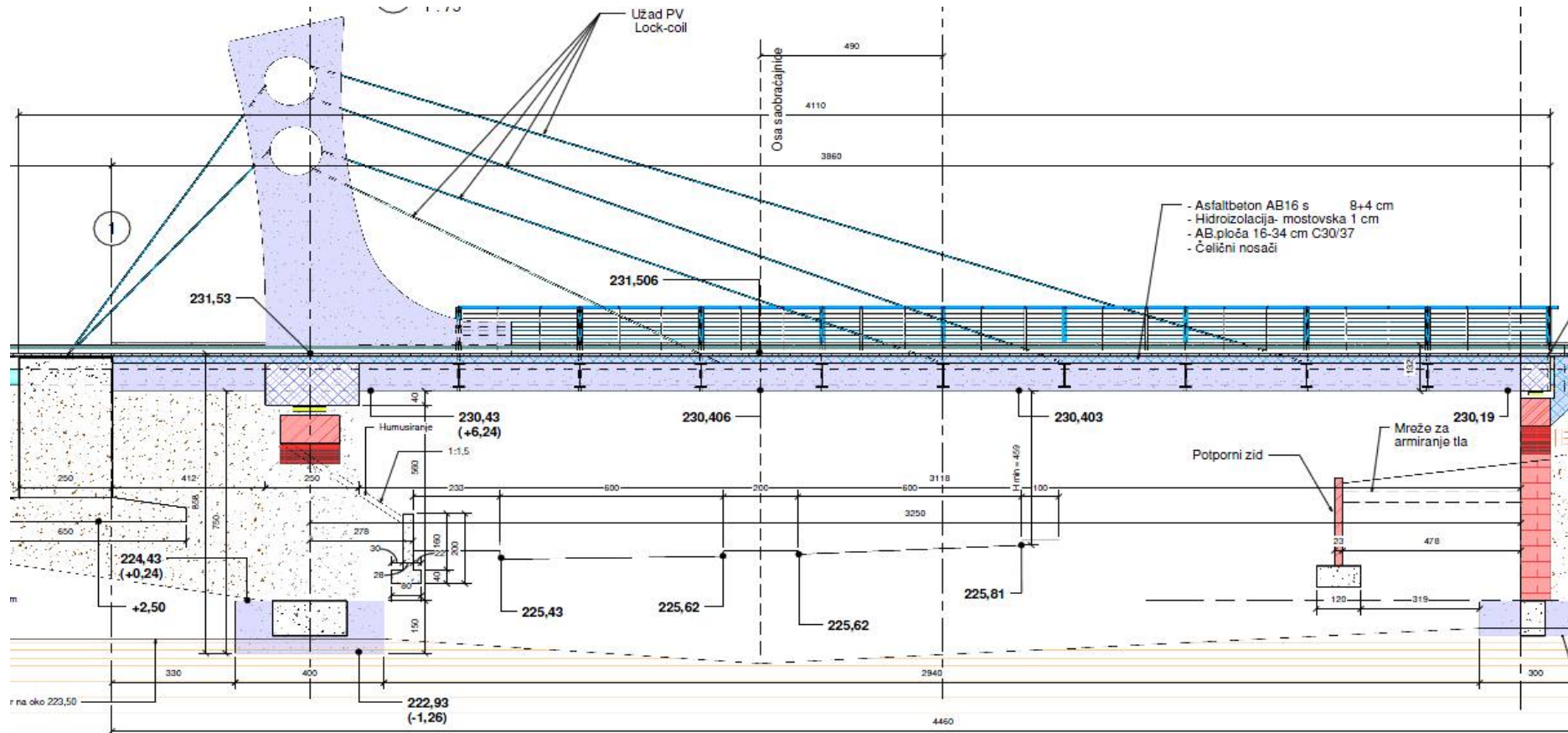


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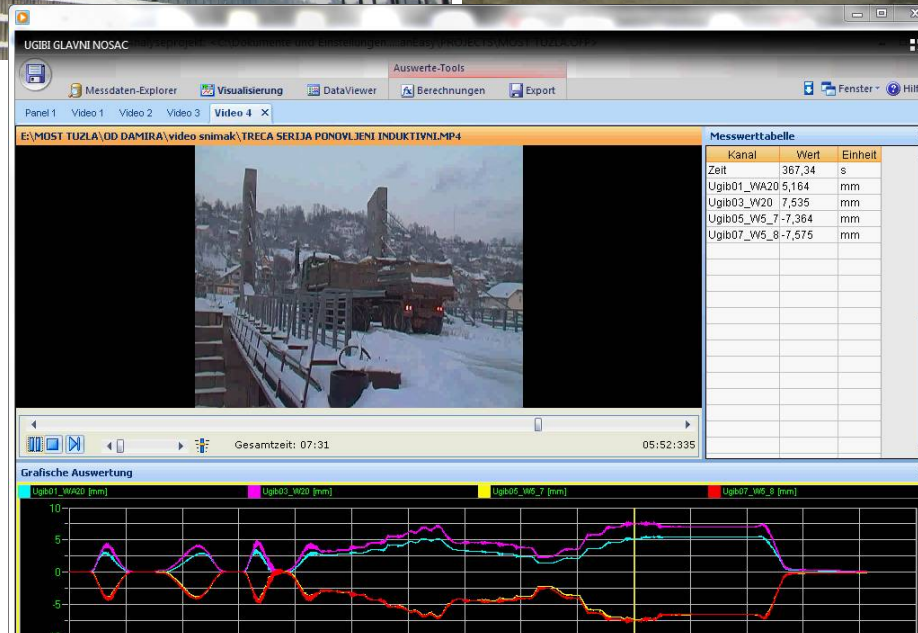
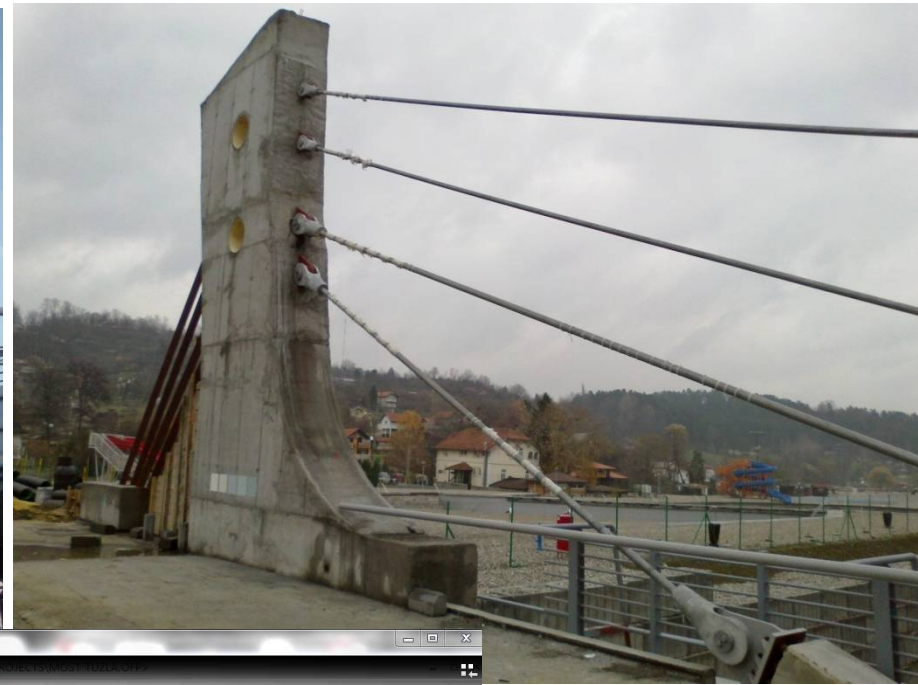
## Elevation and cross-sections of the bridge



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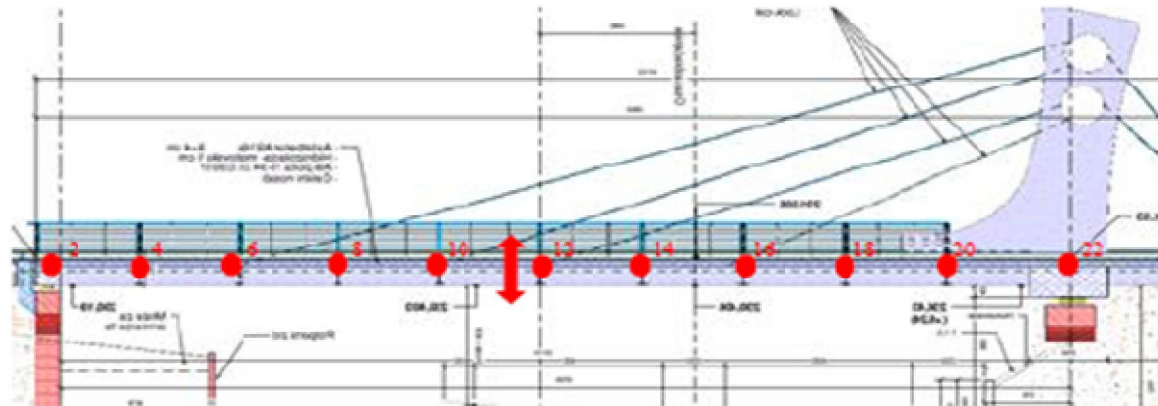
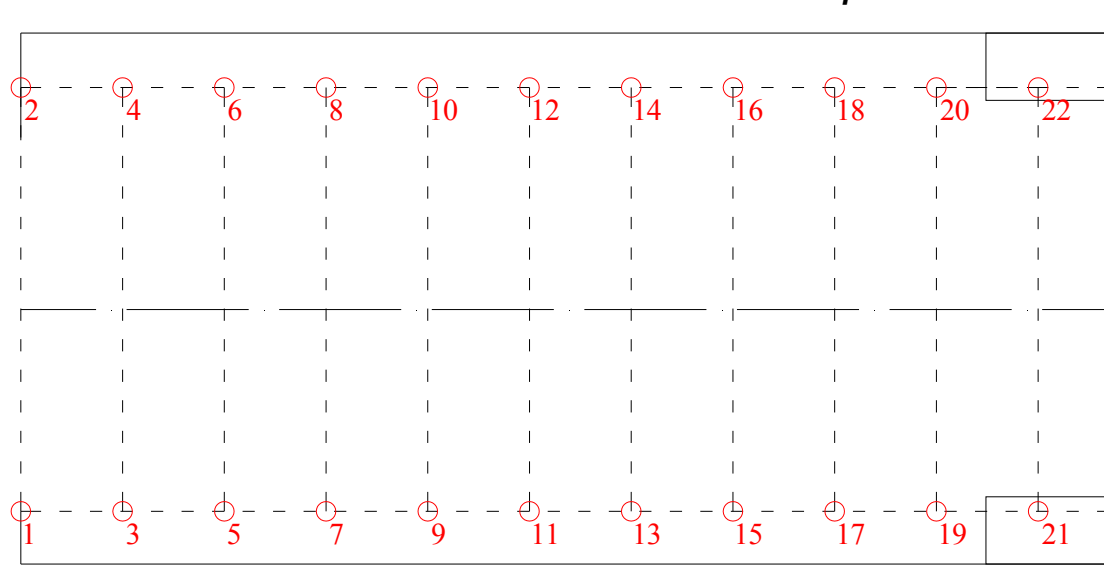


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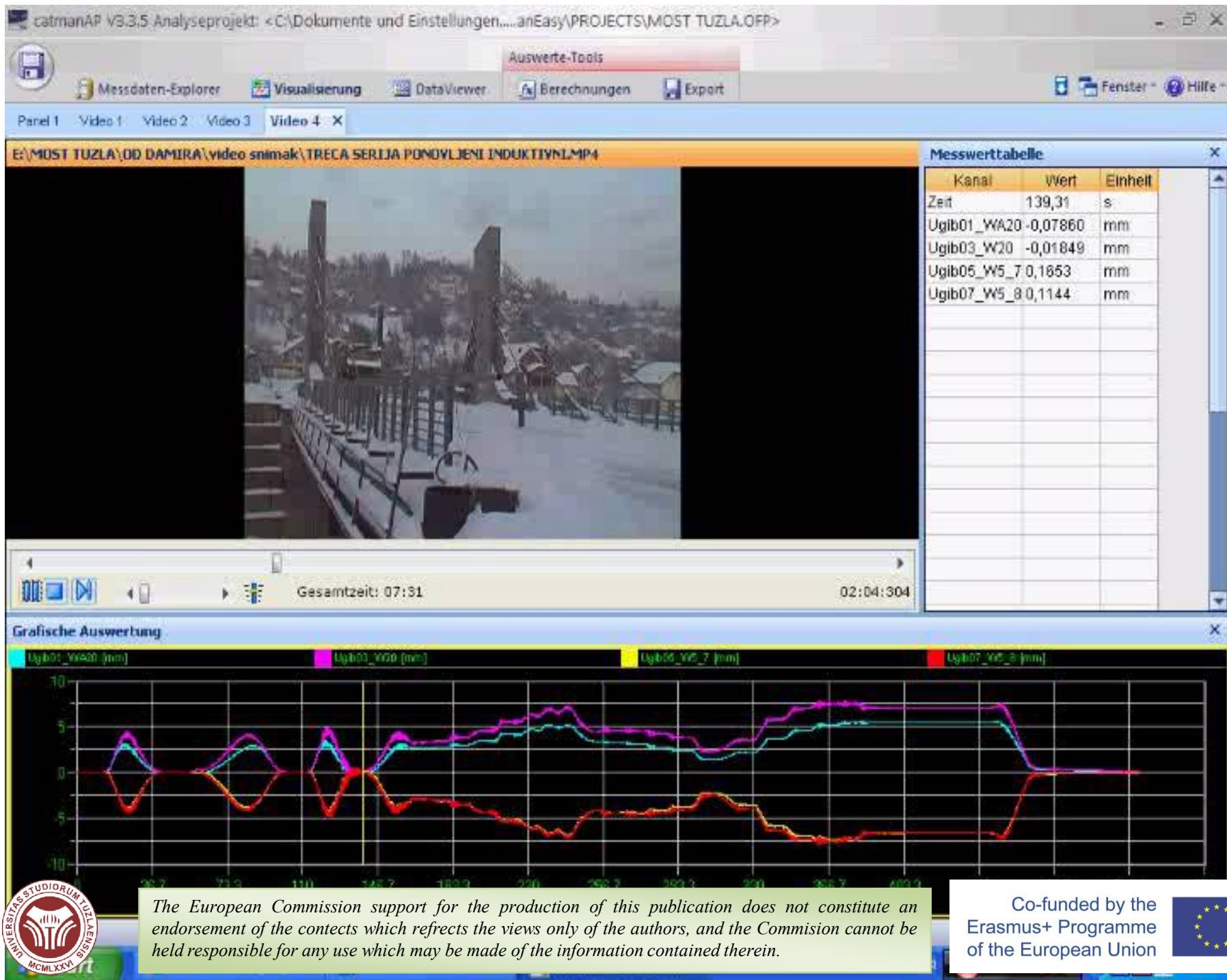
## Measurements setup



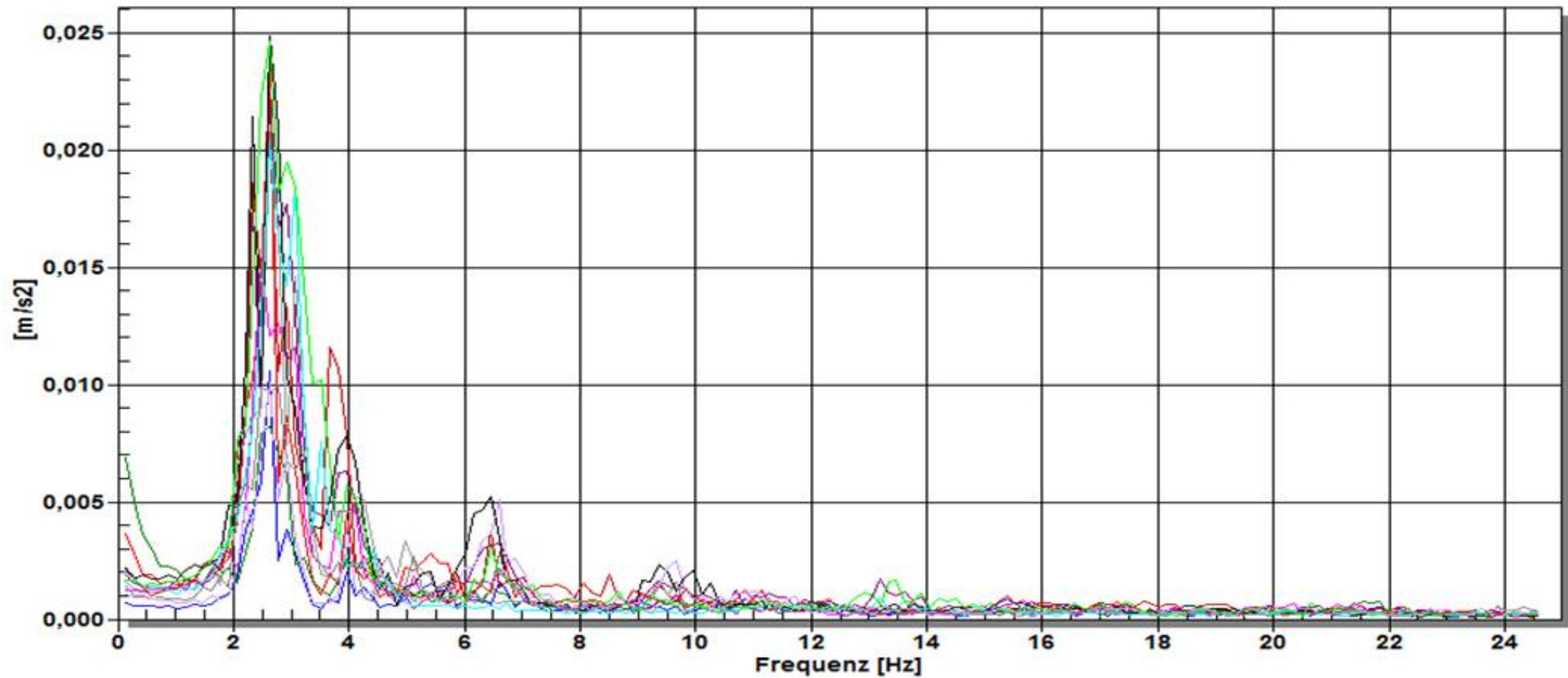
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# Frequency spectrum

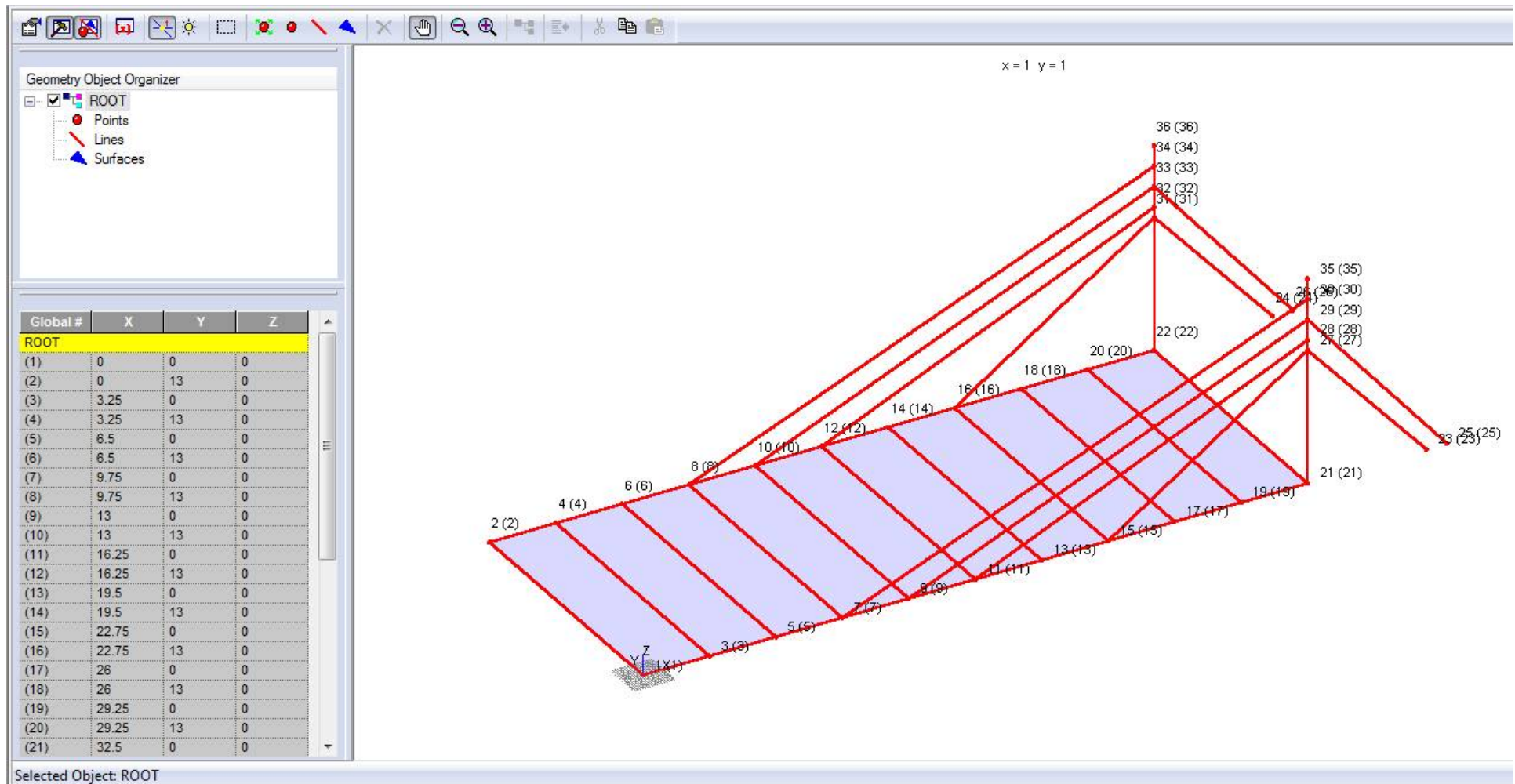


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# ARTEMIS



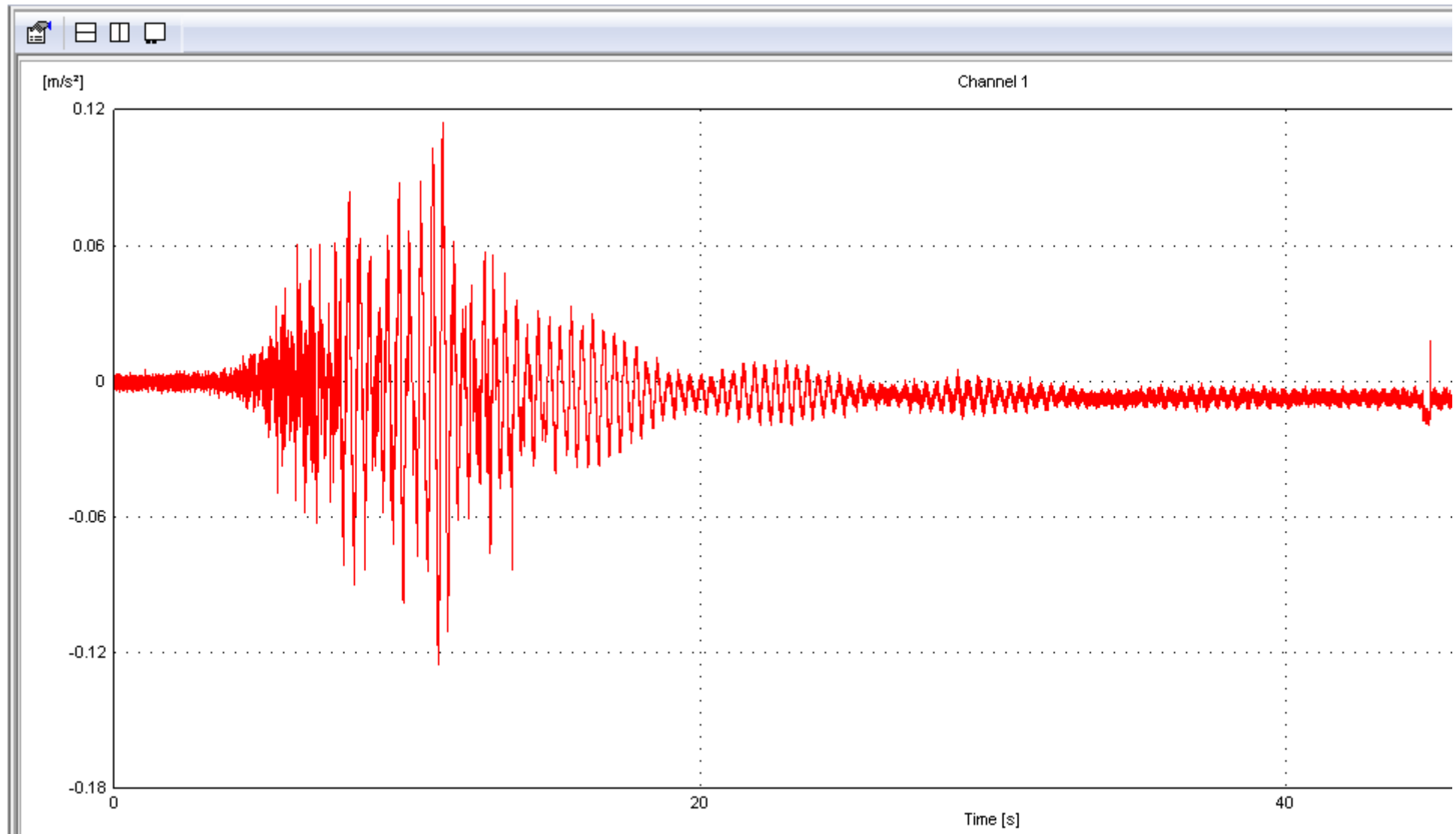
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# ARTEMIS

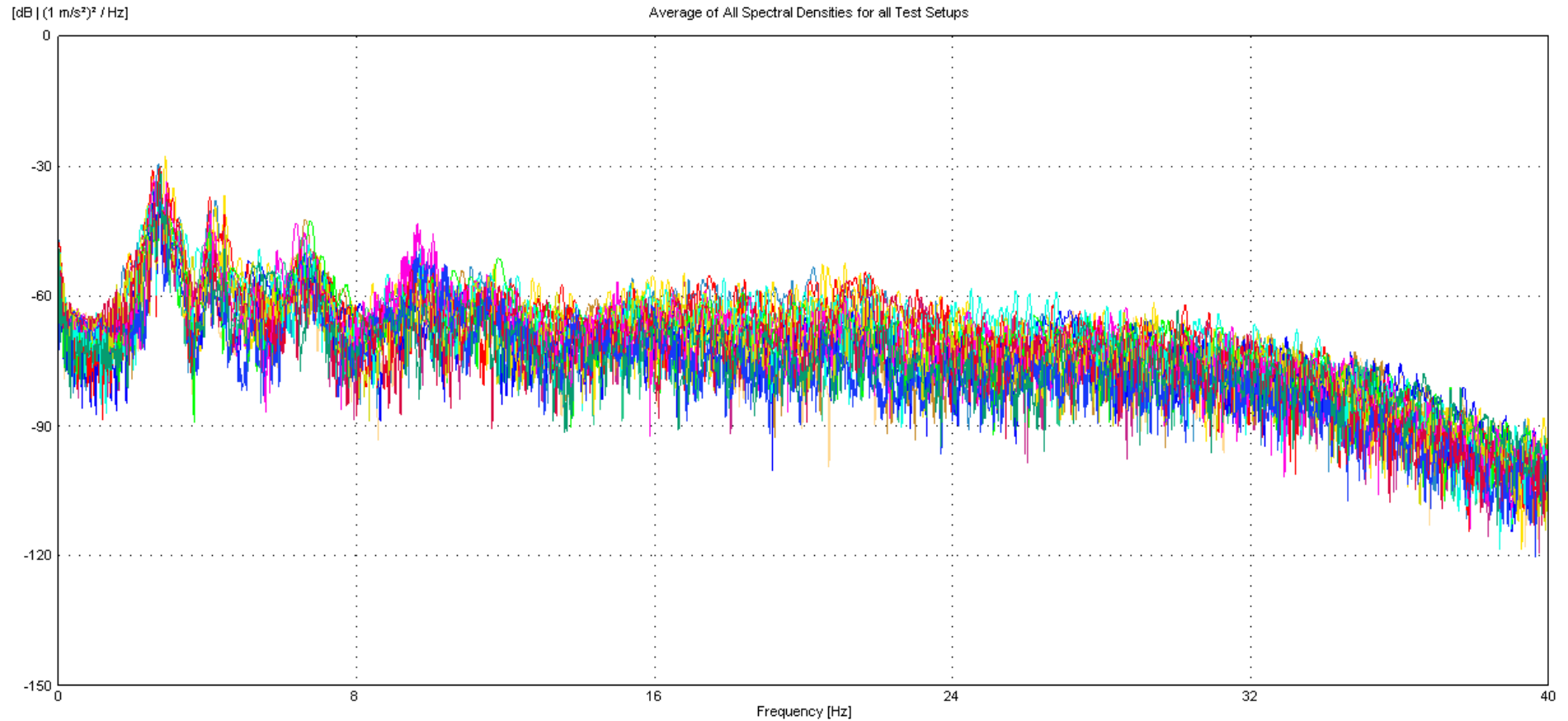


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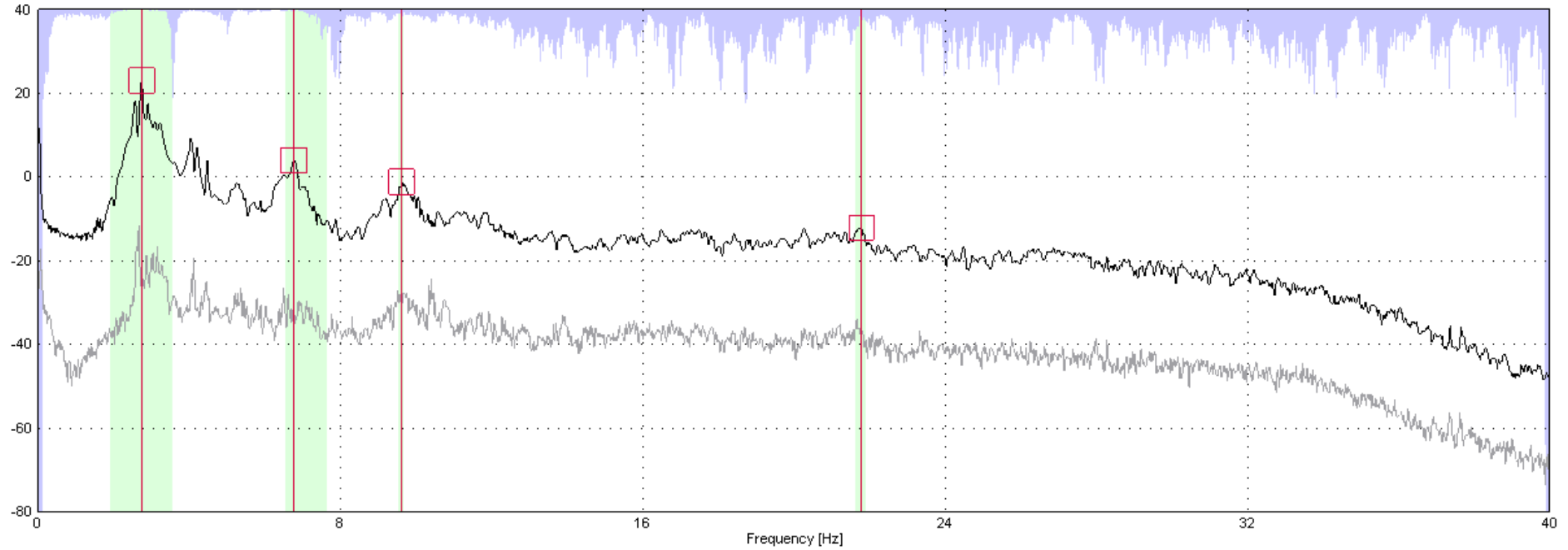
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# ARTEMIS

[dB] (1 m/s<sup>2</sup>)<sup>2</sup> / Hz

Frequency Domain Decomposition - Peak Picking  
Average of the Normalized Singular Values of  
Spectral Density Matrices of all Test Setups



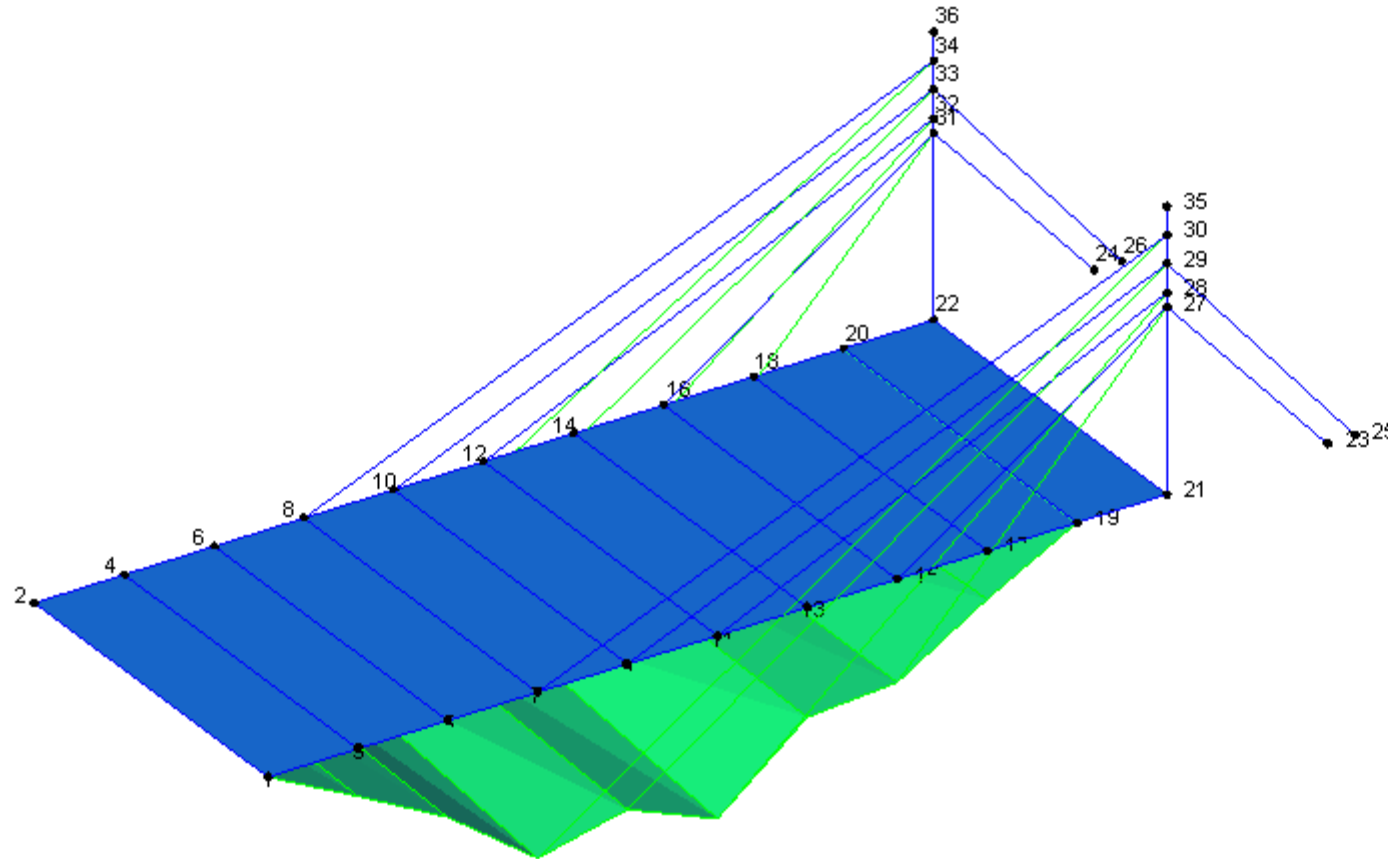
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# 1st mode

EFDD - Enhanced Frequency Domain Decomposition



## Modal Values

Frequency = 2.721 Hz

Damping = 0.5417 %

## Display Settings

Rotation Horz. = 33°

Rotation Vert. = 29°

Translation Horz. = 14

Translation Vert. = 1.2

Zoom Level = 130%

Amplitude = 100%

Phase Angle = 306°

Frames per Sec. = 0

## Undeformed Geometry

— Lines

■ Surfaces

## Deformed Geometry

— Lines

■ Surfaces



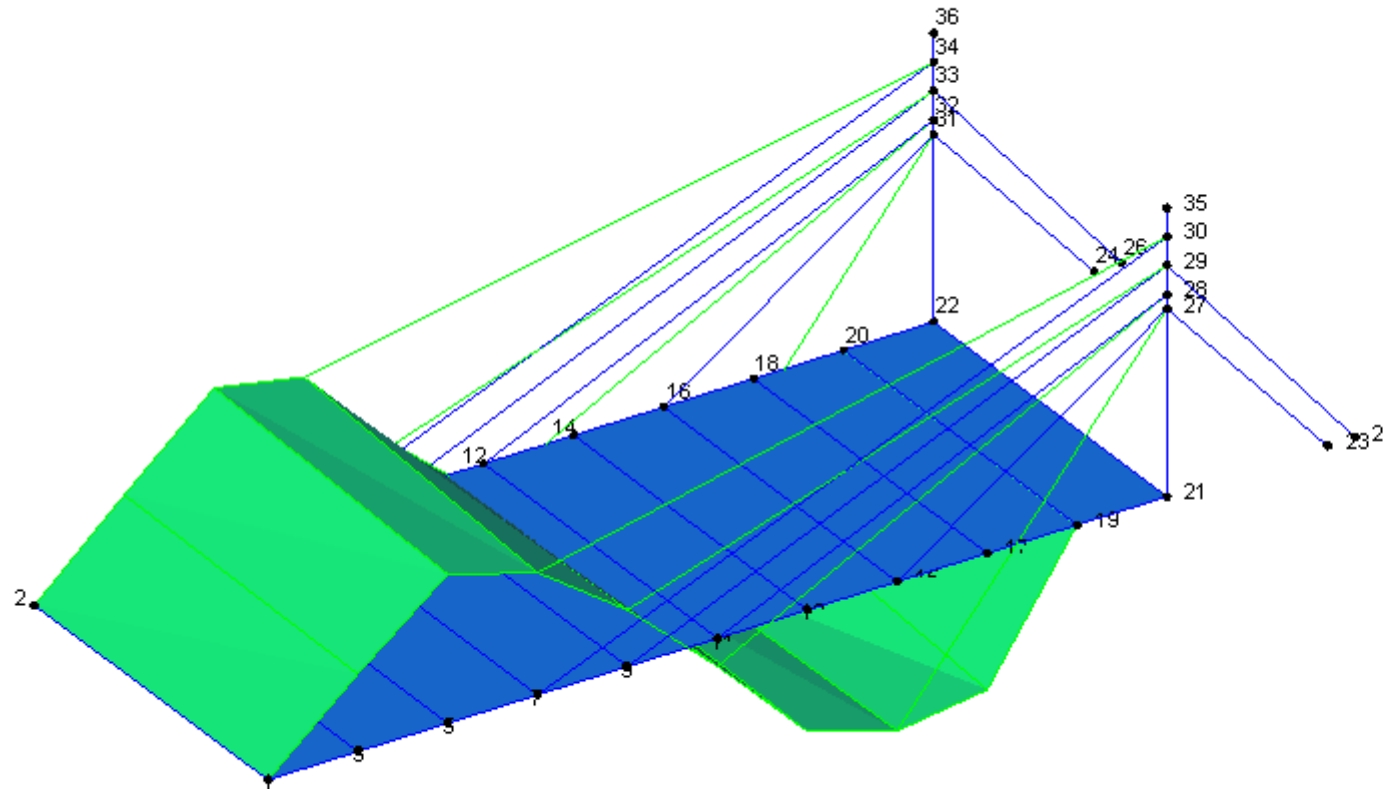
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## 2nd mode

EFDD - Enhanced Frequency Domain Decomposition



### Modal Values

Frequency = 6.562 Hz  
Damping = 1.112 %

### Display Settings

Rotation Horz. = 33°  
Rotation Vert. = 29°  
Translation Horz. = 14  
Translation Vert. = 1.2  
Zoom Level = 130%  
Amplitude = 100%  
Phase Angle = 306°  
Frames per Sec. = 0

### Undeformed Geometry

— Lines  
■ Surfaces

### Deformed Geometry

— Lines  
■ Surfaces



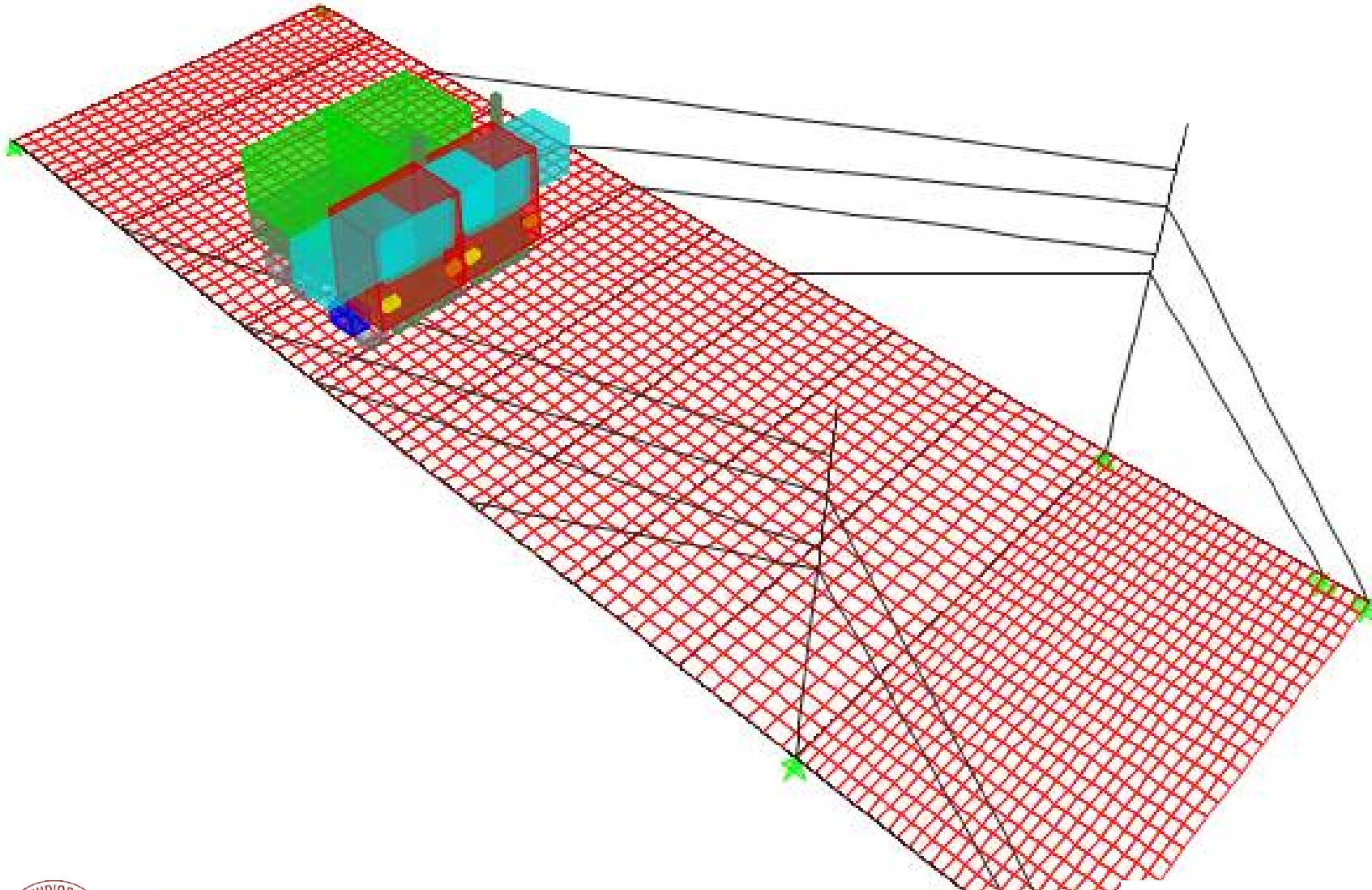
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# Finite Element Models (FEMs)

SAP2000    Filename: MOSTTU- 2.sdb    Deformed Shape    Case: VOZIL01IIV0ZIL02    Step 34

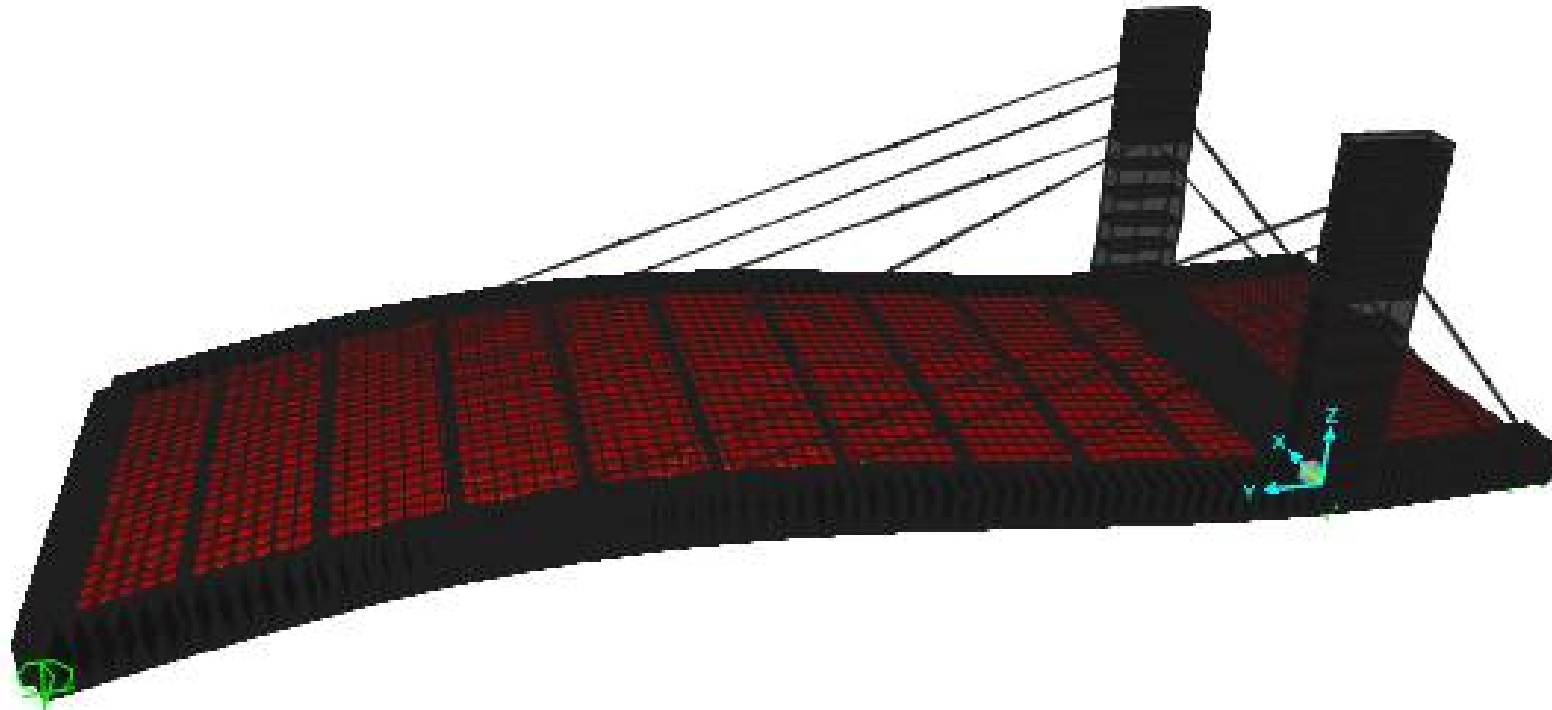


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# Mathematically identified 1<sup>st</sup> mode



Experimentally and mathematically identified modal frequencies (Hz)

MODES	AVM	AM4
FIRST MODE	2.719	2.727
SECOND MODE	6.790	6.512

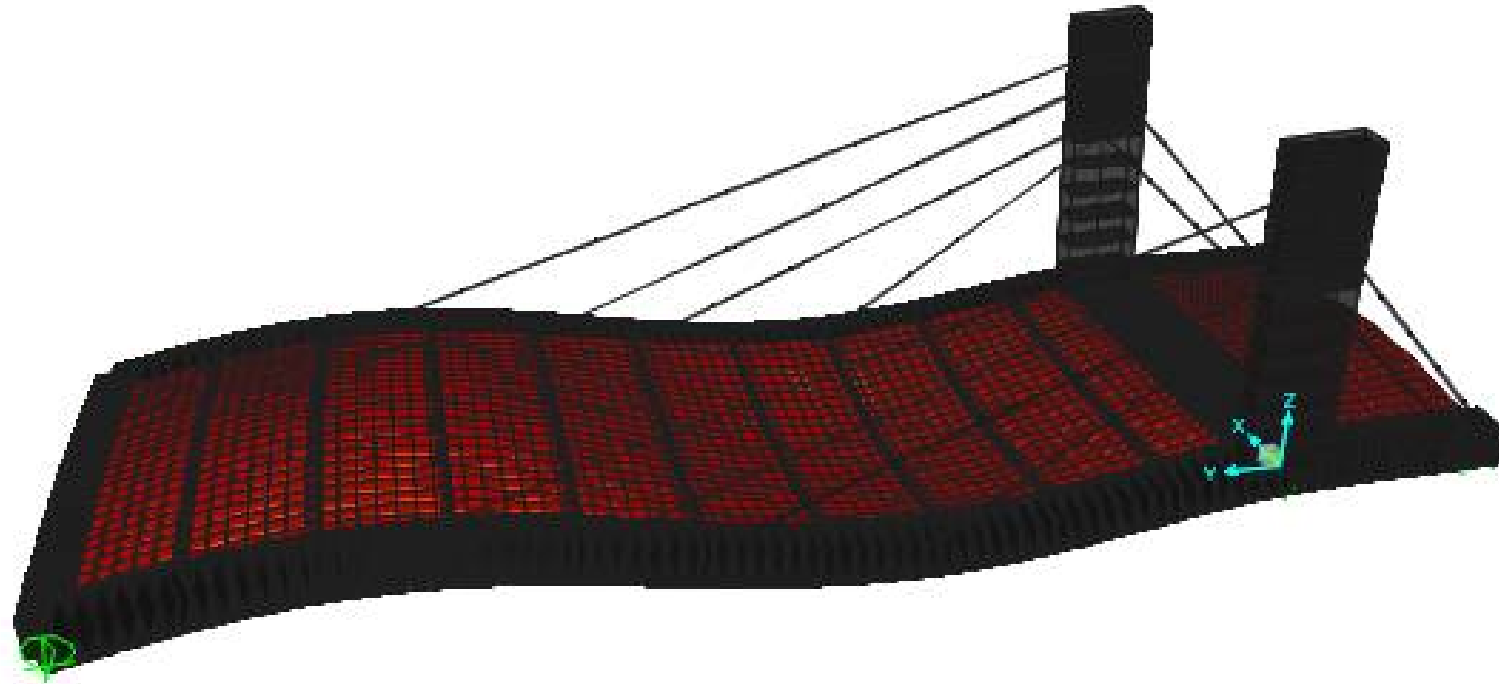


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## Mathematically identified 2nd mode



Experimentally and mathematically identified modal frequencies (Hz)

MODES	AVM	AM4
FIRST MODE	2.719	2.727
SECOND MODE	6.790	6.512



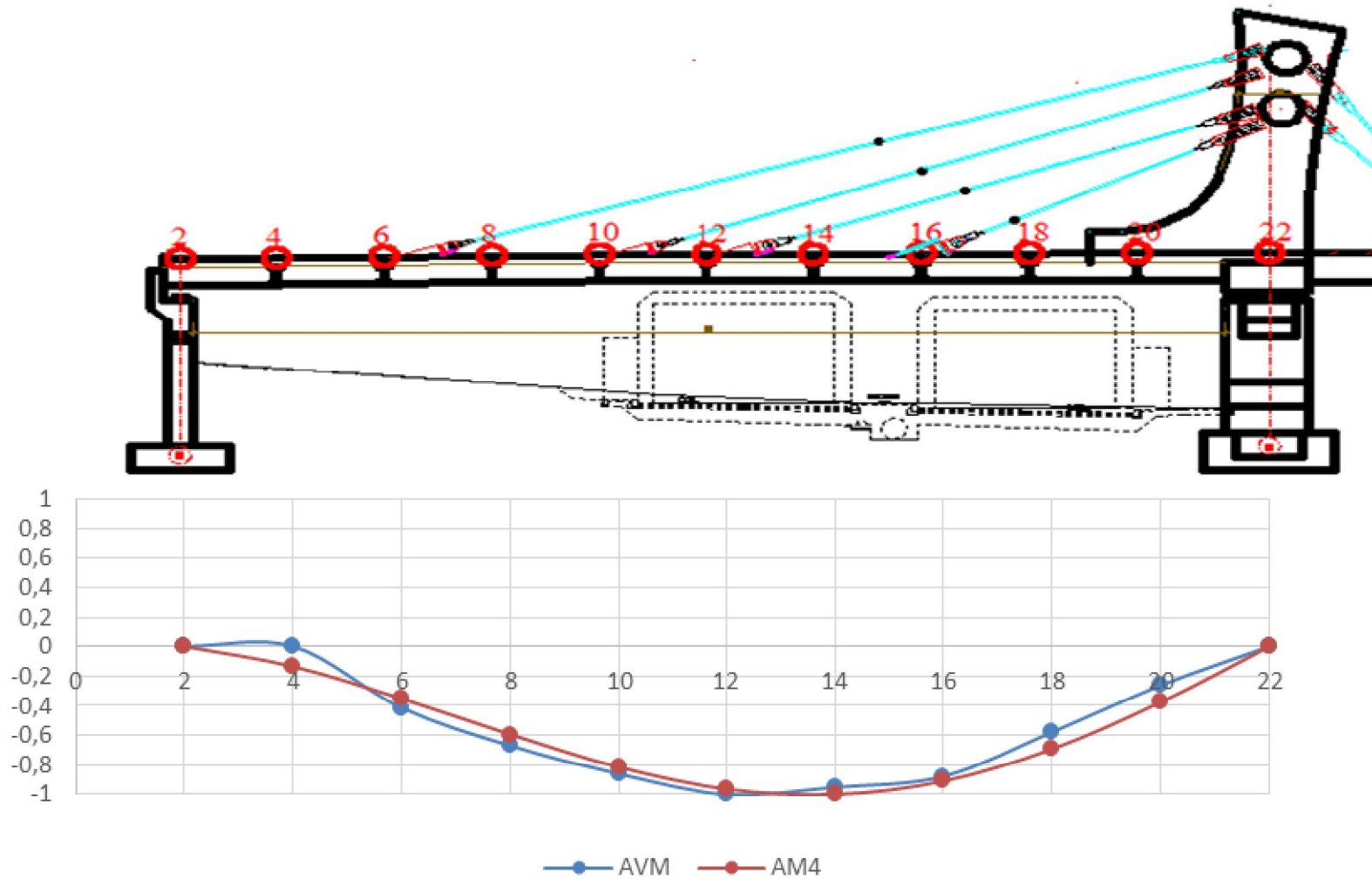
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## Experimentally and mathematically identified first mode shape

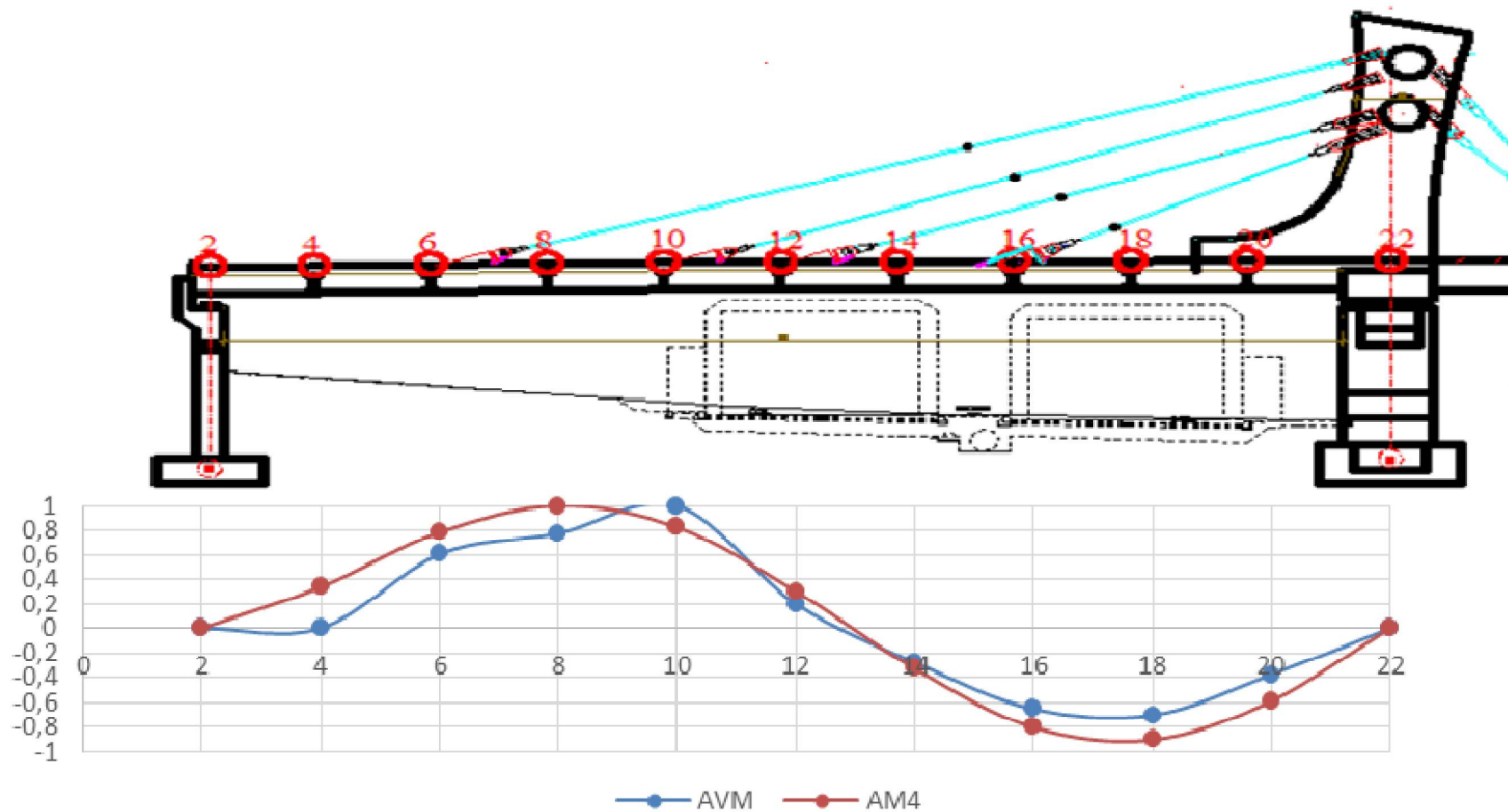


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## Experimentally and mathematically identified second mode shape



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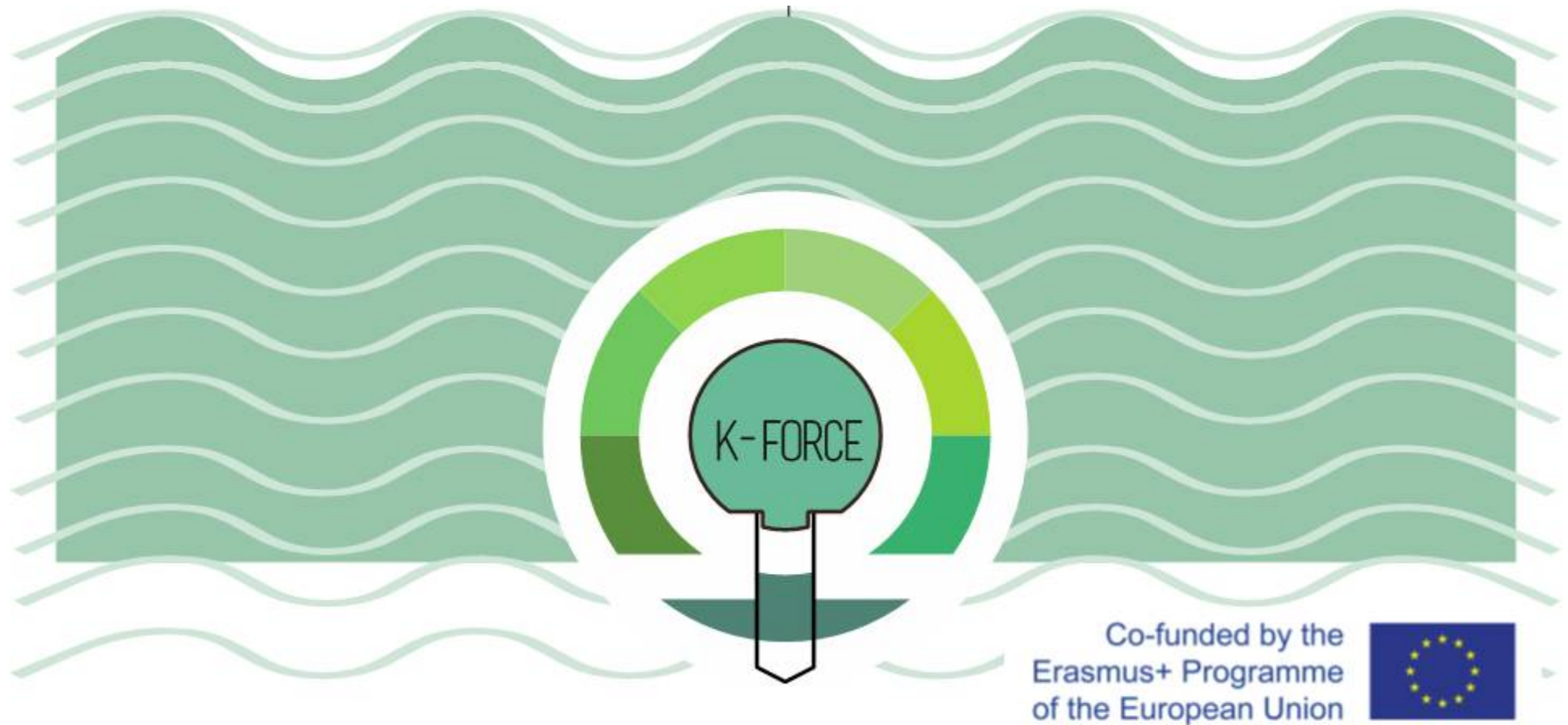
***The presented studies show that the signal analysis of ambient vibration records allows the determination of the dynamic characteristics of the bridge. In addition, the frequency and associated modes of vibration can be assessed with adequate mathematical model. The presented results clearly indicate the great potential that ambient vibration measurements hold for monitoring bridge structures. The data collected during the ambient vibration test, which only took some hours and very few resources, processed with adequate algorithms provided very useful information. The comparisons presented in case studies constitute a validation of the developed mathematical models and at the same time permit some fine tuning, especially concerning the boundary conditions and unexpected channel errors. In particular, this slides clearly shows that it was possible to extract a lot of useful information from data collected during the ambient vibration test.***



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Thank you  
for your attention  
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